

AVC-155

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CODING OF MOTION PICTURES AND ASSOCIATED AUDIO

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Title	MPEG 2 Proposal # 23 Summary
Purpose	Information
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**Introduction**

This document describes the Movies of the Future Program's image coding system in its third revision. This is the codec simulation system used for our MPEGII proposal.

The basic structure is a QMF pyramid sub-band coder. The coder operates on *frames* that are created by using two successive source *fields*. Lower resolution sub-bands are coded using scalable motion compensation while the highest resolution sub-bands do not use motion compensation at all. The sub-bands are compressed with a weighted, uniform scalar quantizer and a binary arithmetic coder.

**Scalability**

The algorithm allows a range over which the sequence can be decoded that is independent of the encoding rate. I.e., a 9Mb/sec sequence can be decoded at rates between approximately 400 Kbits/sec and 9Mbits/sec.

Scalability is provided through the use of sub-bands that can be selectively decoded. At the highest resolution, 6 spatio-temporal sub-bands are "intra-coded" and can be selectively decoded at any time. Information at lower resolutions is motion compensated on a level-by-level basis. Consequently, the first frame of a motion-compensated group of pictures can be decoded at any resolution, while other frames in the group of pictures can be decoded at any resolution less

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than or equal to the resolution of the preceding frame. One can therefore omit data from the bitstream down to the level of the lowest resolution band and can then interpret that data after decoding an intra-coded keyframe. At the highest level, data may be decoded or ignored without restriction.

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### Complexity

In its present form, the motion compensated subbands are more complex to decode than fullframe motion compensated hybrid coded images. Intermediate bands are interpolated up to quarter size before processing to prevent phase effects and filter artifacts from corrupting the estimate. We are investigating simplifications to this part of the algorithm. Since the upsampling operation is effectively a way to achieve fractional-pel motion compensation accuracy, it may be possible to achieve the fractional-pel accuracy without having to do all the explicit filtering.

The filters used in the subband decomposition are overlapping QMF transforms. This is a more complex transformation than the DCT. There are some optimizations that could be made to decrease the number of calculations.

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### Color Space

The color space in which MFC operates is the Y-Cb-Cr color space as defined by CCIR 601. The relationship between this color space and the RGB color space is governed by the following equations. There is no reason why the processing could not occur in a color space different from the color space of the original, but for now it is easiest to use the same color space

$$Yd = 0.299 \times R + 0.587 \times G + 0.144 \times B$$

$$Y = \frac{219 \times Yd}{255} + 16$$

$$Cb = \frac{126 \times (B - Yd)}{255} + 128$$

$$Cr = \frac{160 \times (R - Yd)}{255} + 128$$

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### Subband Decomposition

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A three level spatial sub-band decomposition is used for the lumi-

nance. The chrominance is split vertically into two sub-bands, after which the lowpass sub-band is decomposed into a two level pyramid. Subband decomposition is done serially on previously filtered and subsampled bands, resulting in a pyramid, or wavelet-like decomposition. In this discussion, level 1 refers to the highest frequency sub-images, level 2 refers to the midband sub-images, and level 3 refers to the lowest frequency sub-images. The baseband image is the level three sub-image containing the DC component. Note that for luminance, the level 1 images are 352 x 240 and that for chrominance the level 1 images are 176 x 120. The high vertical frequency subband is 352 x 240.

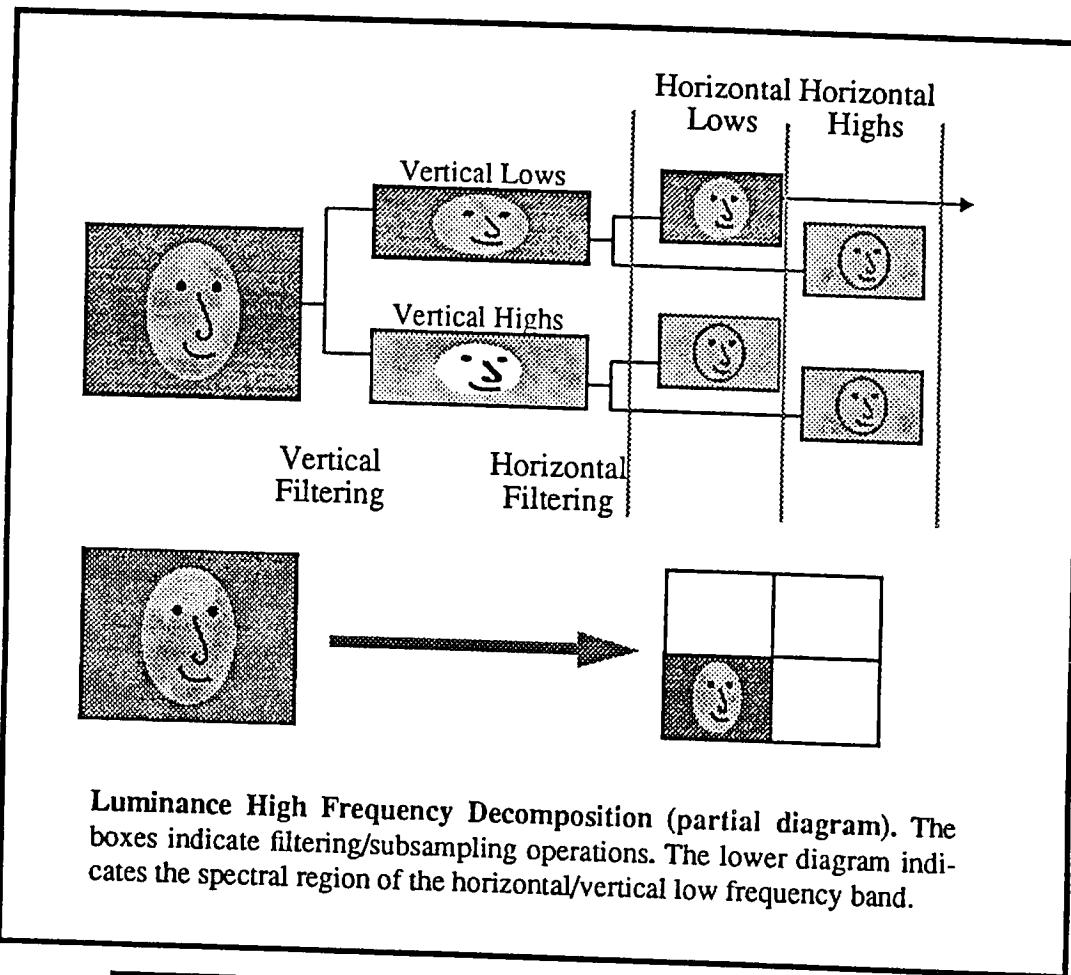
The level 1 luminance bands are further subjected to a 2-frame temporal analysis – sum and difference sub-images are formed.

Lower frequency luminance bands are predicted from previous images using a scaled motion vector field. In the submission tape, every 12 frames is intra-frame coded by omitting the prediction frame. This is, of course, a parameter of encoding.

The level 1 vertically high-passed subbands are subjected to an extra vertical sub-band split. This is done in order to effect a spatiotemporal stepwise approximation to the diagonal region of support (in the vertical/temporal plane) of an interlaced image sequence. This operation need not be performed for sequentially scanned source material.

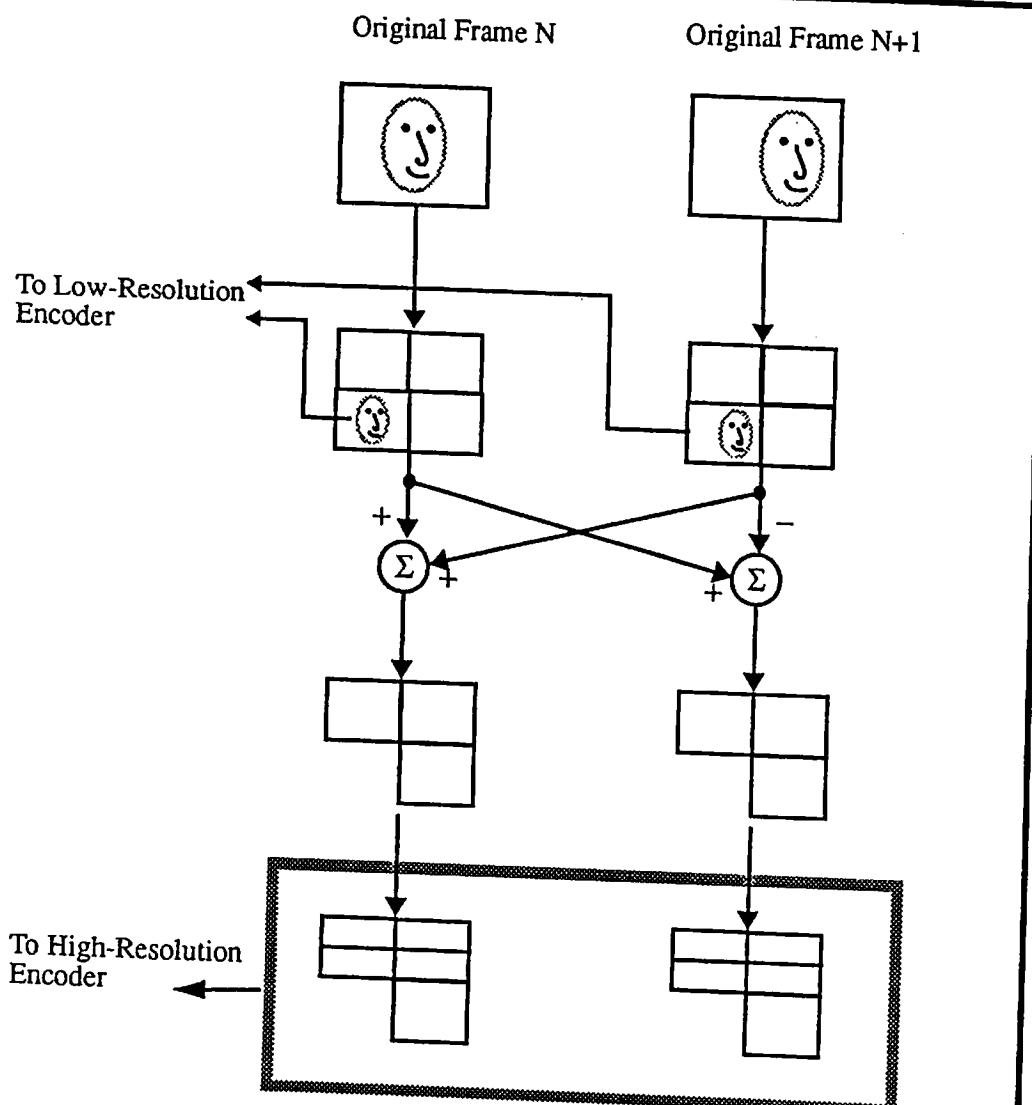
The highest vertical chrominance band is discarded in the tape submitted for testing, resulting in a 4:2:0 resolution ratio. This is not an essential part of the algorithm, 4:2:2 color can be coded if desired.

Each filter has a gain of  $\sqrt{2}$  associated with it, so that the overall gain of each subband increases by 2 as the pyramid is descended. This has been shown to provide enough precision to allow the pyramids to be stored as short integers.



Tap #	Low-pass Tap Value	High-pass Tap Value
1	0.019955	0.019955
2	-0.042705	0.042705
3	-0.052242	-0.052242
4	0.292705	-0.292705
5	0.564575	0.564575
6	0.292705	-0.292705
7	-0.052242	-0.052242
8	-0.042705	0.042705
9	0.019955	0.019955

Filter coefficient values of QMF pair used for spatial sub-band decomposition. (Coefficient values should be multiplied by  $\sqrt{2}$ )



Partial diagram of sub-band structure. First, each frame in a pair is spatially decomposed into a one level pyramid. The two basebands are fed into the low-resolution encoder, while the remaining subbands are decomposed into temporal subbands. The subbands with vertical detail are further split vertically. This results in ten high resolution sub-bands for each frame pair.

## Low Resolution Coder

Motion compensated prediction is used for the lower levels of luminance resolution and all levels of chrominance resolution. Motion vectors are formed using a hierarchical motion estimation method applied to the quarter-sized luminance images that are the inputs to the low resolution coder. Half pixel accuracy is used; a single, full size motion vector field is applied to each sub-image as described below. Motion vector fields are transmitted as in H.261..

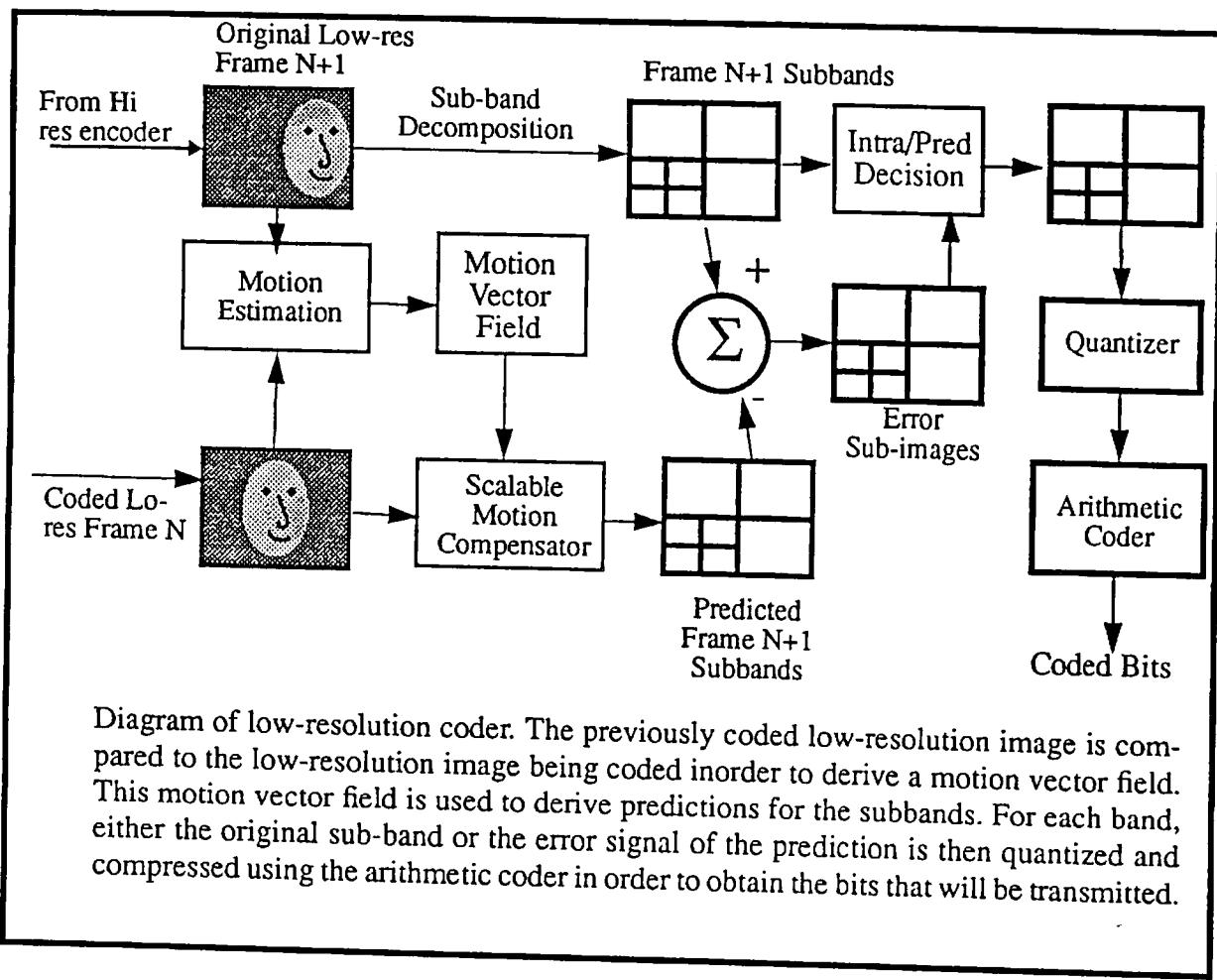


Diagram of low-resolution coder. The previously coded low-resolution image is compared to the low-resolution image being coded in order to derive a motion vector field. This motion vector field is used to derive predictions for the subbands. For each band, either the original sub-band or the error signal of the prediction is then quantized and compressed using the arithmetic coder in order to obtain the bits that will be transmitted.

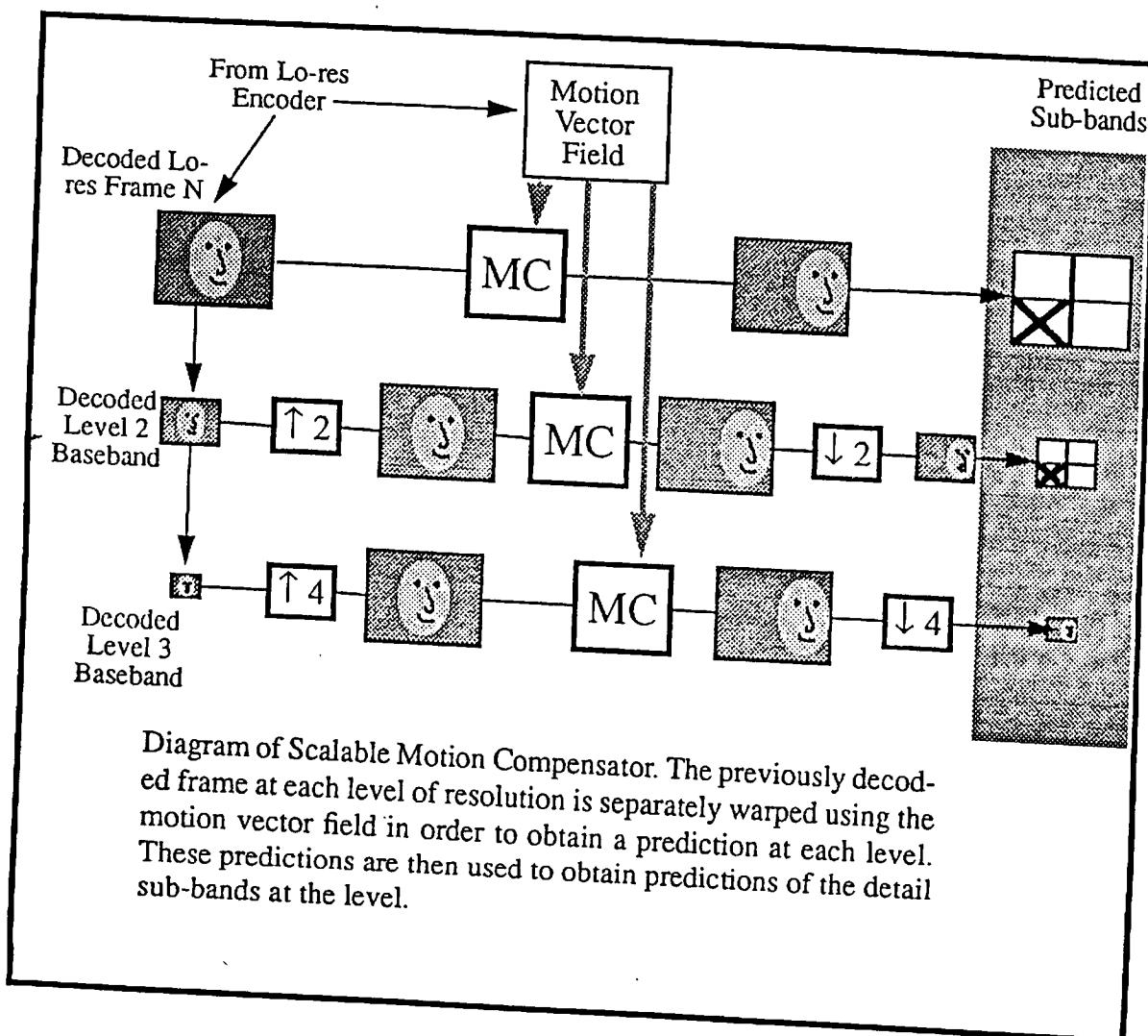
First, the previously decoded baseband (DC) image is interpolated up to 352x240 through a repeated application of the synthesis QMF filter set. This image is then warped using the vector field.

Next, this image is reduced back to its original size and used as a predictor for the baseband image in the next frame to be coded.

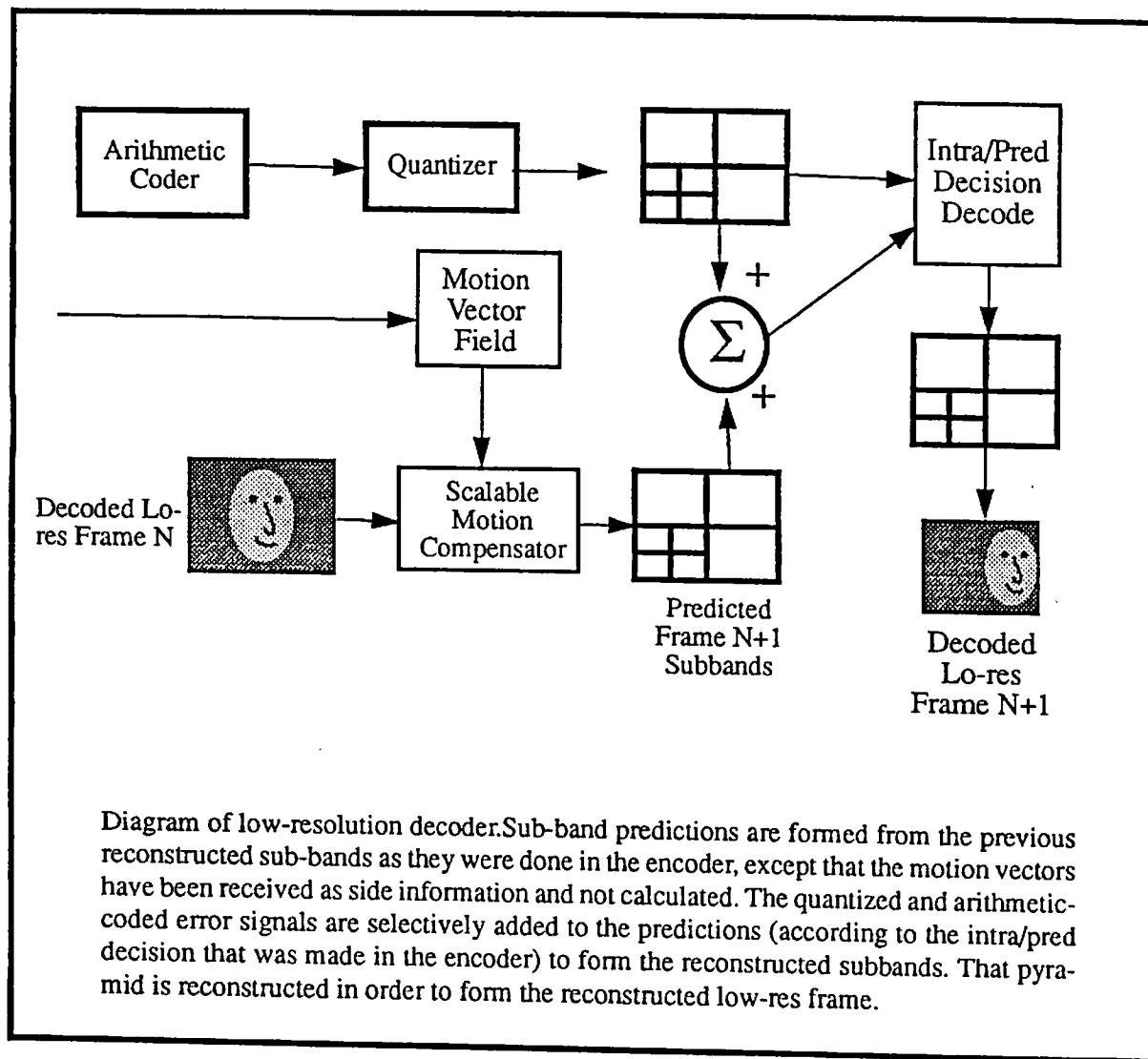
In decoding, the previous frame baseband image is interpolated up by a factor of two and added to the similarly processed level three subbands. The result of these operations is the reconstruction of a level two DC image.

This intermediate image is then scaled up by a factor of two, the motion vector field is applied to it, and it is then reduced back to its appropriate size and a one-level decomposition is applied to this image. The DC image is discarded, since a baseband predictor already exists and it is independent of all higher level images. This is the essence of the scalable motion compensation. The remaining three sub-images are the predictors for the level three bands in the next frame. This process is repeated for the next level, level two.

Thus, scalable motion compensation provides independent estimates (or predictors) for each level of the pyramid. The main expense of this method is that each image, in order to be predicted well, needs to be motion compensated at as high a resolution as possible. In the current implementation, this means that every motion compensated image is interpolated up to 352 x 240 and then decimated back down to its original size..



When a predicted sub-band has a prediction error with a variance greater than the variance of the original sub-band, the original sub-band is coded instead. Note that this intra/inter decision is made on a sub-band by sub-band basis and not on a block-by-block basis as in MPEG-I



Every 12 frames (6 frame pairs), the sub-bands of the first frame in the pair are all encoded using the original. This frame pair is then referred to as an **intra frame pair** while all other frame pairs are referred to as **predicted frame pairs**.

#### High Resolution Coder

The high resolution coder simply quantizes and arithmetic codes the

high-resolution sub-bands.

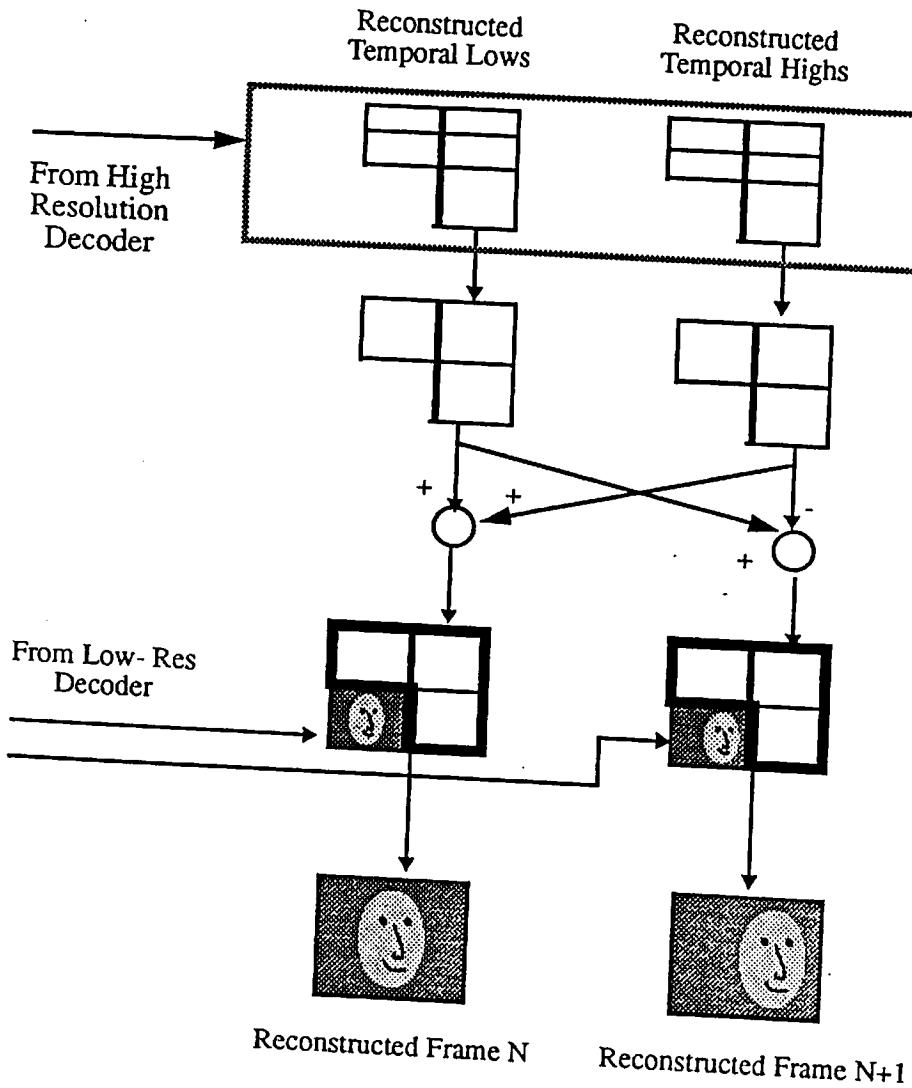


Diagram of Hi-Resolution Decoder. After the high-resolution subbands are decoded, the extra vertical subband decomposition in the vertical highs is reconstructed, and then the temporal subbands are reconstructed. The low-res decoder then supplies the baseband for this final set of pyramid reconstructions which yield the final reconstructed images.

## Quantization

The quantizer stepsize is determined by three factors.

We define a frequency weighting matrix that will be used to reduce the stepsize for high frequency data, analogous to the visual weight-

ing matrix used in a block coder. This matrix determines the relative weighting of the subbands themselves, and consists of one entry per subband.

In addition, we define a 44x30 point spatial weighting matrix, similar to *M-Quant* as used in MPEG-I. This matrix is created on a 16x16 pixel grid with respect to the full-size 704x480 point source image. This array is space-varying within each subband.

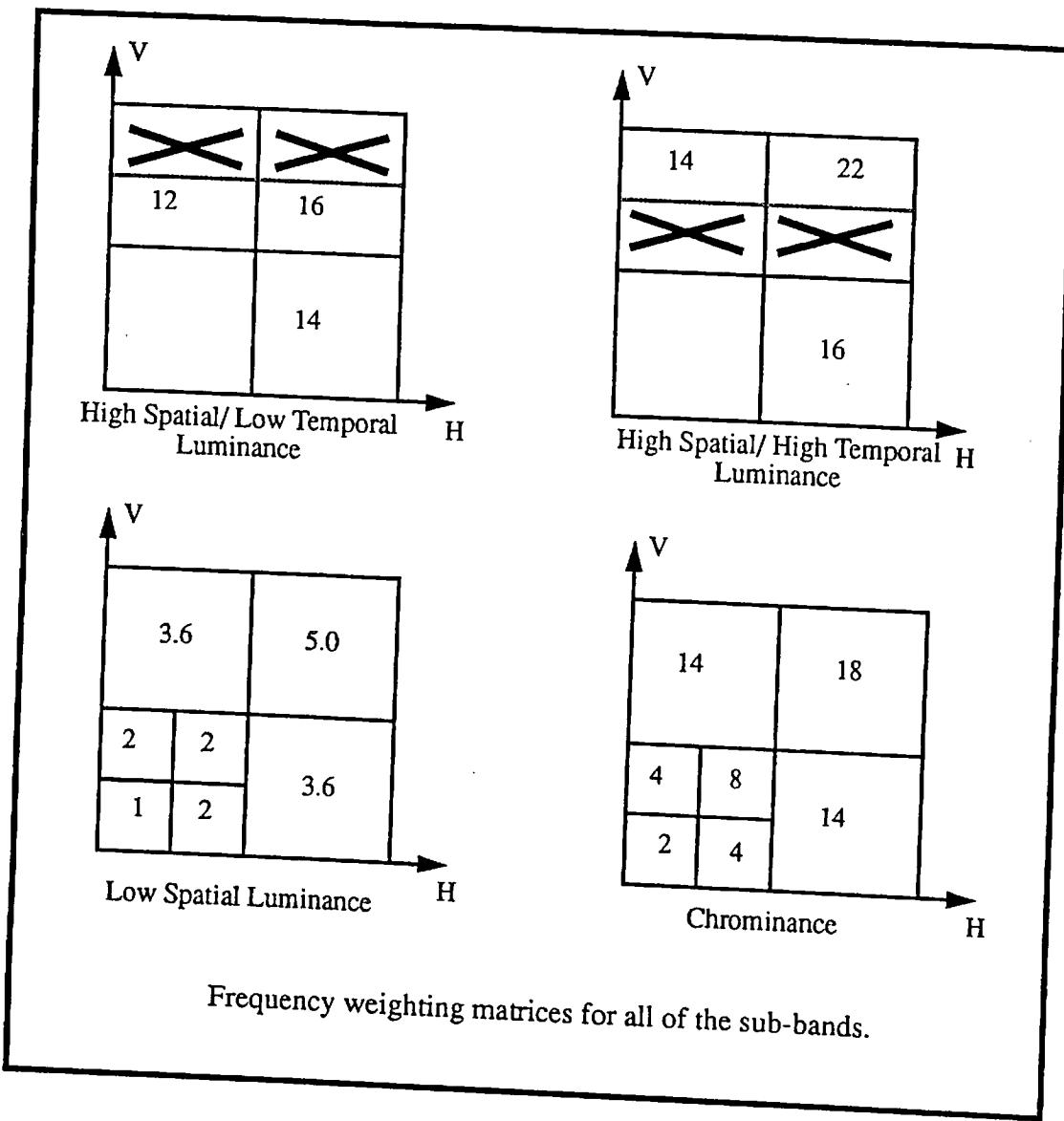
The rate controller reduces or increases all quantization factors by a scalar, the **Quantization Factor**, which is determined by the rate control buffer.

A single spatial weighting matrix is used for all subbands in the current frame to be quantized. It is (non-interpolatively) scaled to an appropriate size for the band. The matrix reduces the quantizer step size in inactive areas while increasing it in active areas.

At each point in each subband, the final quantizer stepsize that is used is the product of the frequency weighting matrix for that band, the spatial weighting matrix for that block in the subband, and the quantization factor.

The DC quantizer's step size does not vary spatially.

The spatial weighting matrix used for the highest-resolution subbands, those that are not within any motion compensation loop, is formed by taking point by point minima of the matrices for the two input frames that formed the temporal sub-bands.



### Computation of spatial weighting matrix

The spatial weighting matrix for each frame is formed on a  $16 \times 16$  block basis on the scale of the  $704 \times 480$  luminance image. The activity of each block is measured by summing the absolute values of the sub-band values (except baseband) that correspond to that region. So, the activity of a particular block is formed from the values of three  $8 \times 8$  blocks from the highest spatial subbands, three  $4 \times 4$  blocks from the next lowest sub-bands, and three  $2 \times 2$  blocks from the lowest detail sub-bands. An average of these sum-of-absolutes is then taken. The spatial quantization value for each region is then the measured activity for that region normalized by the average activity

of all blocks. Values less than 0.5 are rounded up to 0.5 and values above 2.0 are rounded down to 2.0. Finally, the mask is quantized with a step size of 0.1. The spatial mask is encoded with the same DPCM coder that is used on the basebands.

The mask values for the high-spatial-frequency temporally-split bands are formed for each block by taking the minimum of the two corresponding values in the spatial masks for the frames that were used to form the temporal sub-bands.

Bit allocation is altered by a scene change detector (described below). When a scene change is detected, the high spatial sub-bands are not sent for the frame pair before the scene change and for the 2 frame pairs afterwards. This is a temporal rate allocation based on temporal masking.

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### Rate Control

Rate control is achieved by controlling the overall quantization factor in response to the state of a simulated buffer. After each frame pair is coded, the simulated buffer state is updated, and then any modification to the overall quantization factor is made. The rate control algorithm is intended to keep image quality as constant as possible while providing the desired bitrate.

We assume that a steady quantization factor will provide steady perceived image quality. We assume that if a steady quantization factor is used to code the images of a sequence, then the number of bits for each frame pair will be steady as long as there is no scene change. We assume that in the absence of a scene change, the ratio between the number of bits needed to code an intra pair and a predicted pair is constant.

With the above assumptions and goals in mind, the rate control operates by repeatedly estimating what the buffer state will be at the end of the current GOP, and regulating the quantization factor so that the buffer state is approaching a cycle in which the average buffer state is one in which the buffer is half full.

Predicting the state of the buffer at the end of the GOP is achieved by knowing the number of frame pairs remaining to be coded in the GOP, the intra-predicted ratio, the number of bits used to code the latest frame pair, and the current buffer state. The condition which causes the quantization factor to be modified is when the projected buffer state is diverging from the desired buffer state. In other words, if the buffer state is approaching the desired buffer state, no modification is made to the quantization factor.

If the projected buffer state is too empty, the quantization factor is decreased by a value linearly related to the amount by which the projected buffer state deviates from half. If the the projected buffer state is too full, the quantization factor is similarly increased.

No modification is made to the quantization factor between coding the first and second frame pairs of a group of pictures. This is done to ensure that the intra-predicted ratio is measured properly.

When a scene change causes high-resolution sub-bands to be discarded, any decrease in the quantization factor is divided by a factor of 10. This is done in order to allocate less bits to the frames surrounding the scene change, and to make more bits available to avoid overflow if the next scene's footage is difficult to code.

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#### Scene Change Detection

Currently, scene changes are detected through examination of the motion vector fields. A sum is taken of the absolute difference between the neighboring vector components for each component of each vector. The idea is that a motion vector field that does not correspond to a scene change will have a significantly lower "difference-sum" than a motion vector field for a scene change.

When a scene change is detected, the previous frame pair, the current frame pair, and the next two frame pairs have their high-resolution sub-bands discarded

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#### Arithmetic Coding

Different coders are used for the basebands and for the non-basebands. Both coders use the same arithmetic coder, based on the JPEG Q-coder.

The fundamental manner in which this compression is being achieved is that the data to be encoded (currently either DPCM data or subband data) is quantized using a JPEG-style uniform scalar quantizer and then the arithmetic coder.

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#### Baseband coding

Basebands for luminance and chrominance channels are coded independently using a JPEG-style DPCM Coder. After applying a DPCM filter to the band and quantizing it, each coefficient is encoded by using Zero/Non-Zero, Positive/Negative, Magnitude, and Coefficient decisions. All decisions are conditioned by the quantized magnitude of the neighboring samples to the left and above.

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#### Non-baseband coding

The only difference between the baseband and non-baseband coders is that there is no DPCM filter applied to the sub-bands. Early attempts to improve the efficiency of the sub-band coder by condition-

ing decisions from samples adjacent in frequency have not been successful.

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**Channel model**

An errorless channel is assumed in the test material submitted, however, the scaled motion compensation and temporally filtered high resolution information insures separation of information from each band within the sequence. Thus, this coder insures spatiotemporally limited extent of channel errors. We are preparing a bitstream that allows re-synchronization in the face of channel errors or dropouts.

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**Sub-band reconstruction**

The spatial sub-bands are reconstructed by using the same QMF filters. The temporal sub-bands are reconstructed by inverting the sum-difference operation.

# MIT Media Lab MPEG

## 2 Proposal (#23)

### Coded Image Statistics

Because our algorithm coded images in pairs, bit counts are reported on a frame pair by frame pair basis. Signal-to-noise ratios are computed with respect to 255, not to signal peak values.

### Statistics for flower\_4...

#	Bits	Y-SNR	Cb-SNR	Cr-SNR	24.07	32.75	34.22	71	337840	23.57	32.01	33.57	118	221616	23.18	31.23			
0	290240	24.08	32.48	34.73	24.14	32.83	34.25	72	337840	23.58	31.93	33.40	119	23.14	23.14	31.37			
1	214536	24.21	32.56	34.71	24.14	32.83	34.40	73	258928	23.54	32.19	33.75	120	297568	22.93	31.43			
2	216712	24.09	32.40	34.58	24.11	32.46	34.46	53	250792	23.54	32.03	33.65	121	22.90	22.90	31.62			
3	242136	24.08	32.55	34.72	24.10	32.46	34.41	54	258224	23.45	32.21	33.81	122	228656	22.88	31.64			
4	237624	23.80	33.06	34.57	23.80	33.06	34.54	76	235864	23.47	32.14	33.68	123	22.99	22.99	31.45			
5	263416	23.82	33.08	34.67	23.82	33.08	34.43	77	246320	23.40	32.22	33.82	124	218512	22.99	31.42			
6	338768	23.81	33.05	34.56	23.79	32.97	34.49	80	227784	23.29	32.39	33.98	127	23.18	23.18	31.29			
7	272072	23.76	32.92	34.54	23.87	32.87	32.68	81	319880	23.19	32.38	33.80	131	246888	23.16	31.21			
8	259984	23.87	32.87	34.36	23.87	32.87	32.68	85	23.30	32.44	33.88	128	212128	23.30	30.94				
9	35	23.85	32.76	34.29	86	233104	23.22	32.39	33.91	133	23.22	32.32	33.76	129	23.26	31.23	32.84		
10	40	262280	23.78	32.78	34.46	87	23.26	32.40	33.85	134	234624	23.20	31.25	32.95	130	225600	23.30	31.08	
11	41	258528	23.75	32.85	34.45	88	227784	23.23	32.39	33.96	135	23.32	30.99	32.73	131	24.43	31.03	32.62	
12	42	23.73	32.53	34.26	90	240472	23.26	32.28	33.76	137	224744	23.32	31.07	32.65	132	31.16	31.16	32.85	
13	43	277584	23.72	32.43	34.09	91	23.21	32.23	33.80	138	229264	23.35	30.99	32.74	134	23.4624	23.35	30.99	
14	44	251960	23.85	32.33	33.91	92	250792	23.30	32.10	33.75	139	228504	23.35	31.17	32.72	135	23.32	30.99	32.72
15	45	360376	23.57	32.36	34.00	95	23.24	32.23	33.68	140	22.42	30.97	32.62	136	23.42	30.97	32.62		
16	46	23.64	32.54	34.08	94	255752	23.21	32.36	33.89	141	23.42	30.97	32.62	137	23.32	30.97	32.62		
17	47	360376	23.57	32.36	34.00	95	23.19	32.36	33.92	142	235752	23.26	31.38	32.82	138	22.48	31.16	32.57	
18	48	288272	23.52	32.45	34.20	99	23.19	32.23	33.80	138	229264	23.48	30.87	32.49	139	23.48	31.17	32.72	
19	49	23.49	32.35	34.16	100	290256	23.07	32.52	34.07	143	351176	23.48	31.11	32.64	144	246720	23.95	30.94	
20	50	250664	23.55	32.13	33.95	101	23.02	32.69	34.34	145	23.61	31.17	32.62	145	23.36	31.07	32.69		
21	51	23.63	32.46	34.01	98	283576	23.07	32.61	34.19	146	270472	23.71	31.02	32.54	146	23.44	31.15	32.79	
22	52	23.68	32.46	34.01	98	283576	23.17	32.35	33.87	147	23.93	30.79	32.38	147	23.44	31.15	32.79		
23	53	288272	23.52	32.45	34.20	99	23.19	32.42	33.97	148	246720	23.95	30.94	32.37	148	23.61	31.17	32.62	
24	54	23.49	32.35	34.16	100	290256	23.20	32.44	33.96	149	23.93	30.87	32.35	149	23.36	31.07	32.69		
25	55	23.67	32.09	33.85	102	298760	23.17	32.35	33.87	149	23.93	30.87	32.35	149	23.36	31.07	32.69		
26	56	251600	23.58	32.13	33.91	103	23.19	32.39	33.97	149	23.93	30.87	32.35	149	23.36	31.07	32.69		
27	57	23.58	32.22	33.91	104	300824	23.44	31.86	33.39	150	348224	23.26	31.68	33.18	151	23.19	31.95	33.43	
28	58	231056	23.48	32.29	33.94	105	291384	23.34	31.37	31.81	152	266328	23.16	31.79	33.33	153	23.28	31.71	33.24
29	59	23.39	32.43	34.04	106	291384	23.37	31.85	32.08	154	268584	23.15	31.45	33.06	155	23.17	31.50	33.30	
30	60	328504	23.30	32.39	34.04	107	291384	23.37	31.85	32.08	156	23.23	31.23	32.93	157	23.11	31.30	33.03	
31	61	23.50	32.39	34.08	108	348224	23.26	31.44	31.86	158	240872	23.14	31.23	32.94	159	23.16	31.28	32.90	

## Statistics for flower\_9...

#	Bits	Y-SNR	Cb-SNR	Cr-SNR	42	589080	25.28	35.69	36.33	89	24.89	35.54	36.15	136	616296	25.10	34.83	35.18	
0	650224	25.88	36.32	37.23	43	625592	25.21	35.67	36.28	90	586024	24.86	35.56	36.07	137	25.16	34.71	35.32	
1	546856	25.89	36.17	37.07	44	625592	25.24	35.64	36.34	91	592096	24.86	35.36	35.97	138	617592	25.26	34.68	35.19
2	585648	25.86	36.16	37.03	45	590264	25.26	35.59	36.09	92	592096	24.86	35.36	35.97	139	25.28	34.58	35.15	
3	556512	25.84	36.25	37.18	46	590264	25.20	35.55	36.11	93	594216	24.82	35.37	35.94	140	605400	25.10	34.69	35.24
4	597928	25.78	36.29	37.21	47	596416	25.17	35.85	36.23	97	594216	24.77	35.46	36.09	141	25.05	34.70	35.22	
5	593152	25.74	36.15	36.92	48	732280	25.09	35.81	36.26	95	618576	25.02	35.62	36.32	99	24.75	35.50	36.09	
6	634784	25.80	36.14	36.98	49	561536	25.05	35.38	36.04	100	609000	24.66	35.61	36.18	142	603160	24.98	34.76	35.27
7	725176	25.78	36.16	36.91	50	561536	25.07	35.23	35.84	101	609000	24.66	35.27	36.02	147	25.05	34.61	35.18	
8	596640	25.71	36.43	36.95	51	668680	25.09	35.29	35.96	102	593800	24.63	35.57	36.10	148	578664	25.43	33.94	34.49
9	636888	25.69	36.45	36.94	52	562688	25.05	35.25	35.96	103	593800	24.63	35.13	35.83	149	25.39	33.89	34.33	
10	560144	25.71	36.21	36.94	53	534816	24.95	35.32	36.27	104	616520	24.88	34.72	35.33					
11	558536	25.66	35.85	36.35	54	563328	24.93	35.35	36.04	105	593704	24.79	34.74	35.39					
12	543568	25.62	35.76	36.56	55	564576	24.91	35.41	36.24	106	568328	24.62	34.61	35.16					
13	556616	25.69	35.70	36.40	56	546498	24.92	35.25	36.29	107	600704	24.76	34.61	35.19					
14	676448	25.71	35.37	36.21	57	577048	24.94	35.39	36.03	108	673392	24.73	34.65	35.20					
15	525536	25.66	35.43	36.05	58	564576	25.03	35.16	35.83	109	568328	24.66	34.75	35.28					
16	556616	25.62	35.50	36.29	59	546498	25.06	35.18	35.83	110	531120	24.71	34.21	35.01					
17	543568	25.70	35.41	36.09	60	564576	24.98	35.37	36.00	111	541096	24.63	34.23	35.01					
18	556616	25.66	35.43	36.05	61	564576	25.02	35.36	36.06	112	600704	24.69	34.39	35.17					
19	560144	25.71	35.37	36.21	62	577048	24.94	35.39	36.03	113	531120	24.72	34.52	35.19					
20	556616	25.62	35.50	36.29	63	564576	25.03	35.16	35.72	114	507216	24.65	34.02	34.96					
21	556616	25.55	35.70	36.19	64	564576	24.98	35.37	36.00	115	568328	24.68	34.46	35.21					
22	556616	25.54	35.74	36.29	65	546498	24.92	35.25	35.95	116	541096	24.62	34.13	34.97					
23	556616	25.54	35.74	36.21	66	546498	25.03	35.49	36.15	117	614456	24.64	34.05	35.06					
24	556616	25.54	35.74	36.29	67	577048	24.94	35.39	36.03	118	507216	24.65	34.02	34.96					
25	556616	25.55	35.70	36.09	68	564576	25.12	35.38	35.96	119	568328	24.61	34.14	35.05					
26	556616	25.50	35.82	36.41	69	564576	25.22	35.50	35.87	120	614456	24.56	34.46	35.18					
27	556616	25.27	36.03	36.64	70	611336	25.03	35.49	36.15	121	614456	24.39	34.31	35.11					
28	556616	25.24	36.07	36.81	71	628624	25.15	35.47	36.06	122	517592	24.41	34.49	35.45					
29	556616	25.30	35.84	36.53	72	562384	25.03	35.43	36.10	122	517592	24.41	34.38	35.15					
30	555368	25.24	36.03	36.68	73	562384	25.03	35.43	36.03	123	512128	24.43	34.33	35.25					
31	556616	25.22	35.98	36.68	74	596768	25.00	35.44	36.11	124	512128	24.56	34.33	35.21					
32	584264	25.25	35.94	36.66	75	596768	25.01	35.44	36.11	125	512128	24.57	34.31	35.11					
33	556616	25.23	35.90	36.66	76	573608	24.93	35.60	36.22	127	554848	24.79	34.38	35.15					
34	600192	25.21	36.17	36.71	77	588280	24.93	35.60	36.19	128	613928	24.89	34.62	35.29					
35	556616	25.25	36.04	36.55	78	588280	24.92	35.32	36.12	129	585056	24.91	34.56	35.22					
36	663592	25.29	35.97	36.45	79	588280	24.91	35.34	36.04	130	585056	25.00	34.46	35.18					
37	556616	25.23	35.95	36.48	80	693240	24.83	35.86	36.22	131	746352	25.07	34.43	35.02					
38	567424	25.29	35.79	36.33	81	588280	24.85	35.98	36.33	132	632016	25.17	34.88	35.34					
39	556616	25.27	35.70	36.33	82	580792	24.87	35.72	36.21	133	632016	25.15	35.04	35.44					
40	574240	25.22	35.79	36.46	83	580792	24.88	35.66	36.12	134	568056	24.87	35.65	36.16	135	25.15	34.87	35.29	

### Statistics for mobile\_4...

					42	255800	23.07	31.22	31.47	89		23.12	30.90	31.04	136	245536	23.19	31.29	31.42
					43		23.08	31.30	31.51	90	242776	23.09	30.93	31.02	137		23.15	31.31	31.36
					44	263232	23.14	31.34	31.51	91		23.09	30.87	30.96	138	251296	23.19	31.33	31.38
#	Bits	Y-SNR	Cb-SNR	Cr-SNR	45	264600	23.16	31.31	31.50	92	245640	23.00	30.78	30.87	139		23.21	31.24	31.32
0	334104	22.58	31.57	31.95	46		23.18	31.17	31.50	93		23.06	30.74	30.83	140	250056	23.32	31.22	31.33
1		22.68	31.60	32.06	47	358424	23.11	31.29	31.61	95	244528	23.14	30.74	30.89	141		23.39	31.25	31.28
2	261464	22.63	31.63	32.07	48		23.22	31.42	31.62	96	334408	23.08	30.84	31.02	142	273200	23.46	31.24	31.23
3		22.67	31.59	32.02	49		23.17	31.21	31.49	102	230664	23.23	30.87	30.98	143		23.46	31.18	31.18
4	262912	22.66	31.60	31.95	50	267224	23.21	31.42	31.63	97		23.13	30.89	31.08	144	380248	23.32	31.05	31.10
5		22.65	31.49	31.85	51		23.20	31.40	31.68	98	230624	23.14	30.92	31.03	145		23.37	31.11	31.13
6	261024	22.67	31.47	31.79	52	269984	23.20	31.42	31.65	99		23.15	30.89	31.04	146	276568	23.40	31.23	31.24
7		22.63	31.34	31.69	53		23.16	31.34	31.56	100	233096	23.20	30.88	31.05	147		23.47	31.18	31.28
8	256040	22.74	31.41	31.67	54	265824	23.15	31.31	31.56	101		23.23	30.91	30.98	148	263472	23.53	31.13	31.16
9		22.75	31.29	31.66	55		23.17	31.21	31.49	102		23.23	30.87	30.98	149		23.57	31.06	31.06
10	245512	22.75	31.32	31.64	56	259440	23.16	31.16	31.41	103		23.22	30.86	30.97					
11		22.80	31.35	31.70	57		23.04	31.16	31.33	104	232120	23.21	30.92	30.97					
12	325704	22.71	31.33	31.65	58	260480	23.11	31.07	31.29	105		23.25	30.92	30.95					
13		22.79	31.44	31.76	59		23.12	31.07	31.27	106	238584	23.27	30.91	30.89					
14	244552	22.80	31.37	31.80	60	355992	23.08	31.20	31.40	107		23.33	30.84	30.89					
15		22.86	31.42	31.77	61		23.10	31.27	31.49	108	348328	23.21	30.91	30.95					
16	242808	22.92	31.40	31.75	62	257824	23.12	31.29	31.52	109		23.34	30.96	30.96					
17		22.91	31.35	31.75	63		23.10	31.31	31.54	110	247080	23.26	30.95	30.89					
18	243680	22.92	31.37	31.65	64	255784	23.15	31.27	31.54	111		23.20	30.98	30.92					
19		22.87	31.24	31.57	65		23.17	31.19	31.40	112	246720	23.31	31.05	30.93					
20	240536	22.88	31.24	31.57	66	260808	23.14	31.23	31.36	113		23.35	30.96	30.90					
21		22.91	31.19	31.51	67		23.19	31.17	31.42	114	252992	23.36	30.89	30.94					
22	242016	22.94	31.18	31.57	68	257520	23.12	31.14	31.30	115		23.37	30.90	30.97					
23		22.87	31.27	31.51	69		23.17	31.09	31.26	116	258296	23.38	30.94	31.00					
24	327984	22.85	31.18	31.49	70	259464	23.14	31.03	31.26	117		23.40	30.92	30.93					
25		22.94	31.24	31.65	71		23.16	30.99	31.19	118	257240	23.44	31.02	31.05					
26	236544	22.97	31.35	31.68	72	360200	23.00	31.07	31.24	119		23.43	31.04	31.05					
27		22.96	31.28	31.63	73		23.12	31.08	31.25	120	355528	23.39	31.01	31.05					
28	234560	22.92	31.31	31.65	74	269640	23.12	31.10	31.24	121		23.42	31.13	31.23					
29		22.98	31.28	31.57	75		23.09	31.09	31.20	122	250384	23.40	31.20	31.25					
30	233704	22.99	31.15	31.46	76	252880	23.00	30.99	31.05	123		23.35	31.20	31.28					
31		22.99	31.16	31.37	77		22.96	30.96	31.01	124	252672	23.37	31.16	31.25					
32	238112	23.04	31.11	31.34	78	246048	23.14	30.90	31.02	125		23.35	31.09	31.22					
33		23.09	31.16	31.31	79		23.13	30.84	31.00	126	247920	23.14	31.15	31.18					
34	244032	23.11	31.27	31.39	80	241264	23.13	30.81	30.95	127		23.23	31.07	31.14					
35		23.08	31.23	31.38	81		23.16	30.80	30.97	128	240000	23.28	31.17	31.21					
36	350032	23.10	31.24	31.55	82	237400	23.15	30.80	30.95	129		23.31	31.08	31.24					
37		23.11	31.34	31.60	83		23.21	30.80	30.94	130	243232	23.27	31.22	31.33					
38	258368	23.13	31.33	31.62	84	336752	23.09	30.92	31.04	131		23.25	31.23	31.32					
39		23.10	31.32	31.61	85		23.18	30.92	31.08	132	349488	23.16	31.25	31.29					
40	265208	23.08	31.40	31.64	86	244864	23.17	30.90	31.12	133		23.19	31.36	31.43					
41		23.05	31.32	31.51	87		23.13	30.93	31.05	134	250616	23.16	31.48	31.54					
					88	242504	23.12	30.91	31.05	135		23.17	31.43	31.53					

### Statistics for tennis\_9...

					42	658896	30.73	42.72	43.89	89		29.39	39.57	39.64	136	499376	25.58	39.52	39.47
					43		30.78	42.64	43.90	90	615208	29.44	39.63	39.69	137		25.51	39.52	39.52
					44	651496	30.39	42.67	43.82	91		29.43	39.59	39.65	138	504480	25.49	39.76	39.74
#	Bits	Y-SNR	Cb-SNR	Cr-SNR	45		30.40	42.72	43.97	92	623080	29.45	39.55	39.72	139		25.50	39.66	39.75
0	690232	25.83	39.76	41.07	46	651032	30.38	42.75	43.90	93		29.45	39.53	39.66	140	563632	25.48	39.67	39.57
1		25.75	39.80	41.09	47		30.41	42.64	43.80	94	280864	25.80	39.40	39.57	141		25.51	39.56	39.71
2	553024	25.68	39.83	41.18	48	696152	30.29	42.29	42.56	95		25.80	39.44	39.53	142	598504	25.57	39.46	39.68
3		25.86	39.86	41.28	49		30.35	42.53	43.60	96	720224	25.60	39.81	39.83	143		25.57	39.37	39.61
4	554000	25.97	39.87	41.27	50	651664	30.17	42.38	43.48	97		24.31	40.30	40.45	144		25.59	39.41	39.60
5		25.86	39.86	41.23	51		30.17	42.27	43.43	98	318096	24.31	40.22	40.30	145		25.55	39.43	39.63
6	542872	25.76	39.71	41.07	52	657240	29.89	42.89	42.20	99		24.31	40.12	40.28	146	605488	25.51	39.47	39.66
7		25.89	39.68	40.92	53		29.85	42.18	43.13	100	344232	24.31	40.18	40.26	147		25.51	39.42	39.61
8	607592	25.70	39.75	40.94	54	662968	29.66	42.10	42.98	101		24.32	40.11	40.38	148	556728	25.37	39.31	39.57
9		25.84	39.79	41.08	61		28.85	41.79	42.50	102	934032	28.98	40.43	40.66			25.33	39.27	39.55
10	602840	25.56	39.79	41.09	62	708840	28.62	41.69	42.32	103		28.98	40.42	40.65					
11		25.54	39.69	40.99	63		28.												

### Statistics for mobile\_9...

#	B16s	Y-SNR	CB-SNR	CR-SNR	44	601122	30.10	38.85	39.20	96	631032	31.19	42.18	42.57	39.47
0	681984	24.25	34.27	34.76	45	591240	24.87	33.93	34.34	90	558040	25.05	33.02	33.43	34.74
1	582016	24.33	34.24	34.75	47	594400	24.90	33.98	34.32	92	57736	25.01	33.46	33.73	34.58
2	582336	24.40	34.18	34.74	48	712848	24.95	33.79	34.23	94	598816	25.21	33.48	33.87	34.64
3	586698	24.54	34.29	34.76	49	572986	24.94	33.59	33.97	104	595912	25.40	33.68	34.00	34.02
4	582336	24.42	34.10	34.75	50	587016	24.94	33.98	34.41	55	597456	24.95	33.59	34.17	34.33
5	586698	24.46	34.04	34.76	51	574760	24.97	33.93	34.41	100	578216	25.27	33.80	34.18	34.67
6	582336	24.42	34.07	34.75	52	597456	24.96	33.98	34.56	99	572592	25.28	33.85	34.19	34.49
7	586698	24.49	34.04	34.76	53	587016	25.00	34.04	34.48	97	724704	25.22	33.52	33.91	142
8	569208	24.51	34.07	34.75	54	574760	24.94	33.93	34.41	100	578216	25.25	33.85	34.18	144
9	554504	24.55	34.08	34.76	55	59929	24.95	33.72	34.16	102	584128	25.30	33.68	34.20	148
10	543936	24.47	34.09	34.41	56	572986	24.94	33.59	34.17	103	595912	25.40	33.68	34.04	149
11	557064	24.75	34.02	34.38	57	575018	24.97	33.68	33.97	104	595912	25.37	33.84	34.02	149
12	666592	24.46	34.14	34.66	58	572986	24.94	33.59	34.04	103	584128	25.30	33.68	34.04	149
13	536992	24.49	34.19	34.67	59	701544	24.97	33.68	33.97	104	595912	25.45	33.81	33.94	149
14	556992	24.49	34.19	34.67	60	607048	24.98	33.68	34.04	105	602704	25.43	33.72	33.95	149
15	554504	24.55	34.08	34.41	61	701544	24.91	33.62	34.21	107	703076	25.34	33.53	33.72	149
16	554504	24.67	34.16	34.70	62	564088	24.94	33.69	34.20	109	570168	25.45	33.88	34.20	149
17	557064	24.73	34.11	34.76	63	59929	24.95	33.68	34.20	110	605808	25.33	33.80	34.11	149
18	557064	24.47	34.09	34.41	64	55992	24.95	33.59	34.21	111	595912	25.37	33.84	34.02	149
19	557008	24.71	34.21	34.68	65	574632	24.98	33.74	34.20	112	594704	25.33	33.81	33.99	149
20	575008	24.79	34.23	34.69	66	579464	25.03	33.59	34.00	113	570376	25.31	33.68	33.98	149
21	606768	24.42	34.21	34.77	67	575018	25.07	33.74	34.21	114	584560	25.31	33.59	33.98	149
22	570508	24.79	34.23	34.70	68	579464	25.05	33.59	34.00	115	570376	25.31	33.68	33.98	149
23	586698	24.49	34.21	34.66	69	59929	25.07	33.68	34.20	116	585744	25.28	33.85	34.07	149
24	730952	24.29	34.12	34.57	70	572972	25.07	33.68	34.20	117	585744	25.22	33.86	34.09	149
25	52506	34.19	33.92	34.67	71	549256	25.04	33.21	33.56	122	525320	24.77	33.76	34.11	149
26	586698	24.49	34.05	34.55	72	549256	25.04	33.22	33.56	122	525320	24.77	33.76	34.11	149
27	502536	25.10	33.98	34.40	73	549256	25.04	33.22	33.56	122	525320	24.77	33.76	34.11	149
28	586698	24.98	34.04	34.44	74	549256	25.03	33.38	33.68	122	525320	24.77	33.76	34.11	149
29	593800	24.96	34.30	34.64	75	602552	25.01	33.66	34.00	122	535592	25.07	33.92	34.28	149
30	593800	24.96	34.30	34.64	76	569356	25.01	33.66	34.00	122	569356	25.01	33.92	34.28	149
31	593800	24.96	34.30	34.64	77	569356	25.01	33.66	34.00	122	535592	25.07	33.92	34.28	149
32	586698	25.06	34.05	34.55	78	570376	25.07	33.74	34.11	122	570376	25.16	33.68	33.98	149
33	602536	25.10	33.98	34.40	79	570376	25.07	33.74	34.11	122	570376	25.16	33.68	33.98	149
34	602536	25.11	33.91	34.44	80	54920	25.04	33.21	33.56	122	525320	24.77	33.76	34.11	149
35	729752	25.11	33.92	34.67	81	535472	25.10	33.24	33.56	122	527760	24.77	33.88	34.17	149
36	551376	25.02	34.19	34.67	82	535472	25.08	33.21	33.56	122	527760	24.77	33.88	34.17	149
37	603768	25.02	34.19	34.67	83	612200	25.04	33.59	33.90	122	562952	24.81	34.02	34.44	149
38	603768	24.98	34.17	34.67	84	675576	25.04	33.59	33.90	122	754840	24.85	34.04	34.45	149
39	603768	24.98	34.17	34.67	85	549208	25.03	33.81	34.12	122	547288	25.03	33.81	34.12	149
40	591152	24.80	34.17	34.67	86	549208	25.03	33.81	34.12	122	547288	25.03	33.81	34.12	149
41	591152	24.87	34.02	34.50	87	549208	25.00	33.49	34.08	122	619228	24.79	34.49	34.57	149
42	590728	24.45	34.00	34.39	88	550952	25.02	33.45	33.75	123	550952	25.02	33.45	33.75	149
43	590728	24.45	34.00	34.39	89	550952	25.02	33.45	33.75	123	550952	25.02	33.45	33.75	149
44	590728	24.45	34.00	34.39	90	550952	25.02	33.45	33.75	123	550952	25.02	33.45	33.75	149
45	590728	24.45	34.00	34.39	91	550952	25.02	33.45	33.75	123	550952	25.02	33.45	33.75	149
46	590728	24.45	34.00	34.39	92	550952	25.02	33.45	33.75	123	550952	25.02	33.45	33.75	149
47	590728	24.45	34.00	34.39	93	550952	25.02	33.45	33.75	123	550952	25.02	33.45	33.75	149
48	590728	24.45	34.00	34.39	94	550952	25.02	33.45	33.75	123	550952	25.02	33.45	33.75	149
49	590728	24.45	34.00	34.39	95	550952	25.02	33.45	33.75	123	550952	25.02	33.45	33.75	149
50	590728	24.45	34.00	34.39	96	550952	25.02	33.45	33.75	123	550952	25.02	33.45	33.75	149
51	590728	24.45	34.00	34.39	97	550952	25.02	33.45	33.75	123	550952	25.02	33.45	33.75	149
52	590728	24.45	34.00	34.39	98	550952	25.02	33.45	33.75	123	550952	25.02	33.45	33.75	149
53	590728	24.45	34.00	34.39	99	550952	25.02	33.45	33.75	123	550952	25.02	33.45	33.75	149
54	590728	24.45	34.00	34.39	100	578216	25.28	33.80	34.18	124	578216	25.28	33.80	34.18	149
55	590728	24.45	34.00	34.39	101	578216	25.28	33.80	34.18	124	578216	25.28	33.80	34.18	149
56	590728	24.45	34.00	34.39	102	584128	25.30	33.80	34.20	124	584128	25.30	33.80	34.20	149
57	590728	24.45	34.00	34.39	103	595912	25.40	33.84	34.04	125	595912	25.40	33.84	34.04	149
58	590728	24.45	34.00	34.39	104	595912	25.40	33.84	34.04	125	595912	25.40	33.84	34.04	149
59	590728	24.45	34.00	34.39	105	595912	25.40	33.84	34.04	125	595912	25.40	33.84	34.04	149
60	590728	24.45	34.00	34.39	106	602704	25.45	33.84	34.00	125	602704	25.45	33.84	34.00	149
61	590728	24.45	34.00	34.39	107	703076	25.45	33.84	34.00	125	703076	25.45	33.84	34.00	149
62	590728	24.45	34.00	34.39	108	703076	25.45	33.84	34.00	125	703076	25.45	33.84	34.00	149
63	590728	24.45	34.00	34.39	109	703076	25.45	33.84	34.00	125	703076	25.45	33.84	34.00	149
64	590728	24.45	34.00	34.39	110	703076	25.45	33.84	34.00	125	703076	25.45	33.84	34.00	149
65	590728	24.45	34.00	34.39	111	703076	25.45	33.84	34.00	125	703076	25.45	33.84	34.00	149
66	590728	24.45	34.00	34.39	112	703076	25.45	33.84	34.00	125	703076	25.45	33.84	34.00	149
67	590728	24.45	34.00	34.39	113	703076	25.45	33.84	34.00	125	703076	25.45	33.84	34.00	149
68	59072														

### Statistics for tennis\_4...

					42	237560	29.33	40.91	41.68	89		28.52	38.00	37.72	136	219232	24.28	38.09	37.94
					43		29.42	40.83	41.53	90	237640	28.55	37.98	37.67	137		24.21	38.23	38.00
					44	336536	29.63	41.56	42.20	91		28.53	37.95	37.66	138	204160	24.17	38.26	38.06
#	Bits	Y-SNR	Cb-SNR	Cx-SNR	45	29.62	41.51	42.13	92	262568	28.56	37.97	37.72	139		24.12	38.18	38.11	
0	299088	23.46	38.33	38.85	46	330880	29.61	41.49	42.20	93		28.54	37.93	37.77	140	221032	24.07	38.18	37.98
1		23.36	38.35	38.92	47		29.70	41.38	42.18	94	145816	25.59	37.96	37.72	141		24.01	38.02	37.98
2	223568	23.37	38.39	38.99	48	373152	29.59	41.25	41.90	95		25.60	37.90	37.71	142	245408	24.06	37.93	37.96
3		23.62	38.47	39.07	49		29.59	41.20	41.65	96	474344	25.41	38.01	37.88	143		24.06	37.93	37.93
4	220864	23.62	38.46	39.05	50	336384	29.46	41.06	41.68	97		24.15	38.69	38.53	144	333856	24.04	37.71	37.55
5		23.52	38.49	39.01	51		29.43	40.91	41.55	98	175848	24.15	38.70	38.51	145		24.06	37.80	37.73
6	215064	23.47	38.39	38.92	52	298448	29.05	40.62	41.10	99		24.15	38.66	38.49	146	260040	24.02	37.95	37.80
7		23.59	38.38	38.82	53		28.96	40.66	41.05	100	174064	24.15	38.62	38.51	147		23.96	37.87	37.86
8	249480	23.61	38.55	38.08	54	301856	28.85	40.62	40.79	101		24.15	38.57	38.43	148	255808	23.94	37.88	37.88
9		23.70	38.55	39.08	55		28.81	40.61	40.67	102	347240	27.90	38.58	38.33	149		23.89	37.93	37.92
10	258768	23.59	38.57	39.00	56	306072	28.55	40.42	40.64	103		27.91	38.53	38.33					
11		23.56	38.49	39.12	57		28.55	40.29	40.43	104	319888	27.93	38.49	38.36					
12	362592	23.42	38.59	39.48	58	321320	28.33	40.18	40.39	105		27.93	38.46	38.28					
13		23.67	38.61	39.40	59		28.39	40.18	40.29	106	320232	27.95	38.44	38.29					
14	275336	24.10	38.61	39.26	60	372504	28.05	40.14	40.35	107		27.94	38.46	38.30					
15		23.85	38.60	39.35	61		28.11	40.08	40.39	108	466528	27.89	38.49	38.31					
16	270992	23.69	38.59	39.34	62	326856	27.93	40.09	40.30	109		27.90	38.47	38.31					
17		23.63	38.56	39.38	63		28.01	39.95	40.17	110	314432	27.90	38.44	38.32					
18	255456	23.72	38.61	39.26	64	231384	25.92	39.65	39.81	111		27.92	38.42	38.31					
19		23.87	38.62	39.28	65		25.92	39.51	39.69	112	250472	27.71	38.36	38.17					
20	267376	23.93	38.55	39.11	66	357824	25.80	39.48	39.45	113		27.69	38.32	38.17					
21		23.81	38.47	39.06	67		25.39	38.16	38.13	114	259120	27.67	38.31	38.12					
22	281728	23.36	38.36	38.97	68	121248	25.31	38.13	38.03	115		27.66	38.29	38.15					
23		23.81	38.39	39.04	69		25.23	38.09	38.02	116	218728	27.41	38.27	38.08					
24	352040	24.28	38.42	39.30	70	138296	25.17	38.08	37.99	117		27.40	38.19	38.06					
25		25.01	38.67	39.77	71		25.08	38.05	37.93	118	234064	27.35	38.18	38.07					
26	267776	25.40	38.77	39.88	72	369016	27.91	37.94	37.82	119		27.30	38.14	38.01					
27		25.83	38.87	40.15	73		27.92	37.90	37.78	120	378904	27.21	38.04	37.86					
28	224096	26.19	39.03	40.13	74	244840	28.21	37.83	37.73	121		27.23	38.06	37.92					
29		26.35	39.04	40.09	75		28.23	37.82	37.67	122	266288	27.08	38.09	37.89					
30	200768	26.56	39.15	40.31	76	240632	28.27	37.79	37.60	123		27.01	38.12	37.83					
31		26.82	39.32	40.42	77		28.25	37.74	37.59	124	250864	26.42	38.08	37.66					
32	179240	27.06	39.51	40.40	78	232816	28.32	37.68	37.53	125		25.98	38.11	37.54					
33		27.32	39.66	40.55	79		28.33	37.71	37.50	126	247960	25.57	38.04	37.51					
34	174416	27.59	39.80	40.65	80	239832	28.23	37.74	37.56	127		25.24	38.05	37.48					
35		27.76	39.97	40.68	81		28.18	37.72	37.54	128	255240	24.90	38.07	37.58					
36	216808	28.22	40.00	40.67	82	252624	28.22	37.76	37.58	129		24.82	38.06	37.65					
37		28.20	40.31	40.87	83		28.22	37.77	37.58	130	252256	24.74	38.14	37.65					
38	163568	28.42	40.23	40.84	84	387224	28.36	37.99	37.75	131		24.69	38.08	37.62					
39		28.45	40.34	40.65	85		28.39	37.98	37.74	132	333672	24.55	37.96	37.40					
40	191416	28.98	40.66	41.00	86	250216	28.44	38.00	37.80	133		24.50	37.97	37.63					
41		29.11	40.56	41.07	87		28.46	37.99	37.71	134	246160	24.36	38.16	37.70					
					88	245648	28.54	37.99	37.71	135		24.30	38.14	37.90					