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**Jitter and wander accumulation in digital
networks**

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NOTES

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2 In this Supplement, the expression “Administration” is used for conciseness to indicate both a telecommunication administration and a recognized operating agency.

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As an example of what these factors mean consider the white FM noise component in Figure I-2 (plus sign tagged data). For the 10 000 second lag, the square root of the sample variance is 8×10^{-12} . The 90% confidence interval for the true variance is bounded by the confidence factors multiplied by the sample variance. This leads to the square root of the Allan variance being bounded between 6.9×10^{-12} and 9.8×10^{-12} with a 90% confidence level.

Reference

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Supplement No. 36

JITTER AND WANDER ACCUMULATION IN DIGITAL NETWORKS

(Referred to in Recommendation G.824)

The present Supplement describes a model which has been used to compute jitter/wander accumulation in digital networks arising from cascaded digital regenerators and asynchronous digital multiplexes. This model does not include other sources of wander generation; e.g., environmental, disruptions in synchronization reference distribution, etc.

1 Jitter and wander accumulation – Digital regenerator component

The most widely used model of regenerator jitter/wander accumulation, attributed to Chapman [1], treats the regenerator as linear, shift-invariant system. In order to compute the accumulated jitter/wander after N cascaded regenerators, intrinsic regenerator jitter/wander is categorized in terms of “random” and “systematic” components. Chamzas model of regenerator jitter/wander accumulation [2] addresses how stochastic variations in regenerator retiming circuits affect jitter/wander accumulation. The results of this study demonstrate that use of the appropriate *mean* jitter/wander transfer characteristic in the identical regenerator accumulation model, summarized above, provides a very good estimate to jitter/wander accumulation computed assuming a stochastic variation of retiming circuits.

Using Chapman’s model for a chain of N *identical* regenerators, defining $H_1(j\omega)$ as the jitter/wander transfer characteristic for one regenerator, and redefining the random and systematic components as completely uncorrelated and correlated components, respectively,

- the power spectral density of the random jitter/wander component is:

$$\Phi_N^R(\omega) = \Phi_{i1}^R |H_1(j\omega)|^2 \frac{1 - |H_1(j\omega)|^{2N}}{1 - |H_1(j\omega)|^2} \quad (1)$$

where Φ_{i1}^R is the constant, internally generated, random (pattern independent plus uncorrelated pattern dependent) jitter/wander power spectral density for one regenerator.

- the power spectral density of the systematic jitter/wander component is:

$$\Phi_N^S(\omega) = \Phi_{i1}^S |H_1(j\omega)|^2 \frac{|1 - H_1(j\omega)^N|^2}{|1 - H_1(j\omega)|^2} \quad (2)$$

where Φ_{i1}^S is the constant, internally generated, systematic (correlated pattern dependent) jitter/wander power spectral density for one regenerator. Φ_{i1}^R and Φ_{i1}^S can be estimated from practical measurements based upon the regenerator’s jitter/wander response to short and long word lengths from a pattern generator, and correlation studies.

When there is no peaking in the regenerator jitter/wander transfer characteristic, the systematic jitter/wander accumulates much more rapidly than the random jitter/wander [1], [4], [5]; as a result, random jitter/wander accumulation is often ignored. However, for a large number of regenerators with peaking in the jitter/wander transfer characteristic, the total jitter/wander accumulation can be dominated by the random component.

2 Jitter and wander accumulation – Asynchronous digital multiplex component

With Gaussian input jitter/wander, having an rms amplitude of σ , and double-sided power spectral density $\theta_{in}(f)$, the unfiltered multiplex intrinsic jitter/wander is given by [6].

$$\begin{aligned} \Phi_{out}(f) = & \text{sinc}^2 f \text{ rep } \Phi_{in}(f) + \sum_{n=1}^x \frac{p^2}{(2\pi n)^2} [\delta(f-n) + \delta(f+n)] \\ & + \sum_{n=1}^x \frac{\text{sinc}^2 f}{(2\pi n)^2} [\text{rep } Z_n(f-np) + \text{rep } Z_n(f+np)] \end{aligned} \quad (3)$$

where $\text{rep } X(f) = \sum_{k=-x}^x X(f-k)$

$$Z_n(f) = e^{-2\pi n \sigma} \left[\delta(f) + \sum_{k=1}^x \left[\frac{2\pi n}{k!} \right]^{2k} \Phi_{in}(f) * \dots * \Phi_{in}(f) \right]$$

k terms

p Multiplexer stuffing ratio

f jitter/wander frequency normalized by the multiplexer maximum suffising frequency

3 Method of combination

Assuming that the jitter/wander accumulation from each component part can be modeled by filtered Gaussian random variables, the power spectrum and rms amplitude after each component part¹⁾ is computed as the accumulation due to the preceding parts according to the following rules [3]:

- i) The jitter/wander spectrum at the output of a chain of regenerators is the power sum of the jitter/wander generated by the regenerators (equations [1] and [2]) and any jitter/wander at the input of the chain, appropriately filtered by the equivalent jitter/wander transfer characteristic. Thus, for input jitter/wander, $\theta_{in}(\omega)$, the output jitter/wander, $\theta_{out}(\omega)$, is given by

$$\begin{aligned} \Phi_{out}(\omega) = & \Phi_{i1}^R |H_1(j\omega)|^2 \frac{1 - |H_1(j\omega)|^{2y}}{1 - |H_1(j\omega)|^2} + \\ & + \Phi_{i1}^S |H_1(j\omega)|^2 \frac{|1 - H_1(j\omega)^N|^2}{|1 - H_1(j\omega)|^2} + \Phi_{in}(\omega) |H_1(j\omega)^N|^2 \end{aligned} \quad (4)$$

- ii) The jitter/wander spectrum at the output of a demultiplexer is the power sum of the unfiltered intrinsic multiplex jitter/wander and the accumulated higher rate input jitter/wander, attenuated by the desynchronizer jitter/wander transfer characteristic. Thus, if $\theta_{in,1}(\omega)$ is the unfiltered intrinsic multiplex jitter/wander and $\theta_{in,2}(\omega)$ is the accumulated higher rate input jitter/wander, the output jitter/wander, $\theta_{out}(\omega)$ is given by

$$\Phi_{out}(\omega) = \left\{ \Phi_{in,1}(\omega) + \frac{\Phi_{in,2}(\omega)}{r^2} \right\} |G(j\omega)|^2 \quad (5)$$

where r is the ratio of the multiplexer output frequency to tributary frequency, and $G(j\omega)$ represents the desynchronizer jitter/wander transfer characteristic.

¹⁾ The following equations are valid for both single- and double-sided power spectra and corresponding transfer characteristics.

4 Definition of peak-to-peak jitter/wander amplitude

The probability that the jitter/wander exceeds a particular threshold amplitude $|x|$ n times in the time interval $(t, t + \Delta t)$ may be described by a Poisson density function [3].

$$Pr\left\{n(\pm x) \text{ crossings in } (t, t + \Delta t)\right\} = \frac{\{\overline{N(x)\Delta t}\}^n}{n!} e^{-\overline{N(x)\Delta t}} \quad (6)$$

where $\overline{N(x)}$ is the average number of times/second that the threshold $|x|$ is exceeded.

For Gaussian jitter/wander, with double-sided power spectral density $\theta(\omega)$, $\overline{N(x)}$ is given by [7]

$$\begin{aligned} \overline{N(x)} &= N_0 e^{-x^2/\Omega\sigma^2} \\ \text{where } \sigma^2 &= \frac{1}{2\pi} \int_{-\infty}^{\infty} \Phi(\omega) d\omega \\ N_0 &= \frac{1}{\pi} \left\{ \frac{\int_{-\infty}^{\infty} \omega^2 \Phi(\omega) d\omega}{2\pi\sigma^2} \right\}^{1/2} \end{aligned} \quad (7)$$

The probability that the jitter/wander doesn't exceed the threshold during the time interval $(t, t + \Delta t)$ is

$$1 - P_0 = e^{-\overline{N(x)\Delta t}} \quad (8)$$

Solving for the threshold,

$$|x| = \left\{ 2\sigma^2 \ln \left[N_0 \frac{\Delta t}{\ln\left(\frac{1}{1-P_0}\right)} \right] \right\}^{1/2} \quad (9)$$

If we assume that each time the threshold is crossed, an undesirable event (impairment) may result, the mean time between impairments, MTBI, may be taken as

$$MTBI = \frac{1}{\overline{N(x)}} \quad (10)$$

Thus, equation (9) may be expressed as

$$|x| = \left\{ 2\sigma^2 \ln(N_0 MTBI) \right\}^{1/2} \quad (11)$$

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