International Telecommunication Union



Recommendation ITU-R BT.1368-9 (12/2011)

Planning criteria, including protection ratios, for digital terrestrial television services in the VHF/UHF bands

> BT Series Broadcasting service (television)



International Telecommunication

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Series	Title
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BS	Broadcasting service (sound)
BT	Broadcasting service (television)
F	Fixed service
Μ	Mobile, radiodetermination, amateur and related satellite services
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RA	Radio astronomy
RS	Remote sensing systems
S	Fixed-satellite service
SA	Space applications and meteorology
SF	Frequency sharing and coordination between fixed-satellite and fixed service systems
SM	Spectrum management
SNG	Satellite news gathering
TF	Time signals and frequency standards emissions
V	Vocabulary and related subjects

Note: This ITU-R Recommendation was approved in English under the procedure detailed in Resolution ITU-R 1.

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RECOMMENDATION ITU-R BT.1368-9

Planning criteria, including protection ratios, for digital terrestrial television services in the VHF/UHF bands

(1998-1998-2000-2002-2004-2005-2006-2007-2009-2011)

Scope

This Recommendation defines planning criteria for various methods of providing digital terrestrial television services in the VHF/UHF bands.

The ITU Radiocommunication Assembly,

considering

a) that systems have been developed for the transmission of digital terrestrial television services (DTTS) in the VHF/UHF bands;

b) that the VHF/UHF television bands are still occupied by analogue television services;

c) that the analogue television services will remain in use in some administrations for a considerable period of time;

d) that the availability of consistent sets of planning criteria agreed by administrations will facilitate the planning of digital terrestrial television services;

e) that parts of the VHF/UHF television bands are shared with other primary services;

f) that sharing between digital terrestrial television broadcasting (DTTB) and some other primary services is an evolving situation;

g) that the protection ratios established for the protection of digital terrestrial television need to be at the threshold of signal failure,

recommends

1 that the relevant protection ratios (PRs) and the relevant minimum field strength values given in Annexes 1, 2, 3 and 4 and the additional information given in Annexes 5, 6, 7 and 8 should be used as the basis for frequency planning for digital terrestrial television services.

Introduction

This Recommendation contains the following Annexes:

Annex 1 – Planning criteria for ATSC digital terrestrial television systems in the VHF/UHF bands

- Annex 2 Planning criteria for DVB-T digital terrestrial television systems in the VHF/UHF bands
- Annex 3 Planning criteria for ISDB-T digital terrestrial television systems in the VHF/UHF bands
- Annex 4 Planning criteria for DTMB digital terrestrial television systems in the VHF/UHF bands
- Annex 5 Other planning factors
- Annex 6 Subjective comparison method (SCM) with a reference interferer for assessment protection ratios for analogue television systems
- Annex 7 Failure point assessment methods

Annex 8 - Tropospheric and continuous interference

General

The RF protection ratio is the minimum value of wanted-to-unwanted signal ratio, usually expressed in decibels at the receiver input.

The reference level of the digital signal is defined as the r.m.s. value of the emitted signal power within the channel bandwidth. It should preferably be measured with a thermal power meter. Historically, protection ratio values for wanted digital signals were measured with a -60 dBm receiver input power. Where possible, protection ratios for digital TV systems are derived from measurements using a range of signal levels.

The reference level of the analogue vision-modulated signal is defined as the r.m.s. value of the vision carrier at peaks of the modulation envelope. All protection ratio values for wanted analogue signals are measured with a receiver input power of $-39 \text{ dBm} (70 \text{ dB}(\mu \text{V}) \text{ at } 75 \Omega)$.

1 Wanted digital terrestrial television systems

The protection ratios for digital terrestrial television systems apply to both continuous and tropospheric interference. The protection ratios refer to the centre frequency of the wanted digital terrestrial television system.

Because a digital television receiver needs to operate successfully in the presence of high level analogue signals on nearby channels, a high degree of receiver front-end linearity is required.

The protection ratios for digital terrestrial television systems as the interfering system are those for the case where the wanted and unwanted signals are not synchronized and/or do not have a common programme source. Results relevant to single frequency networks (SFN) are yet to be developed and simple aggregate power sum calculations taking into account transmitter sites and propagation for each transmitter in the network may be used as an initial guide.

For the digital terrestrial television system, ATSC, the protection ratios are measured for a BER = 3×10^{-6} at the input of the MPEG-2 demultiplexer.

For the digital terrestrial television systems (digital video broadcasting-terrestrial (DVB-T) and integrated service digital broadcasting-terrestrial (ISDB-T)) the protection ratios are measured between the inner and outer codes, before Reed Solomon decoding, for a BER = 2×10^{-4} ; this corresponds to a BER < 1×10^{-11} at the input of the MPEG-2 demultiplexer. For domestic receivers it may not be possible to measure the BER before Reed-Solomon decoding. The BER for such cases is under study.

For digital television terrestrial multimedia broadcasting (DTMB), the protection ratios are measured at the output of BCH, $BER = 3 \times 10^{-6}$ at the input of demultiplexer.

To reduce the number of measurements and tables, it is proposed that protection ratio measurements for DVB-T systems should preferably be made with the following three modes shown in Table 1. Protection ratio values for the different required operational modes for fixed, portable or mobile reception can be calculated from the given measured values. The tabulated scaling values for varying reception channel qualities from Gaussian, through Ricean, to Rayleigh are provided in Table 50 § 4 of Annex 2.

TABLE 1

1 1	<i></i>		
Modulation	Code rate	C/N ⁽¹⁾ (dB)	Bit rate ⁽²⁾ (Mbit/s)
QPSK	2/3	6.9	≈ 7
16-QAM	2/3	13.1	≈ 13
64-QAM	2/3	18.7	≈ 20

Proposed preferable DVB-T mode types for measurements on protection ratios

⁽¹⁾ The figures are given for a Gaussian channel (including a typical implementation margin) for a BER $< 1 \times 10^{-11}$.

⁽²⁾ For a guard interval of 1/4.

To reduce the number of measurements and tables, it is proposed that protection ratio measurements for DTMB systems should preferably be made with the following 11 modes shown in Table 2.

TABLE 2

Proposed preferable DTMB mode types for measurements on protection ratios

Modulation	Code rate	C/N ⁽¹⁾ (dB)	Bit rate ⁽²⁾ (Mbit/s)
4-QAM	0.4	2.5	5.414
16-QAM	0.4	8.0	10.829
64-QAM	0.4	14.0	16.243
4-QAM	0.6	4.5	8.122
16-QAM	0.6	11.0	16.243
64-QAM	0.6	17.0	24.365
4-QAM-NR	0.8	2.5	5.414
4-QAM	0.8	7.0	10.829
16-QAM	0.8	14.0	21.658
32-QAM	0.8	16.0	27.072
64-QAM	0.8	22.0	32.486

⁽¹⁾ The figures are given for a Gaussian channel at BCH output BER $< 3 \times 10^{-6}$.

⁽²⁾ For a guard interval of 1/9 and RF bandwidth 8 MHz.

2 Wanted analogue terrestrial television systems

Measurements of protection ratios for the vision signal of a wanted analogue terrestrial television system should preferably be made with the subjective comparison method with a sine-wave reference interferer described in Annex 6.

The values of protection ratio quoted apply to interference produced by a single source. Except where otherwise stated, the ratios apply to tropospheric, T, interference and correspond closely to a slightly annoying impairment condition. They are considered to be acceptable only if the interference occurs for a small percentage of the time, not precisely defined but generally considered to be between 1% and 10%. For substantially non-fading unwanted signals, it is necessary to provide a higher degree of protection and ratios appropriate to continuous, C, interference should be used (see Annex 8).

When the wanted signal is an analogue television signal, two or more protection ratio values should be considered, one for the protection ratio of the vision signal and others for the protection ratios of sound signals. The most stringent value should then be used.

Significantly strong wanted input signals can require higher protection ratio values because of non-linear effects in the receiver.

For 625-line systems, the reference impairment levels are those which correspond to co-channel protection ratios of 30 dB and 40 dB, when two-thirds line offset is used, see Recommendation ITU-R BT.655. These conditions approximate to impairment grades 3 (slightly annoying) and 4 (perceptible but not annoying) and apply to tropospheric, T, and continuous, C, interference, respectively.

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Planning criteria for ATSC digital television systems in the VHF/UHF bands

1 Protection ratios for ATSC wanted digital terrestrial television signals

Tables 3 to 5 and 6 to 9 show protection ratios for an ATSC digital terrestrial television signal interfered with by an ATSC digital terrestrial television signal, and by an analogue terrestrial television signal, respectively.

1.1 Protection of an ATSC digital terrestrial television signal interfered with by an ATSC digital terrestrial television signal

TABLE 3

Co-channel protection ratios (dB) for a 6 MHz ATSC signal interfered with by a 6 MHz ATSC signal at various signal-to-noise ratios (S/N)

Signal-to-noise ratio (S/N) of wanted signal (dB)	Unwanted signal protection ratio (dB)
	ATSC 6 MHz
16 dB	23
Greater than 16 dB but less than 28 dB	Use equation below ⁽¹⁾
Greater than or equal to 28 dB	15

⁽¹⁾ Protection Ratio (dB) = $15 + 10 \log_{10} \{1/(1-10^{-x/10})\}$ where x = S/N - 15.19 (minimum S/N).

TABLE 4

Protection ratios (dB) for a 6 MHz ATSC signal (wanted) interfered with by a 6 MHz ATSC signal (unwanted) in the lower (N - 1) and upper (N + 1) adjacent channels at the given wanted signal average power levels at the receiver input

	Adjacent channel protection ratio (dB)			
Type of interference	Weak wanted ATSC signal (–68 dBm)	Moderate wanted ATSC signal (-53 dBm)	Strong wanted ATSC signal (-28 dBm)	
Lower adjacent channel interference (N-1)	-28	-28	-20	
Upper adjacent channel interference (N+1)	-26	-26	-20	

The protection ratios (dB) apply to both continuous and tropospheric interference.

TABLE 5

Protection ratios (dB) for a 6 MHz ATSC signal (wanted) interfered with by a 6 MHz ATSC signal (unwanted) in multiple adjacent channels, $N \pm 2$ to $N \pm 15$, at the given wanted signal average power levels at the receiver input

	Multiple adjacent channel protection ratio (dB)		
Type of interference	Weak wanted ATSC signal (–68 dBm)	Moderate wanted ATSC signal (–53 dBm)	Strong wanted ATSC signal (-28 dBm)
N ± 2	-44	-40	-20
$N \pm 3$	-48	-40	-20
$N \pm 4$	-52	-40	-20
$N \pm 5$	-56	-42	-20
$N \pm 6$ to $N \pm 13$	-57	-45	-20
$N \pm 14$ and $N \pm 15$	-50	-45	-20

- **1.2** Protection of ATSC digital terrestrial television interfered with by analogue terrestrial television
- **1.2.1** Protection from co-channel interference

TABLE 6

Co-channel protection ratios (dB) for an ATSC 6 MHz signal interfered with by an analogue television signal

Wanted signal	Unwanted signal (Analogue TV signal including sound carriers)	
	M/NTSC	PAL B
ATSC	2 ⁽¹⁾ 7	9
ATSC with 1/2 rate concatenated trellis coding	1	3
ATSC with 1/4 rate concatenated trellis coding	-2	0

⁽¹⁾ Using a comb filter in the digital television receiver and C/N of 19 dB.

1.2.2 Protection from lower adjacent channel (N - 1) interference

TABLE 7

Protection ratios (dB) for lower adjacent channel (N-1) interference for an ATSC 6 MHz signal interfered with by an analogue television signal including sound

Wanted signal	Unwanted signal (Analogue TV signal including sound carriers)	
	M/NTSC	
ATSC	-48	

1.2.3 Protection from upper adjacent channel (N + 1) interference

TABLE 8

Protection ratios (dB) for upper adjacent channel (N + 1) interference for an ATSC 6 MHz signal interfered with by an analogue television signal

Wanted signal	Unwanted signal (Analogue TV signal including sound carriers)
	M/NTSC
ATSC	-49

1.2.4 Protection from other channel interference

TABLE 9

Protection ratios (dB) for an ATSC 6 MHz signal interfered with by an M/NTSC signal at other out-of-band channels

Wanted signal	Unwanted signal	Unwanted channels	Protection ratio
ATSC	M/NTSC	$N \pm 2$ to $N \pm 8$	-58

2 Protection ratios for wanted analogue terrestrial television signals interfered with by unwanted ATSC digital terrestrial television signals

Table 10 and Tables 11 to 13 show protection ratios for wanted 525-line and 625-line, respectively, analogue television signals interfered with by ATSC digital terrestrial television signals.

2.1 **Protection ratios for 525-line television systems**

2.1.1 Protection for vision signals interfered with by ATSC digital television

In this section the protection ratios for an analogue wanted signal interfered by an unwanted ATSC digital signal apply only to the interference to the vision and colour carriers.

TABLE 10

Unwanted digital channel	Tropospheric interference grade 3	Continuous interference grade 4
N-1 (lower)	-16	
N (co-channel)	34	
N + 1 (upper)	-17	
<i>N</i> + 14 (image)	-33	
<i>N</i> + 15 (image)	-31	
$N\pm 2$	-24	
N ± 3	-30	
$N \pm 4$	-25	
$N\pm7$	-34	
$N \pm 8$	-32	

Protection ratios (dB) for a wanted analogue vision signal (NTSC, 6 MHz) interfered with by an unwanted ATSC signal

2.2 **Protection ratios for 625-line television systems**

2.2.1 Protection of wanted vision signals interfered with by ATSC digital terrestrial television

In this section the protection ratios for an analogue wanted signal interfered by an unwanted digital signal relate only to the interference to the vision signal.

The protection ratio values given are related to an out-of-channel spectrum attenuation of the unwanted DVB-T transmitter of 40 dB.

2.2.1.1 **Protection from co-channel interference**

TABLE 11

Protection ratios (dB) for a wanted analogue vision signal interfered with by an unwanted ATSC 6 MHz signal

Wanted signal: analogue system	Unwanted signal: ATSC 6 MHz					
	Tropospheric interference	Continuous interference				
B/PAL	38	45				

2.2.1.2 Protection from lower adjacent channel interference

TABLE 12

Protection ratios (dB) for a wanted analogue vision signal interfered with by an ATSC 6 MHz signal (lower adjacent channel)

Wanted signal:	Unwanted signal: ATSC 6 MHz signal (lower adjacent channel)				
analogue system	Tropospheric interference	Continuous interference			
B/PAL	-7	-1			

2.2.1.3 **Protection from upper adjacent channel interference**

TABLE 13

Protection ratios (dB) for a wanted analogue vision signal interfered with by an ATSC 6 MHz signal (upper adjacent channel)

Wanted signal:	Unwanted signal: ATSC 6 MHz signal (upper adjacent channel)				
analogue system	Tropospheric interference	Continuous interference			
B/PAL	_7	0			

3 Protection ratios for sound signals of wanted analogue terrestrial television signals interfered with by unwanted ATSC digital terrestrial television signals

3.1 Protection for NTSC sound signals (BTSC MTS system and SAP) interfered with by an ATSC digital television signal (see Note 1)

In the case of an unwanted upper adjacent digital channel N + 1 the audio signals degrade before the vision signal. The protection ratio value for the interference into the BTSC MTS and SAP sound signals was measured with -12 dB. (Vision protection ratio for N + 1 is -17 dB.) The -12 dB sound protection ratio figure is related to the wanted NTSC vision carrier level.

NOTE 1 – BTSC MTS: broadcast television system committee multichannel television sound; SAP: sound audio programme.

4 Minimum field strengths for ATSC terrestrial digital television

TABLE 14

Derivation by the figure of merit method ATSC 6 MHz system*

Planning parameter ⁽¹⁾	Low VHF 54-88 MHz	High VHF 174-216 MHz	UHF 470-806 MHz	
Frequency (MHz)	69	194	615	
<i>C</i> / <i>N</i> (dB)	19.5 ⁽²⁾	19.5 ⁽²⁾	19.5 ⁽²⁾	
<i>k</i> (dB)	-228.6	-228.6	-228.6	
<i>B</i> (dB(Hz)) (6 MHz)	67.8	67.8	67.8	
$G_{1\mathrm{m}^2}(\mathrm{dB})$	-1.8	7.3	17.2	
G_D (dB)	6	8	10	
$G_I(\mathrm{dB})$	8.2	10.2	12.2	
Transmission line loss (dB) α_{line}	1.1	1.9	3.3	
Antenna 300/75 balun loss (dB) α _{balun}	0.5	0.5	0.5	
Receiver noise figure (dB)	5	5	10	
$T_{rx}(\mathbf{K})$	627.1	627.1	2610	
T _{line} (K)	65.0	102.9	154.4	
LNA noise figure (dB)	5	5	5	
LNA gain (dB)	20	20	20	
T_{LNA} (dB)	627.1	627.1	627.1	
$T_{balun}\left(\mathrm{K} ight)$	31.6	31.6	31.6	
$T_a(\mathbf{K})$	9972.1	569.1	Negligible	
$T_a \alpha_{balun} (\mathrm{K})$	8 8 8 5.1	507.1	Negligible	
$T_{line}/\alpha G(\mathbf{K})$	0.8	1.6	3.3	
$T_{rx}/\alpha G(\mathbf{K})$	8.1	9.7	55.8	
$T_{e}\left(\mathrm{K} ight)$	9552.6	1 1 7 6.8	717.8	
$10\log(T_e)$ (dB(K))	39.8	30.7	28.6	
G_A (dB)	7.7	9.7	11.7	
$E_{rx} (dB(\mu V/m))^{(2), (3)} (TBC)$	35	33	39	

* The values in the Table were calculated assuming *C/N* with typical multipath reception impairment and equal partitioning for noise and interference. The receiving system model is a typical receiving installation located near the edge of coverage and consists of an externally mounted antenna, a low noise amplifier (LNA) mounted at the antenna, an interconnecting downlead cable and an ATSC receiver.

⁽¹⁾ For definitions see Appendix 1 to Annex 1.

⁽²⁾ Figures should be adjusted downward (towards better performance) by 6 dB for 1/2 rate concatenated trellis coding or 9 dB for 1/4 rate concatenated trellis coding.

⁽³⁾ For formula see Appendix 1 to Annex 1.

Appendix 1 to Annex 1

Derivation by the figure of merit method

Required field strength

$$E_{rx} (dB(V/m)) = \varphi (dB(W/m^2)) + 10 \log(120 \pi)$$

$$C/N = \varphi - G_{lm}^2 + G_A/T_e - k - B_{rf}$$

$$E_{rx} (dB(\mu V/m)) = \varphi (dB(W/m^2)) + 25.8 (dB) + 120 (dB)$$

$$= 145.8 + C/N + G_{lm}^2 - G_A/T_e + 10 \log(k) + 10 \log(B_{rf})$$

- E_{rx} : required field strength at the receive system antenna
- φ : power flux-density at the receive system antenna
- C/N: carrier-to-noise ratio
- G_{lm}^2 : gain of 1 m²
- G_A/T_e : figure of merit of the receive system
 - *k*: Boltzmann's constant (J/K)
 - B_{rf} : system equivalent noise bandwidth.

Receive system figure of merit

(For receiving system model with LNA)

$$G_A/T_e = (G-L)/(\alpha_{balun} T_a + T_{balun} + T_{LNA} + T_{line}/(\alpha_{line} G_{LNA}) + T_{rx}/(\alpha_{line} G_{LNA}))$$

Receiver noise temperature

$$T_{rx} = (10^{NF/10} - 1) \times 290^{\circ}$$

LNA noise temperature

$$T_{LNA} = (10^{NF/10} - 1) \times 290^{\circ}$$

Transmission line noise temperature

$$T_{line} = (1 - \alpha_{line}) \times 290^{\circ}$$

Balun noise temperature

$$T_{balun} = (1 - \alpha_{balun}) \times 290^{\circ}$$

Antenna noise temperature

$$T_a = 10^{(6.63 - 2.77(\log f))} \times 290^{\circ}$$
 (for dipole antenna)

where *f* is expressed in MHz.

Antenna noise temperature (referred to LNA input)

$$\alpha T_a = T_a(\alpha_{balun})$$

System noise temperature

$$T_{e} = (\alpha_{balun} T_{a} + T_{balun} + T_{LNA} + T_{line} / (\alpha_{line} G_{LNA}) + T_{rx} / (\alpha_{line} G_{LNA}))$$

$$T_{e} (dB(K)) = 10 \log(\alpha_{balun} T_{a} + T_{balun} + T_{LNA} + T_{line} / (\alpha_{line} G_{LNA}) + T_{rx} / (\alpha_{line} G_{LNA}))$$

$$= 10 \log(T_{balun} + T_{LNA} + T_{line} / (\alpha_{line} G_{LNA}) + T_{rx} / (\alpha_{line} G_{LNA})) + N_{ext}$$

when T_a is not known.

Gain of $1 m^2$

$$G_{1m}^2 = 10 \log(4 \pi / \lambda \lambda^2)$$

Data

 G_I : antenna gain (isotropic) (dB)

L: transmission line loss (dB)

 α_{line} : transmission line loss (numeric ratio)

 T_a : antenna noise temperature (K)

- T_{rx} : receiver noise temperature (K)
- n_f : noise factor (numeric ratio)
- *NF*: noise figure (dB)
- T_0 : reference temperature = 290 K
- λ : wavelength of frequency of operation
- G_A : system gain (dB)
- T_e : system noise temperature (K)
- N_{ext} : dB value representing the contribution due to external noise
 - *k*: Boltzmann's constant 1.38×10^{-23} (-228.6 dB) (J/K)
 - *B*: system equivalent noise bandwidth (dB(Hz))
- α_{balun} : antenna 300/75 Balun loss (numeric ratio)
- LNA: low noise amplifier
- T_{LNA} : LNA noise temperature (K)

Annex 2

Planning criteria for DVB-T digital television systems in the VHF/UHF bands

1 Protection ratios for DVB-T wanted digital terrestrial television signals

Tables 15 to 17, 19 to 25, 26 to 28 and 29 to 30 show protection ratios for the DVB-T wanted digital terrestrial television signals interfered with:

- by DVB-T digital terrestrial television signals,
- by analogue terrestrial television signals,
- by a single continuous wave (CW) or FM carrier,
- by terrestrial digital audio broadcasting (T-DAB) signals, respectively.

or

1.1 Protection of a DVB-T digital terrestrial television signal interfered with by a digital terrestrial television signal

TABLE 15

Modulation	Code rate	Gaussian channel	Rice channel	Rayleigh channel
QPSK	1/2	5	6	8
QPSK	2/3	7	8	11
16-QAM	1/2	10	11	13
16-QAM	2/3	13	14	16
16-QAM	3/4	14	15	18
64-QAM	1/2	16	17	19
64-QAM	2/3	19	20	23
64-QAM	3/4	20	21	25

Co-channel protection ratios (dB) for a DVB-T signal interfered with by a DVB-T signal

Protection ratios are given for three types of propagation channels (i.e. Gaussian, Ricean and Rayleigh). For fixed and portable reception, the values relevant to the Ricean and Rayleigh channels, respectively, should be adopted.

The same protection ratios should be applied for DVB-T systems with 6, 7 and 8 MHz bandwidth.

Protection ratios are rounded to the nearest integer.

For overlapping channel, in absence of measurement information, and if the overlapping bandwidth between the wanted and unwanted signals is less than 1 MHz, the protection ratio, *PR*, should be extrapolated from the co-channel ratio figure as follows:

$$PR = CCI + 10 \log_{10}(BO/BW)$$

where:

CCI: co-channel protection ratio

BO: bandwidth (MHz) in which the two DVB-T signals are overlapping

BW: bandwidth (MHz) of the wanted signal

PR = -30 dB should be used when the above formula gives PR < -30 dB.

However, further studies are needed on this subject.

TABLE 16

DVB-T system variant	PR, dB
QPSK1/2	6
QPSK 2/3	8
QPSK 1/4	9.3
QPSK 5/6	10.5
QPSK 7/8	11.5
16-QAM 1/2	11
16-QAM 2/3	14
16-QAM 3/4	15
16-QAM 5/6	16.9
16-QAM 7/8	17.5
64-QAM 1/2	17
64-QAM 2/3	20
64-QAM 3/4	21
64-QAM 5/6	23.3
64-QAM 7/8	24.3

Co-channel protection ratios (dB) for a DVB-T signal interfered with by a DTMB signal for the case of fixed reception

The treatment of overlapping and adjacent channel cases DVB-T vis-à-vis DTMB is based on Recommendation ITU-R BT.1368-6 with correction to the measurements. The protection ratios for the adjacent channels in Table 18 are used.

For overlapping channel the protection ratio, PR, should be extrapolated from the co-channel ratio figure as follows:

$$PR = CCI + 10 \log_{10}((0.855784 * BO + 1.153725)/BW)$$

where:

CCI: co-channel protection ratio

BO: bandwidth (MHz) in which the DVB-T and DTMB signals are overlapping

BW: bandwidth (MHz) of the wanted DVB-T signal

PR = -30 dB should be used when the above formula gives PR < -30 dB.

NOTE – This formula is not valid for adjacent channel protection ratio (< 0.1 MHz overlap).

TABLE 17

Δf MHz	PR, dB (90 th percentile)	O _{th} , dBm (10 th percentile)
-80	-54	-4.4
-72	-53	-4.7
-64	-52	-5.6
-56	-51	-5.0
-48	-51	-8.5
-40	-50	-8.5
-32	-49	-9.0
-24	-47	-10.5
-16	-43	-10.4
-8	-30	NR
8	-30	NR
16	-42	-10.7
24	-45	-22.6
32	-49	-12.7
40	-49	-10.6
48	-50	-8.8
56	-51	-8.6
64	-51	-3.1
72	-40	-3.8
80	-53	-3.0

Protection ratios (dB) and overload thresholds (dBm) for an 8 MHz 64-QAM code rate 2/3 DVB-T signal interfered with by an 8 MHz DVB-T signal in the adjacent channels and beyond (see Notes 1 to 6)

NOTE 1 – The 90th percentile for the protection ratio value corresponds to the protection of 90% of receivers measured, with respect to the given frequency offset and parameter; whereas the 10^{th} percentile for the overload threshold should be used to protect 90% of receivers measured.

NOTE $2 - \Delta f$ is the difference between the centre frequency of the unwanted channel and the centre frequency of the wanted channel.

NOTE 3 – NR: O_{th} is not reached. That is at this frequency offset PR is the predominant criterion. Consequently, DVB-T receiver is interfered with by the interfering signal due to insufficient C/I (<PR) before reaching its O_{th} .

NOTE 4 – PR is applicable unless the interfering signal level is above the corresponding O_{th} . If the interfering signal level is above the corresponding O_{th} , the receiver is interfered with by the interfering signal whatever the signal to interference ratio is.

NOTE 5 – At wanted signal level close to receiver sensitivity, noise should be taken into account, e.g. at sensitivity +3 dB, 3 dB should be added to the PR.

NOTE 6 – PR for different system variants and various reception conditions can be obtained using the correction factors in Table 50 in § 4 of this Annex. The overload threshold is assumed to be independent of system variant and reception conditions.

The protection ratio is given in dB and applies to both continuous and tropospheric interference.

The values given apply to the case where wanted and unwanted DVB-T signals have the same channel width. Other combinations of channel width need further studies.

TABLE 18

Protection ratios (dB) for a DVB-T 64 QAM code rate 2/3 signal interfered with by a DTMB signal in the lower (N - 1) and upper (N + 1) adjacent channels

Reception mode (Note 1)	Channel				
	N – 1	N + 1			
FX	-30	-30			

NOTE 1 – PR for different system variants and various reception conditions of the wanted DVB-T signal can be obtained using the correction factors in Table 50 in § 4 of this Annex.

1.2 Protection of DVB-T digital terrestrial television interfered with by analogue terrestrial television

1.2.1 Protection from co-channel interference

TABLE 19

Co-channel protection ratios (dB) for DVB-T 7 MHz and 8 MHz signals interfered with by analogue television (non-controlled frequency condition) signals

Modulation	Code rate	Gaussian channel	Rice channel	Rayleigh channel
QPSK	1/2	-12		-12
QPSK	2/3	-8		-8
QPSK	3/4	-4		
QPSK	5/6	3		
QPSK	7/8	9		
16-QAM	1/2	-8		-8
16-QAM	2/3	-3		3
16-QAM	3/4	0		5
16-QAM	5/6	9		
16-QAM	7/8	16		
64-QAM	1/2	-3		3
64-QAM	2/3	3		6
64-QAM	3/4	9		15
64-QAM	5/6	15		
64-QAM	7/8	20		

NOTE 1 – The PAL/SECAM values are valid for the following sound carrier modes:

- MONO FM with a single sound carrier at -10 dB referred to the vision carrier;
- DUAL FM and FM + NICAM with two sound carriers at -13 dB and -20 dB level;
- AM + NICAM with two sound carriers at respectively -10 dB and -27 dB level.

According to the available measurements, the same protection ratio values are applicable for 2k and 8k modes.

In all Tables except Table 28, the so-called non-controlled conditions are used.

Actual measurements of protection ratio values will reflect the cyclic variation that occurs when the offset between a wanted DVB-T signal and an unwanted analogue signal is varied over a frequency range equivalent to the spacing between carriers of coded orthogonal frequency division multiplex (COFDM) systems. The protection ratios given represent a conservative, but realistic, value that covers the expected offset performance of existing receivers. The adoption of fine offset between COFDM signals and interfering analogue TV signals will permit the achievement of up to 3 dB improvement in protection ratio. The required transmitter frequency stability is similar to that of analogue precision offset, that means a range of some ± 1 Hz.

Protection ratios for DVB-T 6 MHz are missing due to lack of measurement results.

1.2.2 Protection from lower adjacent channel (N - 1) interference

TABLE 20

Protection ratios (dB) for lower adjacent channel (N – 1) interference for DVB-T 7 MHz and 8 MHz signals interfered with by analogue television signals including sound

Wanted	signal	Unwanted signal							
Constellation	Code rate	PAL B	ALB PALG, B1 PALI PALD, K SECAML SECAM						
QPSK	1/2		-44						
QPSK	2/3	-44	-44						
16-QAM	1/2		-43	-43					
16-QAM	2/3	-42	-42						
16-QAM	3/4		-38						
64-QAM	1/2		-40	-38					
64-QAM	2/3	-35	-35	-34		-35	-37		
64-QAM	3/4		-32						

All values applicable for fixed and portable reception conditions.

1.2.3 Protection from upper adjacent channel (N + 1) interference

TABLE 21

Protection ratios (dB) for upper adjacent channel (N + 1) interference for DVB-T 7 MHz and 8 MHz signals interfered with by an analogue television signal

Wante	d signal	Unwanted signal
Constellation	Code rate	PAL/SECAM
QPSK	2/3	-47
16-QAM	2/3	-43
64-QAM	2/3	-38

1.2.4 Protection from overlapping channel interference

TABLE 22

Protection ratios (dB) for a DVB-T 8 MHz signal interfered with by an overlapping PAL B signal including sound

Unwanted signal: PAL B analogue TV system	Wanted signal: DVB-T, 8 MHz, 64-QAM, code rate 2/3												
Δf (MHz)	-9.75	-9.25	-8.75	-8.25	-6.75	-3.95	-3.75	-2.75	-0.75	2.25	3.25	4.75	5.25
PR	-37	-14	-8	-4	-2	1	3	3	3	2	-1	-29	-36

The frequency difference Δf is the vision carrier frequency of the analogue television signal minus the centre frequency of the DVB-T signal.

TABLE 23

Protection ratios (dB) for a DVB-T 7 MHz signal interfered with by an overlapping 7 MHz analogue TV signal including sound

Unwanted signal: 7 MHz analogue TV system		Wanted signal: DVB-T, 7 MHz, 64-QAM, code rate 2/3												
$\Delta f(\text{MHz})$	-9.25	-8.75	-8.25	-7.75	-6.25	-3.45	-3.25	-2.25	-1.25	0	1.75	2.75	4.25	4.75
PR	-35	-12	-11	-5	-3	-1	4	1	0	2	-5	-5	-36	-38

The frequency difference Δf is the vision carrier frequency of the analogue television signal minus the centre frequency of the DVB-T signal.

TABLE 24

Protection ratios (dB) for a DVB-T 7 MHz signal interfered with by an overlapping 8 MHz analogue TV signal including sound

Unwanted signal: 8 MHz analogue TV system	Wanted signal: DVB-T, 7 MHz, 64-QAM, code rate 2/3													
$\Delta f(\text{MHz})$	-10.25	-9.75	-9.25	-8.75	-7.25	-3.45	-3.25	-2.25	-1.25	0	1.75	2.75	4.25	4.75
PR	-35	-12	-11	-5	-3	-1	4	1	0	2	-5	-5	-36	-38

The frequency difference Δf is the vision carrier frequency of the analogue television signal minus the centre frequency of the DVB-T signal.

TABLE 25

Protection ratios (dB) for a DVB-T 8 MHz signal interfered with by an overlapping 8 MHz analogue TV signal including sound

Unwanted signal: 8 MHz analogue TV system	Wanted signal: DVB-T, 8 MHz, 64-QAM, code rate 2/3													
$\Delta f(MHz)$	-10.75	-10.25	-9.75	-9.25	-7.75	-3.45	-3.25	-2.25	-1.25	0	2.25	3.25	4.75	5.25
PR	-35	-12	-11	-5	-3	-1	4	1	0	2	-5	-5	-36	-38

The frequency difference Δf is the vision carrier frequency of the analogue television signal minus the centre frequency of the DVB-T signal.

1.3 Protection of DVB-T digital terrestrial television signal from CW or FM signals

TABLE 26

Co-channel protection ratios (dB) for a DVB-T 8 MHz 64-QAM code rate 2/3 signal interfered with by a CW or a FM carrier (non-controlled frequency offset)

Unwanted signal: CW or FM carrier	Wanted signal: DVB-T, 8 MHz, 64-QAM, code rate 2/3						
Δf (MHz)	-12	-4.5	-3.9	0	3.9	4.5	12
PR	-38	-33	-3	-3	-3	-33	-38

TABLE 27

Co-channel protection ratios (dB) for a DVB-T 7 MHz 64-QAM code rate 2/3 signal interfered with by a CW or an FM carrier (non-controlled frequency offset)

Unwanted signal: CW or FM carrier	Wanted signal: DVB-T, 7 MHz, 64-QAM, code rate 2/3						
Δf (MHz)	-10.5	-4.0	-3.4	0	3.4	4.0	10.5
PR	-38	-33	-3	-3	-3	-33	-38

The given protection ratio Tables can be used for interfering signals with narrow bandwidth e.g. analogue sound carriers or non-broadcast services.

TABLE 28

Co-channel protection ratios (dB) for a DVB-T 7 MHz 64-QAM code rate 2/3 signal interfered with by a CW carrier (controlled frequency offset)

Unwanted signal: CW carrier	Wanted signal: DVB-T, 7 MHz, 64-QAM, code rate 2/3						I,
Δf (MHz)	-8	-4	-3	0	3	4	8
PR	-48	-41	-8	-9	-6	-39	-48

The given protection ratio Tables can be used for interfering signals with narrow bandwidth e.g. analogue sound carriers or non-broadcast services. It should be noted that the fine structure of the protection ratio versus frequency offset between the OFDM signal and the interfering CW signal exhibits a cyclic variation. The values shown in Table 28 are for the optimum offset.

1.4 Protection of DVB-T digital terrestrial television signals from T-DAB signals

TABLE 29

Co-channel protection ratios (dB) for a DVB-T 7 MHz and 8 MHz signal interfered with by four T-DAB frequency block signals

Wanted sig	Wanted signal DVB-T					
Constellation	Code rate					
QPSK	1/2	10				
QPSK	2/3	12				
QPSK	3/4	14				
16-QAM	1/2	15				
16-QAM	2/3	18				
16-QAM	3/4	20				
64-QAM	1/2	20				

Wanted sig	Wanted signal DVB-T			
Constellation	Code rate			
64-QAM	2/3	24		
64-QAM	3/4	26		
64-QAM	7/8	31		

TABLE 29	(end)
----------	-------

NOTE 1 – The given protection ratios for DVB-T signals represent the worst case of interference from T-DAB (These values are derived from measurements using four T-DAB frequency blocks with equal power levels).

TABLE 29bis

Co-channel protection ratios (dB) for a DVB-T 7 MHz interfered with by fewer than four T-DAB frequency block signals within a 7 MHz channel

Wanted sigr	nal DVB-T	PR (Note 1)				
Constellation	Code rate	1 T-DAB 2 T-DAB 3 T-DA				
64-QAM	2/3	13	21	23		
64-QAM	3/4	17	23	25		

NOTE 1 – These values were derived from measurements in a Gaussian channel. (The measured Subjective Failure Point (SFP) values were increased by 1 dB and rounding up to the nearest integer to derive QEF values). For planning situations involving Ricean channels a further 0.6 dB increase should be applied to these values.

TABLE 30

Protection ratios (dB) for a DVB-T 7 MHz and 8 MHz signal interfered with by a T-DAB signal in the lower (N - 1) or upper (N + 1) adjacent channels

Channel	N-1	N + 1
PR	-30	-30

The protection ratio is given in dB.

1.5 Protection of DVB-T from wideband signals other than terrestrial broadcasting

1.5.1 Protection ratios for DVB-T interfered with by the fixed service (relocatable system)

TABLE 31

Protection ratios for DVB-T 8 MHz 64-QAM code rate 2/3 signal interfered with by emissions of the fixed service

$\Delta f(MHz)$	-12	-4.5	-3.75	0	3.75	4.5	12
PR (dB)	-45	-27	1	4	1	-27	-45

 Δf : difference between the centre frequencies.

Technical characteristics of the interferer

- Modulation 2-FSK
- Bandwidth: 750 kHz (3 dB)

1.5.2 Protection ratios for DVB-T interfered with by code-division multiple access (CDMA)

It should be noted that the Tables 32 and 33 refer to the situation where one single channel of the CDMA system is interfering with DVB-T.

TABLE 32

Protection ratios for DVB-T 8 MHz 64-QAM code rate 2/3 signal interfered with by emissions of CDMA-1X

$\Delta f(MHz)$	-12	-4.5	-3.75	0	3.75	4.5	12
PR (dB)	-38	-20	-3	10	-3	-20	-38

 Δf : difference between the centre frequencies.

Characteristics of the interfering signal

- Modulation: QPSK
- Bandwidth: 1.25 MHz (99%)

TABLE 33

Protection ratios for DVB-T 8 MHz 64-QAM code rate 2/3 signal interfered with by emissions of CDMA-3X

$\Delta f(MHz)$	-12	-4.5	-3.75	0	3.75	4.5	12
PR (dB)	-38	8	13	18	13	8	-38

 Δf : difference between the centre frequencies.

Characteristics of the interfering signal

- Modulation: QPSK
- Bandwidth: 4 MHz (99%)

The following section provides protection ratios and overload thresholds for DVB-T systems interfered with by UMTS W-CDMA FDD systems. All measurements to derive these parameters were performed on DVB-T receivers designed for a frequency tuning range from 470 to 862 MHz, all interfering signals were within the frequency range 759 to 862 MHz.

The protection ratio and overload threshold can be significantly different for silicon tuners¹ and can tuners². Silicon tuners are increasingly being used in TV receiver equipment including high-end products such as iDTVs and PVRs.

As silicon and can tuners have different performance characteristics, planners are advised to consider the relative usage volumes of each tuner type and the difference in characteristics during network planning. Compared to can tuners, silicon tuners do not suffer from degradations in PR and O_{th} when the interferer is at the 36 MHz IF frequency or at the 2/IF = 72 MHz image frequency, however some have higher protection ratios at other interferer offsets.

It is likely that a mixture of these types of tuners will exist and their proportion is likely to change with time. This Recommendation provides separate results for each type of tuners. (For further information the technical explanation of the differences can be found in Report "Measurement of protection ratios and overload threshold for TV receivers".)

If the actual distribution is not known the administrations might have to make a choice between the values.

If the actual distribution is known, e.g. X% for can tuners and Y% for silicon tuners, a possible way of weighting the figures would be to apply the following equation for each parameter (protection ratio or overload threshold):

Combined Parameter = $(X\% / 100) / (\text{can tuners parameter}) + (Y\% / 100) / (\text{silicon tuners parameter})^3$

The highest level of protection (to protect both types of tuner) is achieved by taking the higher value for the protection ratio and the lower value for the overload threshold.

The characteristics of the UMTS (W-CDMA FDD) signal used in the measurements are given in Report "Measurement of protection ratios and overload threshold for TV Receivers".

This section includes the case of TPC On (transmit power control) used at the user equipment.

Using statistical analysis the 50^{th} and 90^{th} percentile of all measured protection ratios and the 10^{th} and 50^{th} percentile of all measured overload thresholds for UMTS interference into DVB-T were calculated. They are listed in Table 34 and Table 35 for the interfering UMTS base station signal and the UMTS user equipment signal respectively. The PR and O_{th} for the UMTS user equipment signal are relative to the interfering signal maximum r.m.s. The frequency offset is measured between the centre frequencies of wanted and interfering signals.

The 90th (respectively 50th) percentile for the protection ratio value corresponds to the protection of 90% (respectively 50%) of receivers measured.

¹ "Silicon" tuners are IC-based tuners integrating all tuner circuitry into a small package directly to be fitted onto main boards. The tuned circuits may be completely absent or can be integrated onto the silicon. The silicon chip may be protected from external electromagnetic interference by a metallic cover. When integrated onto the silicon there is a compromise in performance when compared with discrete classical layouts. The units measured represent an early generation on the market. This technology is still developing.

² "Can" tuners are classical super heterodyne tuners housed in a metal enclosure containing discrete components. Classically, there are fixed and tuneable circuits made up from discrete inductors and transistors usually with varactor diode frequency control. The metal enclosure should minimize RF interference and eliminate crosstalk and stray radiation.

³ The values X% and Y% are in the range of 0 to 100 and their sum is equal to 100.

The 10th (respectively 50th) percentile for the overload threshold value corresponds to the protection of 90% (respectively 50%) of receivers measured.

TABLE 34

Protection ratios (PR) and overload thresholds (O_{th}) for DVB-T 8 MHz 64-QAM code rate 2/3 signal interfered with by emissions of 5 MHz UMTS base station without transmit power control (TPC Off) (see Notes 1 to 4)

Number of Rx		Can	tuner			Silicor	n tuner	
Number of Kx		14			(No	(Note 5)		
Interferer offset N/(MHz)	PR, dB 50 th percentile	PR, dB 90 th percentile	O _{th} , dBm 10 th percentile	O _{th} , dB 50 th percentile	PR, dB 50 th percentile	PR, dB 90 th percentile	O _{th} , dBm 10 th percentile	O _{th} , dBm 50 th percentile
0/(0 MHz)	17.0	18.1	NR	NR				
1/(6.5 MHz)	-32.0	-30.3	-12.4	-8.0				
2/(11.5 MHz)	-43.5	-38.3	-7.7	-3.0				
3/(16.5 MHz)	-44.0	-33.7	-7.8	0.0				
4/(21.5 MHz)	-50.5	-34.9	-13.2	-1.0				
5/(26.5 MHz)	-56.0	-41.9	-15.1	-5.0				
6/(31.5 MHz)	-60.0	-43.8	-13.8	-5.5				
7/(36.5 MHz)	-45.0	-18.1	-23.9	-9.5				
8/(41.5 MHz)	-67.5	-55.1	-12.1	-2.0				
9/(46.5 MHz)	-65.0	-55.5	-12.4	-0.5				
10/(51.5 MHz)	-68.0	-57.2	-12.7	0.0				
11/(56.5 MHz)	-69.5	-60.0	-12.0	0.5				
14/(71.5 MHz)	-50.5	-41.6	-12.8	2.5				

NOTE 1 - NR: O_{th} is not reached. That is at this frequency offset PR is the predominant criterion. Consequently, DVB-T receiver is interfered with by the interfering signal due to insufficient C/I (<PR) before reaching its O_{th}.

NOTE 2 – PR is applicable unless the interfering signal level is above the corresponding O_{th} . If the interfering signal level is above the corresponding O_{th} , the receiver is interfered with by the interfering signal whatever the signal to interference ratio is.

NOTE 3 – At wanted signal level close to receiver sensitivity, noise should be taken into account, e.g. at sensitivity +3 dB, 3 dB should be added to the PR.

NOTE 4 – PR for different system variants and various reception conditions can be obtained using the correction factors in Table 50 in § 4 of this Annex. The overload threshold is assumed to be independent of system variant and reception conditions.

NOTE 5 – Silicon tuners may have a significant difference. A limited number of three silicon tuners has been tested. Therefore no valid statistics can be provided. The values can be found in Table 62 in Appendix 2 to Annex 2 as a guidance and should be used carefully.

Protection ratios (PR) and overload thresholds for DVB-T 8 MHz 64-QAM code rate 2/3 signal interfered with by emissions of 5 MHz UMTS user equipment with transmit power control (TPC on) (see Notes 1 to 5)

		Can tuner				Silicor	n tuner	
Number of Rx		14				No	te 6	
Interferer offset N/(MHz)	PR, dB 50 th percentile	PR, dB 90 th percentile	O _{th} , dBm 10 th percentile	O _{th} , dB 50 th percentile	PR, dB 50 th percentile	PR, dB 90 th percentile	O _{th} , dBm 10 th percentile	O _{th} , dB 50 th percentile
0/(0 MHz)	18.0	19.0	NR	NR				
1/(6.5 MHz)	-18.0	-16.0	-33.8	-13.0				
2/(11.5 MHz)	-37.0	-25.6	-24.7	-4.0				
3/(16.5 MHz)	-42.5	-30.6	-6.8	0.0				
4/(21.5 MHz)	-42.0	-35.9	-13.0	0.0				
5/(26.5 MHz)	-49.5	-37.3	-15.5	-0.5				
6/(31.5 MHz)	-57.5	-41.1	-8.7	-2.5				
7/(36.5 MHz)	-47.0	-18.2	-24.0	-12.0				
8/(41.5 MHz)	-68.0	-53.6	-9.0	0.0				
9/(46.5 MHz)	-66.5	-55.3	-9.0	0.5				
10/(51.5 MHz)	-71.0	-57.6	-9.7	1.5				
11/(56.5 MHz)	-72.0	-58.6	-9.1	1.5				
14/(71.5 MHz)	-50.0	-43.2	-9.5	3.0				

NOTE 1 – NR: O_{th} is not reached. That is at this frequency offset PR is the predominant criterion. Consequently, DVB-T receiver is interfered with by the interfering signal due to insufficient C/I (<PR) before reaching its O_{th} .

NOTE 2 – PR is applicable unless the interfering signal level is above the corresponding O_{th} . If the interfering signal level is above the corresponding O_{th} , the receiver is interfered with by the interfering signal whatever the signal to interference ratio is.

NOTE 3 – At wanted signal level close to receiver sensitivity, noise should be taken into account, e.g. at sensitivity +3 dB, 3 dB should be added to the PR.

NOTE 4 - PR for different system variants and various reception conditions can be obtained using the correction factors in Table 50 in § 4 of this Annex. The overload threshold is assumed to be independent of system variant and reception conditions.

NOTE 5 – DVB-T PR and O_{th} relative to the interfering signal maximum r.m.s. power is applicable to sharing studies when the interfering UMTS user equipment signal power is taken fixed to its maximum value.

NOTE 6 – Silicon tuners may have a significant difference. A limited number of three silicon tuners has been tested. Therefore no valid statistics can be provided. The values can be found in Table AA1 in Appendix 2 to Annex 2 as a guidance and should be used carefully.

1.5.3 Protection ratios and overload thresholds for DVB-T interfered with by LTE OFDMA and SC-FDMA signals

This section provides protection ratios and overload thresholds for DVB-T systems interfered with by LTE OFDMA and SC-FDMA system. All measurements to derive these parameters were performed on DVB-T receivers designed for a frequency tuning range from 470 to 862 MHz, all interfering signals were within the frequency range 759 to 862 MHz.

The protection ratio and overload threshold can be significantly different for silicon tuners¹ and can tuners². Silicon tuners are increasingly being used in TV receiver equipment including high-end products such as iDTVs and PVRs.

As silicon and can tuners have different performance characteristics, planners are advised to consider the relative usage volumes of each tuner type and the difference in characteristics during network planning. Compared to can tuners, silicon tuners do not suffer from degradations in PR and O_{th} when the interferer is at the 36 MHz IF frequency or at the 2 IF = 72 MHz image frequency, however some have higher protection ratios at other interferer offsets.

It is likely that a mixture of these types of tuners will exist and their proportion is likely to change with time. This Recommendation provides separate results for each type of tuners. (For further information the technical explanation of the differences can be found in Report "Measurement of protection ratios and overload threshold for TV receivers".)

If the actual distribution is not known the administrations might have to make a choice between the values.

If the actual distribution is known, e.g. X% for can tuners and Y% for silicon tuners, a possible way of weighting the figures would be to apply the following equation for each parameter (protection ratio or overload threshold):

Combined parameter = (X% / 100) (can tuners parameter) + (Y% / 100) (silicon tuners parameter)³

The highest level of protection (to protect both types of tuner) is achieved by taking the higher value for the protection ratio and the lower value for the overload threshold.

The characteristics of the LTE signal used in the measurements are given in Report "Measurement of protection ratios and overload threshold for TV receivers".

Using statistical analysis the 50^{th} and 90^{th} percentile of all measured protection ratios and the 10^{th} and 50^{th} percentile of all measured overload thresholds for LTE interference into DVB-T were calculated.

The 90th (respectively 50th) percentile for the protection ratio value corresponds to the protection of 90% (respectively 50%) of receivers measured.

The 10th (respectively 50th) percentile for the overload threshold value corresponds to the protection of 90% (respectively 50%) of receivers measured.

The sharing between DVB-T and the mobile LTE service is an evolving situation. The design of both the television tuners and the implementation of base stations are evolving in both cases. All parties involved are actively encouraged to improve the performance of their respective equipment so that these tables can be revisited in the near future.

The range of protection ratios and overload thresholds obtained for LTE-BS interferer is listed in Table 36 for can tuners and Table 37 for silicon tuners for the BS traffic load range of 0% to $100\%^4$.

For the case of 0% and the 50% BS traffic load the figures in the following tables have been derived from a limited number of measurements (6 silicon tuners). Administrations are invited to provide additional measurements in order to improve statistical accuracy. Therefore the values are for guidance and should be used carefully.

⁴ The term 0% traffic loading on an LTE BS refers to the situation where the base station is not handling any user traffic but is still transmitting signalling, synchronisation and possibly occasional broadcast data. Experiments showed that two out of the four TV receivers tested suffered degraded protection ratios when the BS traffic loading was between 0% and 30%.

The current worst-case situation corresponds to very low traffic load on the base station. All situations of traffic load are provided here as the actual traffic load in the real BS operation is unlikely to be predictable.

The highest level of protection (to protect broadcasting for all BS traffic load cases) is achieved by taking the highest value for the protection ratio and the lowest value for the overload threshold.

The protection ratios for interference signals with 0% traffic load were generally higher than those for higher traffic load. The overload threshold for interference signals with 0% traffic load were generally lower than those for higher traffic load. For further explanation see Report "Measurement of protection ratios and overload threshold for TV receivers".

The frequency offset is measured between the centre frequencies of wanted and interfering signals.

TABLE 36

PR values at the 50th and 90th percentile and O_{th} values at the 10th and 50th percentile for a 8 MHz DVB-T 64-QAM with code rate 2/3 signal interfered with by a 10 MHz LTE BS signal in a Gaussian channel environment for can tuners (see Notes 1 to 5)

Interferer offset N/(MHz)	PR, dB 50 th percentile	PR, dB 90 th percentile	O _{th} , dBm 10 th percentile	O _{th} , dB 50 th percentile
1/(10 MHz)	-39 TBD	-33 TBD	TBD –13	TBD –9
2/(18 MHz)	-46 TBD	-42 TBD	TBD8	TBD –3
3/(26 MHz)	-49 TBD	-39 TBD	TBD –18	TBD –2
4/(34 MHz)	-58 TBD	-55 TBD	TBD –13	TBD8
5/(42 MHz)	−64 TBD	-63 TBD	TBD8	TBD –4
6/(50 MHz)	−59 TBD	-58 TBD	TBD5	TBD1
7/(58 MHz)	−67 TBD	-66 TBD	TBD5	TBD 1
8/(66 MHz)	-68 TBD	−65 TBD	TBD –5	TBD 1
9/(74 MHz)	-46 TBD	−39 TBD	TBD3	TBD 2

NOTE 1 - PR is applicable unless the interfering signal level is above the corresponding O_{th} . If the interfering signal level is above the corresponding O_{th} , the receiver is interfered with by the interfering signal whatever the signal to interference ratio is.

NOTE 2 – At wanted signal level close to receiver sensitivity, noise should be taken into account, e.g. at sensitivity +3 dB, 3 dB should be added to the PR.

NOTE 3 - PR for different system variants and various reception conditions can be obtained using the correction factors in Table 50 in § 4 of this Annex. The overload threshold is assumed to be independent of system variant and reception conditions.

NOTE 4 – TBD: to be determined. A limited number of can-tuners (two) has been tested for the cases of 0% and 50% BS traffic load. Therefore no valid statistics can be provided. The values can be found in Tables 65 and 67 in Appendix 2 to Annex 2 as a guidance and should be used carefully.

NOTE 5 – For further detail on the different BS traffic load case see 64, 66; 68 in Appendix 2 to Annex 2.

Interferer offset N/(MHz)	PR, dB 50 th percentile	PR, dB 90 th percentile	O _{th} , dBm 10 th percentile	O _{th} , dB 50 th percentile
1/(10 MHz)	-4030.5 ⁽¹⁾	-39.520.5 ⁽¹⁾	$-40.8^{(1)}\dots -10$	$-38^{(1)}\dots -2.5$
2/(18 MHz)	-5127.5 ⁽¹⁾	-4621.5 ⁽¹⁾	$-35.5^{(1)}\ldots -8$	$-6^{(1)} \dots 1$
3/(26 MHz)	$-52 \dots -30^{(1)}$	$-47 \dots -24.5^{(1)}$	$-39^{(1)}\dots -6$	$-4.5^{(1)}\dots 2.5$
4/(34 MHz)	$-54.5 \dots -32^{(1)}$	$-48 \dots -28.5^{(1)}$	$-32.5^{(1)}\dots -9.5$	$-4.5^{(1)}\dots 4$
5/(42 MHz)	$-55 \dots -37^{(1)}$	$-49.5 \dots -32^{(1)}$	$-31.5^{(1)}\dots -9$	$-3^{(1)} \dots 5$
6/(50 MHz)	-56.544.5 ⁽¹⁾	$-50 \dots -35^{(1)}$	$-29^{(1)} \dots -8.5$	$-2^{(1)} \dots 4.5$
7/(58 MHz)	$-56.5 \dots -52^{(1)}$	$-52 \dots -37^{(1)}$	$-28^{(1)} \dots -8$	$-1^{(1)} \dots 5$
8/(66 MHz)	$-56.5 \dots -53^{(1)}$	$-52.5 \dots -38.5^{(1)}$	$-26^{(1)}\dots -7$	$-1.5^{(1)}5.5$
9/(74 MHz)	$-56.5 \dots -53^{(1)}$	$-53 \dots -40^{(1)}$	-25 ⁽¹⁾ 6	$-1.5^{(1)}\dots 5.5$

PR values at the 50th and 90th percentile and O_{th} values at the 10th and 50th percentile for a 8 MHz DVB-T 64-QAM with code rate 2/3 signal interfered with by a 10 MHz LTE BS signal in a Gaussian channel environment for silicon tuners (see Notes 1 to 4)

⁽¹⁾ The value is for the 0% BS traffic load case and is based on a limited number of measurements (6 tuners).

NOTE 1 – PR is applicable unless the interfering signal level is above the corresponding O_{th} . If the interfering signal level is above the corresponding O_{th} , the receiver is interfered with by the interfering signal whatever the signal to interference ratio is.

NOTE 2 – At wanted signal level close to receiver sensitivity, noise should be taken into account, e.g. at sensitivity +3 dB, 3 dB should be added to the PR.

NOTE 3 - PR for different system variants and various reception conditions can be obtained using the correction factors in Table 50 in § 4 of this Annex. The overload threshold is assumed to be independent of system variant and reception conditions.

NOTE 4 – For further detail on the different BS traffic load case see 64, 66, 68 in Appendix 2 to Annex 2.

The range of protection ratios and overload thresholds obtained for LTE-UE interferer is listed in Table 38 for can tuners and Table 38A for silicon tuners for time variant and continuous interference.

The current worst case situation corresponds to interference from time varying signals. The highest level of protection (to protect broadcasting in the cases of continuous and time variant interference) is achieved by taking the highest value for the protection ratio and the lowest value for the overload threshold.

The protection ratios for interference signals with constant average power and no frequency variation were generally lower than those for time varying interference signals such as the pulsed LTE UE waveform. The overload threshold for interference signals with constant average power and no frequency variation were generally higher than those for time varying interference signals such as the pulsed LTE UE waveform. For further explanation see Report "Measurement of protection ratios and overload threshold for TV receivers".

The frequency offset is measured between the centre frequencies of wanted and interfering signals.

Interferer offset N/(MHz)	No. Rx	PR, dB 50 th percentile	PR, dB 90 th percentile	O _{th} , dBm 10 th percentile	O _{th} , dB 50 th percentile
1/(10 MHz)	19	-2113	-1412	-2119	-1611
2/(18 MHz)	19	4847	-4542	-184	-62
3/(26 MHz)	19	-4948	-4340	-3126	-1610
4/(34 MHz)	19	-6157	-5954	-1911	-139
5/(42 MHz)	19	-6756	-6350	-177	-94
6/(50 MHz)	31	-7356	-6649	-187	-92
7/(58 MHz)	19	-7457	-7147	-163	-3 2
8/(66 MHz)	31	-7859	-7052	-163	-4 2
9/(74 MHz)	19	-5044	-3833	-93	-2 4

PR values at the 50th and 90th percentile and O_{th} values at the 10th and 50th percentile for a 8 MHz DVB-T 64-QAM with code rate 2/3 signal interfered with by a 10 MHz LTE UE signal in a Gaussian channel environment for can tuners (see Notes 1 to 3)

NOTE 1 – PR is applicable unless the interfering signal level is above the corresponding O_{th} . If the interfering signal level is above the corresponding O_{th} , the receiver is interfered with by the interfering signal whatever the signal to interference ratio is.

NOTE 2 – At wanted signal level close to receiver sensitivity, noise should be taken into account, e.g. at sensitivity +3 dB, 3 dB should be added to the PR.

NOTE 3 - PR for different system variants and various reception conditions can be obtained using the correction factors in Table 50 in § 4 of this Annex. The overload threshold is assumed to be independent of system variant and reception conditions.

TABLE 38A

PR values at the 50 th and 90 th percentile and O _{th} values at the 10 th and 50 th percentile for a
8 MHz DVB-T 64-QAM with code rate 2/3 signal interfered with by a 10 MHz LTE
UE signal in a Gaussian channel environment for silicon tuners (see Notes 1 to 4)

Interferer offset N/(MHz)	No. Rx	PR, dB 50 th percentile	PR, dB 90 th percentile	O _{th} , dBm 10 th percentile	O _{th} , dB 50 th percentile
1/(10 MHz)	4	-14	-13	-2317	-16
2/(18 MHz)	4	-4942	-4632	-465	-28 2
3/(26 MHz)	4	-5143	-4835	-472	-26 5
4/(34 MHz)	4	-5246	-4836	-446	-25 2
5/(42 MHz)	4	-5445	-5137	-435	-24 3
6/(50 MHz)	10	-5345	-4538	-417	-25 0
7/(58 MHz)	4	-5648	-5140	-395	-21 4
8/(66 MHz)	10	-5546	-4837	-357	-21 2
9/(74 MHz)	10	-5545	-4737	-3210	-231

NOTE 1 - PR is applicable unless the interfering signal level is above the corresponding O_{th} . If the interfering signal level is above the corresponding Oth, the receiver is interfered with by the interfering signal whatever the signal to interference ratio is.

NOTE 2 – At wanted signal level close to receiver sensitivity, noise should be taken into account, e.g. at sensitivity +3 dB, 3 dB should be added to the PR.

NOTE 3 - PR for different system variants and various reception conditions can be obtained using the correction factors in Table 50 in § 4 of this Annex. The overload threshold is assumed to be independent of system variant and reception conditions.

NOTE 4 – For some offsets only a limited number of tuners (four) have been tested. Therefore no valid statistics can be provided. More measurements are required to stabilize the values. The values can be found in Tables 65 and 67 in Appendix 2 to Annex 2 as a guidance and should be used carefully.

2 Protection ratios for wanted analogue terrestrial television signals interfered with by unwanted DVB-T digital terrestrial television signals

Tables 39 to 46 show protection ratios for a wanted 625-line analogue television signal interfered with by a DVB-T digital terrestrial television signal.

2.1 Protection ratios for 625-line television systems

Protection of wanted vision signals interfered with by DVB-T digital terrestrial 2.1.1 television signal

In this section the protection ratios for an analogue wanted signal interfered by an unwanted DVB-T digital signal relate only to the interference to the vision signal.

The protection ratio values given are related to an out-of-channel spectrum attenuation of the unwanted DVB-T transmitter of 40 dB.

2.1.1.1 Protection from co-channel interference

TABLE 39

Protection ratios (dB) for a wanted analogue vision signal interfered with by an unwanted DVB-T 8 MHz signal

Wanted signal:	Unwanted signal: DVB-T, 8 MHz		
analogue system	Tropospheric interference	Continuous interference	
B, D, D1, G, H, K/PAL	34	40	
I/PAL	37	41	
B, D, K, L/SECAM	35	41	

TABLE 40

Protection ratios (dB) for a wanted analogue vision signal interfered with by an unwanted DVB-T 7 MHz signal

Wanted signal:	Unwanted signal	Unwanted signal: DVB-T, 7 MHz		
analogue system	Tropospheric interference	Continuous interference		
B/PAL, B/SECAM	35	41		

2.1.1.2 Protection from lower adjacent channel interference

TABLE 41

Protection ratios (dB) for a wanted analogue vision signal interfered with by DVB-T 7 MHz and 8 MHz signals (lower adjacent channel)

Wanted signal:	Unwanted signal: DVB-T, 7 or 8 MHz (lower adjacent channel)		
analogue system	Tropospheric interference	Continuous interference	
B, D, D1, G, H, I, K/PAL	-9	-5	
B, D, K, L/SECAM	-5	-1	

2.1.1.3 **Protection from upper adjacent channel interference**

TABLE 42

Protection ratios (dB) for a wanted analogue vision signal interfered with by DVB-T 7 MHz and 8 MHz signals (upper adjacent channel)

Wanted signal: analogue system	Unwanted signal: DVB-T, 7 or 8 MHz (upper adjacent channel)		
analogue system	Tropospheric interference	Continuous interference	
PAL and SECAM	-8	-5	

2.1.1.4 Protection from image channel interference

TABLE 43

Protection ratios (dB) for a wanted analogue vision signal interfered with by a DVB-T 8 MHz signal (image channel)

Wanted analogue system	Unwanted DVB-T channel	Tropospheric interference	Continuous interference
D1, G/PAL	<i>N</i> +9	-19	-15
I/PAL	<i>N</i> +9		
L/SECAM ⁽¹⁾	<i>N</i> +9	-24	-22
D, K/SECAM ⁽¹⁾	N + 8, N + 9	-16	-11
D, K/PAL	<i>N</i> +8, <i>N</i> +9		

⁽¹⁾ Provisional values still under study.

TABLE 44

Protection ratios (dB) for a wanted analogue vision signal interfered with by a DVB-T 7 MHz signal (image channel)

Wanted analogue system Unwanted DVB-T channel		Tropospheric interference	Continuous interference
B/PAL	<i>N</i> +10, <i>N</i> +11	-22	-18

2.1.1.5 **Protection from overlapping interference**

TABLE 45

Protection ratios (dB) for analogue B, D, D1, G, H, K/PAL vision signals* interfered with by a DVB-T 7 MHz signal (overlapping channels)

	y of the centre of the unwanted DVB-T	Protecti	on ratio
0	ninus the vision carrier frequency of wanted analogue television signal (MHz)	Tropospheric interference	Continuous interference
	-7.75	-16	-11
(<i>N</i> – 1)	-4.75	-9	-5
	-4.25	-3	4
	-3.75	13	21
	-3.25	25	31
	-2.75	30	37
	-1.75	34	40
	-0.75	35	41

	of the centre of the unwanted DVB-T	Protection ratio				
0	nus the vision carrier frequency of anted analogue television signal (MHz)	Tropospheric interference	Continuous interference			
(N)	2.25	35	41			
	4.25	35	40			
	5.25	31	38			
	6.25	28	35			
	7.25	26	33			
	8.25	6	12			
(N+1)	9.25	-8	-5			
	12.25	-8	-5			

TABLE 45 (end)

* For all SECAM systems similar values are expected. The values are still under study.

TABLE 46

Protection ratios (dB) for analogue B, D, D1, G, H, K/PAL vision signals* interfered with by a DVB-T 8 MHz signal (overlapping channels)

	f the centre of the unwanted DVB-T	Protecti	on ratio
	nus the vision carrier frequency of nted analogue television signal (MHz)	Tropospheric interference ⁽¹⁾	Continuous interference ⁽¹⁾
	-8.25	-16	-11
(<i>N</i> – 1)	-5.25	-9	-5
	-4.75	-4	3
	-4.25	12	20
	-3.75	24	30
	-3.25	29	36
	-2.25	33	39
	-1.25	34	40
(N)	2.75	34	40
	4.75	34	39
	5.75	30	37
	6.75	27	34
	7.75	25	32
	8.75	5	11

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	of the centre of the unwanted DVB-T	Protection ratio			
signal minus the vision carrier frequency of the wanted analogue television signal (MHz)		Tropospheric interference ⁽¹⁾	Continuous interference ⁽¹⁾		
(<i>N</i> +1)	9.75	-8	-5		
	12.75	-8	-5		

TABLE 46 (end)

* For all SECAM systems similar values are expected. The values are still under study.

⁽¹⁾ The values for tropospheric and continuous interference have been arrived at from Table 45 by calculation.

3 Protection ratios for sound signals of wanted analogue terrestrial television signals interfered with by unwanted DVB-T digital terrestrial television signals

Tables 47 to 49 in this Annex show protection ratios for wanted FM, AM and NICAM television sound carriers interfered with by unwanted digital terrestrial television signals.

All protection ratios in this section refer to the level of the wanted television sound carriers. The reference level of the sound carriers is the r.m.s. value of the unmodulated carrier.

The sound quality for tropospheric interference corresponds to grade 3, for continuous interference to grade 4.

The reference (*S*/*Ns*) for FM sound signals are:

- 40 dB (approximates to impairment grade 3) tropospheric case;
- 48 dB (approximates to impairment grade 4) continuous case.

The reference S/Ns are measured as S/N peak-to-peak weighted, given in Recommendation ITU-R BS.468 and Recommendation ITU-R BS.412.

The reference FM sound signal level corresponds to a maximum frequency deviation of ±50 kHz.

The reference BERs for NICAM digital sound signals are:

- BER = 1×10^{-4} (approximates to impairment grade 3), tropospheric case;
- BER = 1×10^{-5} (approximates to impairment grade 4), continuous case.

In the case of a two-sound carrier transmission, each of the two-sound signals must be considered separately. Multiplex modulated sound signals may require higher protection.

3.1 Protection for FM, AM and NICAM sound signals of analogue television systems interfered with by DVB-T digital terrestrial television signals

TABLE 47

Co-channel protection (dB) ratios for a wanted sound signal interfered with by DVB-T digital terrestrial television signals

	Protection ratio related to the wanted sound carrier	Unwanted signal				
	Wanted sound signal	DVB-T 7 MHz	DVB-T 8 MHz			
FM	Tropospheric case	6	5			
	Continuous case	16	15			
AM	Tropospheric case	21	20			
	Continuous case	24	23			
NICAM	Tropospheric case	5	4			
PAL B/G	Continuous case	6	5			
NICAM	Tropospheric case					
System I	Continuous case					
NICAM	Tropospheric case	12	11			
System L	Continuous case	13	12			

TABLE 48

Protection ratios (dB) for a wanted FM sound signal interfered with by a DVB-T 7 MHz signal (overlapping channels)

			-	ency of the 3 minus sound	-		ignal	
Frequency of the DVB-T signal relative to an FM carrier	Protection ratio related to the wanted sound carrier	-500 kHz	–250 kHz	-50 kHz	0.0 kHz	50 kHz	250 kHz	500 kHz
DVB-T below FM	Tropospheric case	0	0	0	5	5	6	6
DVB-1 below FIVI	Continuous case	9	9	9	14	14	15	16
DVD T shave EM	Tropospheric case	5	5	4	3	-9	-22	-32
DVB-T above FM	Continuous case	15	15	14	12	-6	-16	-27

NOTE 1 – The protection ratio figures are related to an out-of-channel spectrum attenuation of 40 dB. NOTE 2 – This Table is still under study.

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TABLE 49

Protection ratios (dB) for a wanted AM sound signal interfered with by a DVB-T 8 MHz signal for different frequency offsets (upper adjacent channel)

Protection ratio related to the wanted sound carrier	Centre frequency of the DVB-T signal minus sound carrier frequency						
	With negative offset	No offset	With positive offset				
	4.250 – 0.166 MHz = 4.084 MHz	4.250 MHz	4.250 + 0.166 MHz = 4.416 MHz				
Tropospheric case	-1	-2	-4				
Continuous case	+1	0	-2				

4 Correction factors for different wanted DVB-T system variants and different reception conditions

The following Table 50 was developed on the basis of a DVB-T signal interfered with by DVB-T. It is proposed to be used for other types of interferers but further studies are required to confirm the values.

TABLE 50

Theoretical correction factors for protection ratios (dB) for different wanted DVB-T system variants relative to 64-QAM 2/3 DVB-T signal and for different reception conditions (interfered with by DVB-T or other services)

DVB-T system variant	Gaussian channel	Fixed reception	Portable outdoor reception	Portable indoor reception	Mobile reception
QPSK 1/2	-13.5	-12.5	-10.3	-10.3	-7.3
QPSK 2/3	-11.6	-10.5	-8.2	-8.2	-5.2
QPSK 3/4	-10.5	-9.3	-6.9	-6.9	-3.9
QPSK 5/6	-9.4	-8.1	-5.6	-5.6	-2.6
QPSK 7/8	-8.5	-7.1	-4.5	-4.5	-1.5
16-QAM 1/2	-7.8	-6.8	-3.6	-3.6	-1.6
16-QAM 2/3	-5.4	-4.3	-2.0	-2.0	1.0
16-QAM 3/4	-3.9	-2.7	-0.3	-0.3	2.7
16-QAM 5/6	-2.8	-1.5	1.0	1.0	4.0
16-QAM 7/8	-2.3	-0.9	1.7	1.7	4.7
64-QAM 1/2	-2.2	-1.2	1.0	1.0	4.0
64-QAM 2/3	0.0	1.1	3.4	3.4	6.4
64-QAM 3/4	1.6	2.8	5.2	5.2	8.2
64-QAM 5/6	3.0	4.3	6.8	6.8	9.8
64-QAM 7/8	3.9	5.3	7.9	7.9	10.9

As compared to a static transmission channel, the time-variant Rayleigh channel which is relevant for portable DVB-T reception shows a significantly higher need for protection ratios. The average increase in the PR values in a time-variant Rayleigh transmission channel compared to the values in a static Rayleigh transmission channel for all receivers measured is about 5 to 6 dB.

In summary, the PR values in a Gaussian transmission channel are 2 to 3 dB lower than the values in the static Rayleigh transmission channel. Compared to the static Rayleigh transmission channel, the time-variant Rayleigh channel shows 4 dB to 6 dB higher PRs.

5 Protection ratios for a T-DAB signal interfered with by an unwanted digital terrestrial television signal

TABLE 51

Protection ratios (dB) for a T-DAB signal interfered with by a DVB-T 8 MHz signal

	64-QAM, code rate 2/3								
$\Delta f^{(1)}$ (MHz)	$\Delta f^{(1)}(\text{MHz})$ -5 -4.2 -4 -3 0 3 4 4.2 5								
PR	-50	-1	0	1	1	1	0	-1	-50

⁽¹⁾ Δf : centre frequency of the DVB-T signal minus centre frequency of the T-DAB signal.

TABLE 52

Protection ratios (dB) for a T-DAB signal interfered with by a DVB-T 7 MHz signal

64-QAM, code rate 2/3										
$\Delta f^{(1)}(\text{MHz})$ -4.5 -3.7 -3.5 -2.5 0 2.5 3.5 3.7 4.5										
PR	-49	0	1	2	2	2	1	0	-49	

⁽¹⁾ Δf : centre frequency of the DVB-T signal minus centre frequency of the T-DAB signal.

6 Minimum field strengths for DVB-T terrestrial digital television, fixed reception

The formula for calculating minimum field strength is given in Appendix 1 to Annex 2.

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euk	ulation	or minin	inum nei	u su ch			z system	1		
Frequency (MHz)		200			550			700		
System variant guard interval 1/4	QPSK 2/3	16-QAM 2/3	64-QAM 2/3	QPSK 2/3	16-QAM 2/3	64-QAM 2/3	QPSK 2/3	16-QAM 2/3	64-QAM 2/3	
Receiver noise figure, F (dB)	5	5	5	7	7	7	7	7	7	
Receiver carrier/noise ratio ⁽¹⁾ (<i>C</i> / <i>N</i>) (dB)	8	14	20	8	14	20	8	14	20	
Feeder loss $A_f(dB)$	3	3	3	3	3	3	5	5	5	
Antenna gain, G (dB)	5	5	5	10	10	10	12	12	12	
Minimum field strength for fixed reception, $E_{min} (dB(\mu V/m))^{(2)}$	27	33	39	33	39	45	35	41	47	

TABLE 53

Calculation of minimum field strength DVB-T 8 MHz system

⁽¹⁾ For Rice channel.

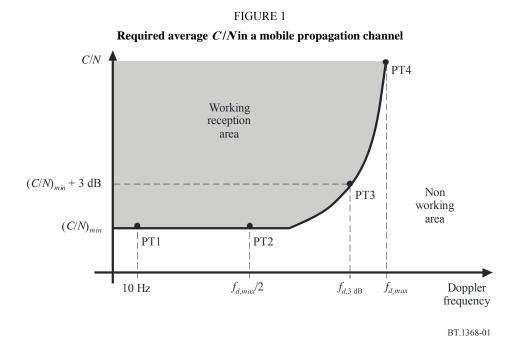
⁽²⁾ For formula, see Appendix 1 to Annex 2.

7 Minimum median field strength for mobile DVB-T reception

The equations for calculating the minimum median field strength are given in Appendix 1 to this Annex. The input values to the calculation are found in this section and in Annex 4. Mobile reception should be calculated with a location probability of 99%.

7.1 Required average *C*/*N* for mobile reception

For a given DVB-T mode the required average C/N for a certain quality level is a function of Doppler frequency only, and a graph like the one presented in Fig. 1 can be drawn.



The minimum required average C/N values (C/N_{min}) , Doppler frequency for an average C/N equal to $C/N_{min} + 3$ dB and the maximum Doppler (speed) limits for mobile reception are given in Table 54 and Table 55. The speed limits for $C/N_{min} + 3$ dB are given for three frequencies (200 MHz, 500 MHz and 800 MHz). The average C/N value, $C/N_{min} + 3$ dB, is suitable for calculation of required field strength. Table 54 shows values for the required average C/N and the speed limits in the non-diversity case. Table 55 contains the corresponding values for the diversity case. The values are based on the typical channel profile "typical urban" shown in Table 56. Quality criteria is the subjective failure point (SFP) corresponding to erroneous seconds ratio, -ESR = 5%, and packet error ratio, $\text{PER} = 1 \times 10^{-4}$.

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TABLE 54

Required average *C*/*N*, speed limits for mobile reception for the non-diversity case

	4 1 1/	20	2k						8k					
Guard II	nterval = 1/	Speed at F_{ab} 3 dB (km/h)				Speed at F_{cb} 3 dB (km/h)								
Modulation	Bit rate (Mbit/s)	Code rate	C/N _{min} (dB)	F _{d, max} (Hz)	<i>F</i> _d at <i>C</i> / <i>N</i> _{min} + 3 dB	200 MHz	500 MHz	800 MHz	C/N _{min} (dB)	F _{d, max} (Hz)	<i>F</i> _d at <i>C</i> / <i>N</i> _{min} + 3 dB	200 MHz	500 MHz	800 MHz
QPSK	6.03	1/2	13.0	318	259	1 398	559	349	13.0	76	65	349	140	87
QPSK	8.04	2/3	16.0	247	224	1 207	483	302	16.0	65	53	286	114	71
16-QAM	12.06	1/2	18.5	224	182	985	394	246	18.5	59	47	254	102	64
16-QAM	16.09	2/3	21.5	176	147	794	318	199	21.5	41	35	191	76	48
64-QAM	18.10	1/2	23.5	141	118	635	254	159	23.5	35	29	159	64	40
64-QAM	24.13	2/3	27.0	82	65	349	140	87	27.0	24	18	95	38	24

TABLE 55

Required average *C*/*N*, speed limits for mobile reception for the diversity case

Guard in	nterval = 1/	32	2k	2k Speed at <i>F_d</i> , 3 dB (km/ł					$8k$ Speed at F_{ab} 3 dB (km/h)					
Modulation	Bit rate (Mbit/s)	Code rate	C/N _{min} (dB)	F _{d, max} (Hz)	<i>F</i> _d at <i>C</i> / <i>N</i> _{min} + 3 dB	200 MHz	500 MHz	800 MHz	C/N _{min} (dB)	F _{d, max} (Hz)	<i>F</i> _d at <i>C</i> / <i>N</i> _{min} + 3 dB	200 MHz	500 MHz	800 MHz
QPSK	6.03	1/2	7.0	560	518	2 795	1 118	699	7.0	140	129	699	280	175
QPSK	8.04	2/3	10.0	494	447	2 414	966	604	10.0	129	106	572	229	143
16-QAM	12.06	1/2	12.5	447	365	1 969	788	492	12.5	118	94	508	203	127
16-QAM	16.09	2/3	15.5	353	294	1 588	635	397	15.5	82	71	381	152	95
64-QAM	18.10	1/2	17.5	282	235	1 271	508	318	17.5	71	59	318	127	79
64-QAM	24.13	2/3	21.0	165	129	699	280	175	21.0	47	35	191	76	48

Tap number	Delay (µs)	Power (dB)	Doppler category		
1	0	-3	Rayleigh		
2	0.2	0	Rayleigh		
3	0.5	-2	Rayleigh		
4	1.6	-6	Rayleigh		
5	2.3	-8	Rayleigh		
6	5	-10	Rayleigh		

Channel profile for measurement of required average *C/N* for mobile reception of DVB-T reception "typical urban"

The values for the bit rate correspond to the shortest guard interval 1/32 which is the least critical case in terms of Doppler. It is to be expected that when the guard interval increases the maximum speed decreases. For instance with 1/4 guard interval, the maximum Doppler, $F_{d max}$, decreases to about 85%.

The performance in a mobile channel depends to large extent on the design of the DVB-T receiver. Improvements may be achieved with receivers particularly designed for mobile reception.

DVB-H uses the DVB-T transmission system as the physical layer and adds extra error correction and time-slicing mechanism on the link layer. The maximum Doppler frequency (speed) in mobile reception will be improved due to the additional time interleaving. C/N values for DVB-H reception need to be developed.

7.2 Receiver noise figure

Noise figure of 5 dB is for integrated vehicle mobile receivers. A lower noise figure is possible when the antenna is internally matched to the first amplifier stage without a need for a loop through connection.

8 Minimum median field strength for hand held pedestrian indoor, pedestrian outdoor and mobile DVB-H reception

The equations for calculating the minimum median field strength are given in Appendix 1 to this Annex. The input values to the calculation are found in this section and in Annex 4. Mobile reception should be calculated with a location probability of 99%.

8.1 Channel models for hand held pedestrian indoor and outdoor reception

The pedestrian indoor (PI) and pedestrian outdoor (PO) channel models have been developed for describing the slowly moving hand held reception indoors and outdoors. The channel models are based on measurements in DVB-H single frequency networks and have paths from two different transmitter locations. Definitions of the taps for the channels are given in Table 58 and Table 59. The indicated Doppler frequency of 1.5 Hz is corresponding 3 km/h velocity at middle of UHF-band. The Doppler spectra of various taps are defined in Table 57.

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TABLE 57

Doppler spectrum definitions for PI- and PO-channels

Spectrum for the 1st tap

 $0.1G(f; 0.08 f_D) + \delta(f - 0.5 f_D)$

Spectrum for taps 2-12 $G(f; 0.08 f_D)$

where: (f_{2}^{2})

$$G(f;\sigma) = \exp\left(\frac{-f^2}{2\sigma^2}\right)$$

Definition of PI-channel

Path	Delay (µs)	Power (dB)	Doppler spectrum	Fd (Hz)	STD Norm.
1	0.0	0.0	See Table 2	1.69	0.08
2	0.1	-6.4	Gauss	1.69	0.08
3	0.2	-10.4	Gauss	1.69	0.08
4	0.4	-13.0	Gauss	1.69	0.08
5	0.6	-13.3	Gauss	1.69	0.08
6	0.8	-13.7	Gauss	1.69	0.08
7	1.0	-16.2	Gauss	1.69	0.08
8	1.6	-15.2	Gauss	1.69	0.08
9	8.1	-14.9	Gauss	1.69	0.08
10	8.8	-16.2	Gauss	1.69	0.08
11	9.0	-11.1	Gauss	1.69	0.08
12	9.2	-11.2	Gauss	1.69	0.08

Definition of PO-channel

Path	Delay (µs)	Power (dB)	Doppler spectrum	Fd (Hz)	STD Norm.
1	0.0	0.0	See Table 2	1.69	0.08
2	0.2	-1.5	Gauss	1.69	0.08
3	0.6	-3.8	Gauss	1.69	0.08
4	1.0	-7.3	Gauss	1.69	0.08
5	1.4	-9.8	Gauss	1.69	0.08
6	1.8	-13.3	Gauss	1.69	0.08
7	2.3	-15.9	Gauss	1.69	0.08
8	3.4	-20.6	Gauss	1.69	0.08
9	4.5	-19.0	Gauss	1.69	0.08
10	5.0	-17.7	Gauss	1.69	0.08
11	5.3	-18.9	Gauss	1.69	0.08
12	5.7	-19.3	Gauss	1.69	0.08

8.2 Channel model for mobile reception

The channel model for mobile reception is given in Table 54. This typical urban model is valid for both DVB-T and DVB-H.

8.3 Required average C/N for hand held indoor and outdoor reception

The DVB-H receiver shall have the performance given in Table 60 when noise (N) is applied together with the wanted carrier (C) in a signal bandwidth of 7.61 MHz. Degradation point criteria is 5% MPE-FEC frame error rate (5% MFER). The C/N performance figures are based on the state of the art receivers on the market added with a 2 dB margin.

TABLE 6	0
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C/N (dB) for 5% MFER in PI and PO channel

Modulation	Code rate	MPE-FEC code rate	PI	РО
QPSK	1/2	1/2	6.6	7.6
QPSK	1/2	2/3	6.8	7.8
QPSK	1/2	3/4	7.0	8.0
QPSK	1/2	5/6	7.2	8.2
QPSK	1/2	7/8	7.4	8.4
QPSK	2/3	2/3	9.8	10.8
QPSK	2/3	3/4	10.0	11.0
QPSK	2/3	5/6	10.2	11.2
QPSK	2/3	7/8	10.4	11.4
16-QAM	1/2	2/3	12.8	13.8

Modulation	Code rate	MPE-FEC code rate	PI	РО
16-QAM	1/2	3/4	13.0	14.0
16-QAM	1/2	5/6	13.2	14.2
16-QAM	1/2	7/8	13.4	14.4
16-QAM	2/3	2/3	15.8	16.8
16-QAM	2/3	3/4	16.0	17.0
16-QAM	2/3	5/6	16.2	17.2
16-QAM	2/3	7/8	16.4	17.4
64-QAM	1/2	5/6	17.7	18.7
64-QAM	1/2	7/8	17.9	18.9
64-QAM	2/3	2/3	20.6	21.6
64-QAM	2/3	3/4	20.8	21.8
64-QAM	2/3	5/6	21.0	22.0

TABLE 60 (end)

8.4 Required average *C*/*N* for hand held indoor and outdoor reception

The DVB-H receiver shall have the performance given in Table 61 when noise (*N*) and Doppler shift (F_d) is applied together with the wanted carrier (*C*) in mobile channel defined in Table 54. The figures are given for guard interval 1/4. The *C*/*N* performance is based on the state of the art DVB-H receivers with added 2 dB margin. The Doppler performance is derived from a use case analysis where the target speed with 8k mode at 750 MHz is 130 km/h. This corresponds to a Doppler frequency of 100 Hz. The 4k and 2k Doppler performance is obtained by multiplying the 8k performance by 2 and 4. Degradation point criteria is 5% MPE-FEC frame error rate (5% MFER).

DVB-H C/N (dB) in mobile channel for 5% MFER

Guard interval = 1/4		2k		Speed at F_d , 3 dB km/h		4k		Speed at F _d , 3 dB km/h		8k		Speed at F_d , 3 dB km/h		
Modula- tion	Code rate	MPE- FEC CR	C/N _{min} dB	<i>F_d</i> 3 dB Hz	474 MHz	746 MHz	C/N _{min} dB	<i>F_d</i> , 3 dB Hz	474 MHz	746 MHz	C/N _{min} dB	<i>F</i> _d , 3 dB Hz	474 MHz	746 MHz
QPSK	1/2	1/2	8.5	400	911	579	8.5	200	456	290	8.5	100	228	145
		2/3	9.0	400	911	579	9.0	200	456	290	9.0	100	228	145
		3/4	9.5	400	911	579	9.5	200	456	290	9.5	100	228	145
		5/6	10.0	400	911	579	10.0	200	456	290	10.0	100	228	145
		7/8	10.5	400	911	579	10.5	200	456	290	10.5	100	228	145
QPSK	2/3	2/3	12.0	400	911	579	12.0	200	456	290	12.0	100	228	145
		3/4	12.5	400	911	579	12.5	200	456	290	12.5	100	228	145
		5/6	13.5	400	911	579	13.5	200	456	290	13.5	100	228	145
		7/8	14.5	400	911	579	14.5	200	456	290	14.5	100	228	145
16-QAM	1/2	2/3	15.0	400	911	579	15.0	200	456	290	15.0	100	228	145
		3/4	15.5	400	911	579	15.5	200	456	290	15.5	100	228	145
		5/6	16.5	400	911	579	16.5	200	456	290	16.5	100	228	145
		7/8	17.5	400	911	579	17.5	200	456	290	17.5	100	228	145
16-QAM	2/3	2/3	18.0	380	866	550	18.0	190	433	275	18.0	95	216	138
		3/4	18.5	380	866	550	18.5	190	433	275	18.5	95	216	138
		5/6	19.5	380	866	550	19.5	190	433	275	19.5	95	216	138
		7/8	20.5	380	866	550	20.5	190	433	275	20.5	95	216	138
64-QAM	1/2	5/6	21.5	200	456	290	21.5	100	228	145	21.5	50	114	73
		7/8	22.5	200	456	290	22.5	100	228	145	22.5	50	114	73
64-QAM	2/3	2/3	25.0	120	273	174	25.0	60	137	87	25.0	30	68	43
		3/4	25.5	120	273	174	25.5	60	137	87	25.5	30	68	43
		5/6	27.0	120	273	174	27.0	60	137	87	27.0	30	68	43

8.5 Receiver noise figure

DVB-H receivers are expected to have a full interoperability with GSM-900 cellular radios and therefore have a GSM-reject filter in front of the DVB-H receiver. The total system noise figure of the receiver and the filter is 6 dB.

Appendix 1 to Annex 2

Calculation of minimum field strength and minimum median equivalent field strength

The minimum field strength and minimum median equivalent field strength values calculated using the following equations:

0 1			
P_n	=	$F + 10 \log (k T_0 B)$	
$P_{s min}$	=	$C/N + P_n$	
A_a	=	$G + 10 \log (1.64 \lambda^2 / 4 \pi)$	
ϕ_{min}	=	$P_{s \min} - A_a + L_f$	
E_{min}	=	$\varphi_{min} + 120 + 10 \log (120 \pi)$	
	=	$\varphi_{min} + 145.8$	
E_{med}	=	$E_{min} + P_{mmn} + C_1$	for roof top level fixed reception
E_{med}	=	$E_{min} + P_{mmn} + C_1 + L_h$	for portable outdoor and mobile reception
E_{med}	=	$E_{min} + P_{mmn} + C_1 + L_h + L_b$	for portable indoor and mobile hand-held reception

$$C_{l} = \mu \cdot \sigma_{t}$$
$$\sigma_{t} = \sqrt{\sigma_{b}^{2} + \sigma_{m}^{2}}$$

where:

 P_n : receiver noise input power (dBW) F: receiver noise figure (dB) Boltzmann's constant ($k = 1.38 \times 10^{-23}$ (J/K)) *k* : absolute temperature ($T_0 = 290$ (K)) T_0 : **B**: receiver noise bandwidth ($B = 7.61 \times 10^{6}$ (Hz)) minimum receiver input power (dBW) P_{smin} : RF *S*/*N* at the receiver input required by the system (dB) C/N: effective antenna aperture (dBm²) A_a : antenna gain related to half dipole (dBd) *G* : λ: wavelength of the signal (m) minimum pfd at receiving place $(dB(W/m^2))$ φ_{min} : L_f : feeder loss (dB) E_{min} : equivalent minimum field strength at receiving place $(dB(\mu V/m))$ E_{med} : minimum median equivalent field strength, planning value $(dB(\mu V/m))$

 P_{mmn} : allowance for man-made noise (dB)

- L_h : height loss (reception point at 1.5 m above ground level) (dB)
- L_b : building or vehicle entry loss (dB)
- C_l : location correction factor (dB)
- σ_t : total standard deviation (dB)
- σ_m : standard deviation macro-scale ($\sigma_m = 5.5$ (dB))
- σ_b : standard deviation building entry loss (dB)
- μ : distribution factor being 0.52 for 70%, 1.28 for 90%, 1.64 for 95% and 2.33 for 99%.

Appendix 2 to Annex 2

The following Table 62 gives the raw measurement results for silicon tuners for the case of UMTS BS interference. These values are for guidance and should be used carefully.

TABLE 62

Protection ratios (PR) and overload thresholds (O_{th}) for DVB-T 8 MHz 64-QAM code rate 2/3 signal interfered with by emissions of 5 MHz UMTS base station without transmit power control (TPC Off) measured for silicon tuners (see Notes 1 to 3)

Interferer offset N/(MHz)		PR, dB		O _{th} , dBm			
(5 MHz Steps)	Si-E	Si-F	Si-B	Si-E	Si-F	Si-B	
1/(6.5 MHz)	-47	-39	-44	-8	-6	0	
2/(11.5 MHz)	-50	-42	-48	2	-3	4	
3/(16.5 MHz)	-51	-45	-48	4	-3	8	
4/(21.5 MHz)	-53	-46	-49	4	-2	10	
5/(26.5 MHz)	-55	-47	-49	5	-3	10	
6/(31.5 MHz)	-57	-48	-49	4	-2	10	
7/(36.5 MHz)	-57	-48	-49	4	-2	10	
8/(41.5 MHz)	-58	-49	-49	4	-2	10	
9/(46.5 MHz)	-57	-50	-49	4	-2	10	
10/(51.5 MHz)	-60	-50	-50	5	-3	10	
11/(56.5 MHz)	-62	-51	-50	5	-3	10	
14/(71.5 MHz)	-59	-53	-53	4	-3	10	

NOTE 1 - PR is applicable unless the interfering signal level is above the corresponding O_{th}. If the interfering signal level is above the corresponding O_{th}, the receiver is interfered with by the interfering signal whatever the signal to interference ratio is.

NOTE 2 – At wanted signal level close to receiver sensitivity, noise should be taken into account, e.g. at sensitivity +3 dB, 3 dB should be added to the PR.

NOTE 3 - PR for different system variants and various reception conditions can be obtained using the correction factors in Table 50 in § 4 of this Annex. The overload threshold is assumed to be independent of system variant and reception conditions.

The following Table 63 gives the raw measurement results for silicon tuners for the case of UMTS UE interference. These values are for guidance and should be used carefully.

TABLE 63

Protection ratios (PR) and overload thresholds for DVB-T 8 MHz 64-QAM code rate 2/3 signal interfered with by emissions of 5 MHz UMTS User Equipment with transmit power control (TPC On) measured for silicon tuners (see Notes 1 to 3)

Interferer offset N/(MHz)		PR, dB		O _{th} , dBm			
(5 MHz Steps)	Si-E	Si-F	Si-B	Si-E	Si-F	Si-B	
1/(6.5 MHz)	-28	-16	-27	NR	NR	-41	
2/(11.5 MHz)	-31	-32	-28	NR	-34	-41	
3/(16.5 MHz)	-31	-32	-29	NR	-33	-38	
4/(21.5 MHz)	-33	-33	-29	NR	-32	-38	
5/(26.5 MHz)	-33	-34	-30	1	-31	-39	
6/(31.5 MHz)	-35	-35	-30	3	-30	-40	
7/(36.5 MHz)	-35	-36	-31	4	-30	-39	
8/(41.5 MHz)	-36	-37	-32	4	-31	-39	
9/(46.5 MHz)	-37	-38	-33	5	-28	-37	
10/(51.5 MHz)	-36	-38	-32	5	-29	-36	
11/(56.5 MHz)	-38	-39	-34	6	-28	-36	
14/(71.5 MHz)	-41	-41	-34	6	-26	-35	

NOTE 1 - PR is applicable unless the interfering signal level is above the corresponding O_{th} . If the interfering signal level is above the corresponding O_{th} , the receiver is interfered with by the interfering signal whatever the signal to interference ratio is.

NOTE 2 – At wanted signal level close to receiver sensitivity, noise should be taken into account, e.g. at sensitivity +3 dB, 3 dB should be added to the PR.

NOTE 3 - PR for different system variants and various reception conditions can be obtained using the correction factors in Table 50 in § 4 of this Annex. The overload threshold is assumed to be independent of system variant and reception conditions.

The following Table 64 provides the protection ratios and overload thresholds obtained for LTE-BS interferer for the BS with 0% traffic load. Tables 64, 66 and 68 are used to fill in Table 37 in Annex 2.

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TABLE 64

PR values at the 50th and 90th percentile and O_{th} values at the 10th and 50th percentile for a 8 MHz DVB-T 64-QAM with code rate 2/3 signal interfered with by a 10 MHz LTE BS signal with 0% traffic load in a Gaussian channel environment for can tuners and silicon tuners (see Notes 1 to 7)

			Can tuner			Silicon tuner				
Interferer offset N/(MHz)	No. Rx (Note 6)	PR, dB 50 th percen- tile	PR, dB 90 th percen- tile	O _{th} , dBm 10 th percen- tile	O _{th} , dB 50 th percen- tile	No. Rx	PR, dB 50 th percen- tile	PR, dB 90 th percen- tile	O _{th} , dBm 10 th percen- tile	O _{th} , dBm 50 th percen- tile
1/(10 MHz)						6	-30.5	-20.5	-40.8	-38.0
2/(18 MHz)						6	-27.5	-21.5	-35.5	-6.0
3/(26 MHz)						6	-30.0	-24.5	-39.0	-4.5
4/(34 MHz)						6	-32.0	-28.5	-32.5	-4.5
5/(42 MHz)						6	-37.0	-32.0	-31.5	-3.0
6/(50 MHz)						6	-44.5	-35.0	-29.0	-2.0
7/(58 MHz)						6	-52.0	-37.0	-28.0	-1.0
8/(66 MHz)						6	-53.0	-38.5	-26.0	-1.5
9/(74 MHz)						6	-53.5	-40.0	-25.0	-1.5

NOTE 1 – PR is applicable unless the interfering signal is above the corresponding O_{th} . If the interfering signal level is above the corresponding O_{th} , the receiver will behave in a non-linear way.

NOTE 2 - At wanted signal level close to receiver sensitivity, noise should be taken into account, e.g. at 3 dB above receiver sensitivity threshold, 3 dB should be added to the PR.

NOTE 3 - PR for different system variants and various reception conditions can be obtained using the correction factors in Table 50 in § 4 of this Annex. The overload threshold is assumed to be independent of system variant and reception conditions.

NOTE 4 – Using statistical analysis (assuming a Gaussian cumulative distribution) the 50^{th} and 90^{th} percentile of all measured protection ratios and the 10^{th} and 50^{th} percentile of all measured overload thresholds for LTE interference into DVB-T were calculated.

NOTE 5 – The 90th (respectively 50th) percentile for the protection ratio value corresponds to the protection of 90% (respectively 50%) of receivers measured. The 10th (respectively 50th) percentile for the overload threshold value corresponds to the protection of 90% (respectively 50%) of receivers measured.

NOTE 6 – The term 0% traffic loading on an LTE BS refers to the situation where the base station is not handling any user traffic but is still transmitting signalling, synchronisation and possibly occasional broadcast data. Experiments showed that two out of the 4 TV receivers tested suffered degraded protection ratios when the BS traffic loading was between 0% and 30%.

NOTE 7 - A limited number of two can-tuners (two) has been tested for this case. Therefore no valid statistics can be provided. The values can be found in Table 65 below as a guidance and should be used carefully.

The following Table 65 gives the raw measurement results for can tuners for the case of LTE BS interference (0% traffic load). These values are for guidance and should be used carefully.

PR values and O_{th} values for a 8 MHz DVB-T 64-QAM with code rate 2/3 signal interfered with by of a 10 MHz LTE BS signal with 0% traffic load in a Gaussian channel environment for the measured can tuners (see Notes 1 to 4)

Interferer offset N/(MHz)	PR	dBm		
(8 MHz Steps)	Rx5(Can)	Rx6(Can)	Rx5(Can)	Rx6(Can)
1/(10 MHz)	-45	-45	-14	-12
2/(18 MHz)	-56	-54	-7	-2
3/(26 MHz)	-45	-52	4	-4
4/(34 MHz)	-49	-67	4	-3
5/(42 MHz)	-52	-70	6	1
6/(50 MHz)	-54	-71	9	2
7/(58 MHz)	-57	-71	7	3
8/(66 MHz)	-58	-70	7	4
9/(74 MHz)	-55	-62	8	3

NOTE 1 - PR is applicable unless the interfering signal level is above the corresponding O_{th} . If the interfering signal level is above the corresponding O_{th} , the receiver is interfered with by the interfering signal whatever the signal to interference ratio is.

NOTE 2 – At wanted signal level close to receiver sensitivity, noise should be taken into account, e.g. at sensitivity +3 dB, 3 dB should be added to the PR.

NOTE 3 - PR for different system variants and various reception conditions can be obtained using the correction factors in Table 50 in § 4 of this Annex. The overload threshold is assumed to be independent of system variant and reception conditions.

NOTE 4 – The term 0% traffic loading on an LTE BS refers to the situation where the base station is not handling any user traffic but is still transmitting signalling, synchronisation and possibly occasional broadcast data. Experiments showed that two out of the 4 TV receivers tested suffered degraded protection ratios when the BS traffic loading was between 0% and 30%.

The following table provides the protection ratios and overload thresholds obtained for LTE-BS interferer for the BS with 50% traffic load.

PR values at the 50th and 90th percentile and O_{th} values at the 10th and 50th percentile for a 8 MHz DVB-T 64-QAM with code rate 2/3 signal interfered with by a 10 MHz LTE BS signal with 50% traffic load in a Gaussian channel environment for can tuners and silicon tuners (see Notes 1 to 5)

			Can Tuner				Silicon Tuner				
Interferer Offset N/(MHz)	No. Rx (Note 6)	PR, dB 50 th percen- tile	PR, dB 90 th percen- tile	O _{th} , dBm 10 th percen- tile	O _{th} , dB 50 th percen- tile	No. Rx	PR, dB 50 th percen- tile	PR, dB 90 th percen- tile	O _{th} , dBm 10 th percen- tile	O _{th} , dBm 50 th percen- tile	
1/(10 MHz)						6	-40.0	-39.5	-10.0	-2.5	
2/(18 MHz)						6	-51.0	-46.0	-10.5	1.0	
3/(26 MHz)						6	-52.0	-47.0	-10.0	2.5	
4/(34 MHz)						6	-54.5	-48.0	-9.5	3.5	
5/(42 MHz)						6	-55.0	-49.5	-9.0	4.5	
6/(50 MHz)						6	-56.5	-50.0	-8.5	4.5	
7/(58 MHz)						6	-56.5	-52.0	-8.5	5.0	
8/(66 MHz)						6	-56.5	-52.5	-8.5	5.5	
9/(74 MHz)						6	-56.5	-53.0	-8.5	5.5	

NOTE 1 – PR is applicable unless the interfering signal is above the corresponding O_{th} . If the interfering signal level is above the corresponding O_{th} , the receiver will behave in a nonlinear way.

NOTE 2 - At wanted signal level close to receiver sensitivity, noise should be taken into account, e.g. at 3 dB above receiver sensitivity threshold, 3 dB should be added to the PR.

NOTE 3 - PR for different system variants and various reception conditions can be obtained using the correction factors in Table 50 in § 4 of this Annex. The overload threshold is assumed to be independent of system variant and reception conditions.

NOTE 4 – Using statistical analysis (assuming a Gaussian cumulative distribution) the 50^{th} , and 90^{th} percentile of all measured protection ratios and the 10^{th} and 50^{th} percentile of all measured overload thresholds for LTE interference into DVB-T were calculated.

NOTE 5 – The 90th (respectively 50th) percentile for the protection ratio value corresponds to the protection of 90% (respectively 50%) of receivers measured. The 10^{th} (respectively 50th) percentile for the overload threshold value corresponds to the protection of 90% (respectively 50%) of receivers measured.

NOTE 6 - A limited number of can-tuners (two) has been tested for this case. Therefore no valid statistics can be provided. The values can be found in Table 67 below as a guidance and should be used carefully.

The following Table 67 gives the raw measurement results for can tuners for the case of LTE BS interference (50% traffic load). These values are for guidance and should be used carefully.

PR values and O_{th} values for a 8 MHz DVB-T 64-QAM with code rate 2/3 signal interfered with by of a 10 MHz LTE BS signal with 50% traffic load in a Gaussian channel environment for the measured can tuners (see Notes 1 to 4)

Interferer offset N/(MHz)	PR	, dB	O _{th} , dBm		
(8 MHz Steps)	Rx5(Can)	Rx6(Can)	Rx5(Can)	Rx6(Can)	
1/(10 MHz)	-44	-46	-14	-18	
2/(18 MHz)	-60	-54	-4	-3	
3/(26 MHz)	-54	-51	-9	1	
4/(34 MHz)	-47	-39	3	1	
5/(42 MHz)	-52	-70	8	1	
6/(50 MHz)	-54	-70	8	2	
7/(58 MHz)	-57	-70	8	3	
8/(66 MHz)	-57	-70	8	2	
9/(74 MHz)	-52	-59	8	3	

NOTE 1 - PR is applicable unless the interfering signal is above the corresponding O_{th} . If the interfering signal level is above the corresponding O_{th} , the receiver will behave in a nonlinear way.

NOTE 2 - At wanted signal level close to receiver sensitivity, noise should be taken into account, e.g. at 3 dB above receiver sensitivity threshold, 3 dB should be added to the PR.

NOTE 3 - PR for different system variants and various reception conditions can be obtained using the correction factors in Table 50 in § 4 of this Annex. The overload threshold is assumed to be independent of system variant and reception conditions.

The following table provides the protection ratios and overload thresholds obtained for LTE-BS interferer for the BS with 100% traffic load. These figures are used to fill-in Table 36.

PR values at the 50th and 90th percentile and O_{th} values at the 10th and 50th percentile for a 8 MHz DVB-T 64-QAM with code rate 2/3 signal interfered with by a 10 MHz LTE BS signal with 100% traffic load in a Gaussian channel environment for can tuners and silicon tuners (see Notes 1 to 5)

		Can tuner					Silicon tuner			
Interferer offset N/(MHz)	No. Rx	PR, dB 50 th percen- tile	PR, dB 90 th percen- tile	O _{th} , dBm 10 th percen- tile	O _{th} , dB 50 th percen- tile	No. Rx	PR, dB 50 th percen- tile	PR, dB 90 th percen- tile	O _{th} , dBm 10 th percen- tile	O _{th} , dBm 50 th percen- tile
1/(10 MHz)	36	-39	-33	-13	-9	20	-38	-34	-13	-7
2/(18 MHz)	36	-46	-42	-8	-3	20	-45	-40	-8	-1
3/(26 MHz)	36	-49	-39	-18	-2	20	-47	-45	-6	2
4/(34 MHz)	24	-58	-55	-13	-8	12	-52	-48	-10	4
5/(42 MHz)	24	-64	-63	-8	-4	12	-53	-49	-10	5
6/(50 MHz)	24	-59	-58	-5	-1	12	-54	-50	-9	4
7/(58 MHz)	24	-67	-66	-5	1	12	-54	-50	-8	3
8/(66 MHz)	24	-68	-65	-5	1	12	-55	-51	-7	3
9/(74 MHz)	36	-46	-39	-3	2	20	-53	-46	-6	3

NOTE 1 – PR is applicable unless the interfering signal is above the corresponding O_{th} . If the interfering signal level is above the corresponding O_{th} , the receiver will behave in a nonlinear way.

NOTE 2 - At wanted signal level close to receiver sensitivity, noise should be taken into account, e.g. at 3 dB above receiver sensitivity threshold, 3 dB should be added to the PR.

NOTE 3 - PR for different system variants and various reception conditions can be obtained using the correction factors in Table 50 in § 4 of this Annex. The overload threshold is assumed to be independent of system variant and reception conditions.

NOTE 4 – Using statistical analysis (assuming a Gaussian cumulative distribution) the 50^{th} , and 90^{th} percentile of all measured protection ratios and the 10^{th} and 50^{th} percentile of all measured overload thresholds for LTE interference into DVB-T were calculated.

NOTE 5 – The 90th (respectively 50th) percentile for the protection ratio value corresponds to the protection of 90% (respectively 50%) of receivers measured. The 10th (respectively 50th) percentile for the overload threshold value corresponds to the protection of 90% (respectively 50%) of receivers measured.

Annex 3

Planning criteria for ISDB-T¹ digital television system in the VHF/UHF bands

1 Protection ratios for ISDB-T wanted digital terrestrial television signals

Tables 69 to 73 and 74 to 79 show protection ratios for an ISDB-T wanted digital terrestrial television signal interfered with by an ISDB-T digital terrestrial television signal and by an analogue terrestrial television signal, respectively. Tables 70 and 73 also show protection ratios for an ISDB-T wanted digital terrestrial television signal interfered with by a DVB-T digital terrestrial television signal.

¹ ISDB-T is used in Japan, Brazil and other countries not part of the GE06 Agreement.

1.1 Protection of an ISDB-T digital terrestrial television signal interfered with by digital television signals

TABLE 69

Co-channel protection ratios (dB) for ISDB-T 6 MHz interfered with by ISDB-T 6 MHz

Cading note		Modulation	
Coding rate	DQPSK	16-QAM	64-QAM
7/8	10	17	23
5/6	9	16	22
3/4	9	15	21
2/3	8	14	20
1/2	6	12	17

TABLE 70

Co-channel protection ratios (dB) for an ISDB-T 8 MHz signal interfered with by an ISDB-T 8 MHz or a DVB-T 8 MHz signal

Coding vote		Modulation	
Coding rate	QPSK	16-QAM	64-QAM
1/2	5	10	16
2/3	7	13	19
3/4		14	20

NOTE 1 – The protection ratios described in this Table are only valid for a Gaussian channel, they can be applied for a DVB-T 8 MHz signal interfered with by an ISDB-T 8 MHz signal.

TABLE 71

Protection ratios (dB) for ISDB-T 6 MHz interfered with by ISDB-T 6 MHz in lower adjacent channel (N – 1)

Coding note		Modulation	
Coding rate	DQPSK	16-QAM	64-QAM
7/8	-28	-27	-24
5/6	-28	-27	-25
3/4	-29	-27	-26
2/3	-29	-28	-26
1/2	-29	-28	-27

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TABLE 72

Coding note		Modulation	
Coding rate	DQPSK	16-QAM	64-QAM
7/8	-29	-28	-27
5/6	-29	-28	-27
3/4	-29	-28	-27
2/3	-30	-29	-27
1/2	-30	-29	-28

Protection ratios (dB) for ISDB-T 6 MHz interfered with by ISDB-T 6 MHz in upper adjacent channel (N + 1)

TABLE 73

Protection ratios (dB) for an ISDB-T 8 MHz signal interfered with by an ISDB-T 8 MHz or a DVB-T 8 MHz signal in the lower (N - 1) and upper (N + 1) adjacent channels

Channel	N-1	N+1
Protection ratio	-30	-30

NOTE – The protection ratios described in this Table are only valid for a Gaussian channel, they can be applied for a DVB-T 8 MHz signal interfered with by an ISDB-T 8 MHz signal.

1.2 Protection of an ISDB-T digital terrestrial television signal interfered with by analogue terrestrial television signals

1.2.1 Protection from co-channel interference

TABLE 74

Co-channel protection ratios (dB) for ISDB-T 6 MHz interfered with by analogue television

	Protection ratio									
Modulation			DQPSK			QPSK 1/2 2/3 3/4 5/6 7/8 -16 -11 -8 0 2 64-QAM 64-QAM 64-QAM				
Code rate	1/2	2/3	3/4	5/6	7/8	1/2	2/3	3/4	5/6	7/8
M/NTSC	-5	-3	-1	2	6	-16	-11	-8	0	2
Modulation			16-QAM	1		64-QAM				
Code rate	1/2	2/3	3/4	5/6	7/8	1/2	2/3	3/4	5/6	7/8
M/NTSC	-11	-5	-1	6	10	-6	-1	5	9	14

NOTE 1 – The sound carrier level is 6 dB lower than NTSC vision carrier level.

NOTE 2 – The values in this Table give the reception threshold. Taking into account the performance variation in domestic receivers, long-term degradation of reception condition, etc., a margin of several dBs should preferably be added in actual frequency planning.

Wanted	Wanted signal	
Modulation	Coding rate	I/PAL, G/PAL
QPSK	1/2	-16
QPSK	2/3	-11
QPSK	3/4	-8
16-QAM	1/2	-11
16-QAM	2/3	-5
16-QAM	3/4	-1
64-QAM	1/2	-6
64-QAM	2/3	-1
64-QAM	3/4	5

Co-channel protection ratios (dB) for an ISDB-T 8 MHz signal interfered with by analogue television (non-controlled frequency condition) signals

1.2.2 Protection from lower adjacent channel (N - 1) interference

TABLE 76

Protection ratios (dB) for lower adjacent channel (N – 1) interference for ISDB-T 6 MHz interfered with by NTSC signals including sound

Wanted signal		Unwanted signal
Modulation	Coding rate	M/NTSC
DQPSK	1/2	-34
DQPSK	2/3	-34
DQPSK	3/4	-33
16-QAM	1/2	-34
16-QAM	2/3	-33
16-QAM	3/4	-32
64-QAM	2/3	-32
64-QAM	3/4	-31
64-QAM	5/6	-29
64-QAM	7/8	-29

Wante	d signal	Unwante	ed signal
Modulation	Coding rate	I/PAL	G/PAL
QPSK	1/2		-44
QPSK	2/3		-44
QPSK	3/4		
16-QAM	1/2	-43	-43
16-QAM	2/3		-42
16-QAM	3/4		-38
64-QAM	1/2	-38	-40
64-QAM	2/3	-34	-35
64-QAM	3/4		-32

Protection ratios (dB) for lower adjacent channel (N – 1) interference for an ISDB-T 8 MHz signal interfered with by analogue television signals including sound

1.2.3 Protection from upper adjacent channel (N + 1) interference

TABLE 78

Protection ratios (dB) for upper adjacent channel (N + 1) interference for ISDB-T 6 MHz interfered with by NTSC 6 MHz signal

Wanted signal		Unwanted signal
Modulation	Coding rate	M/NTSC
DQPSK	1/2	-35
DQPSK	2/3	-35
DQPSK	3/4	-34
16-QAM	1/2	-35
16-QAM	2/3	-34
16-QAM	3/4	-33
64-QAM	2/3	-33
64-QAM	3/4	-33
64-QAM	5/6	-32
64-QAM	7/8	-31

Wantee	Wanted signal		
Modulation	Coding rate	I/PAL, G/PAL	
QPSK	1/2		
QPSK	2/3	-47	
QPSK	3/4		
16-QAM	1/2		
16-QAM	2/3	-43	
16-QAM	3/4		
64-QAM	1/2		
64-QAM	2/3	-38	
64-QAM	3/4		

Protection ratios (dB) for upper adjacent channel (N + 1) interference for an ISDB-T 8 MHz signal interfered with by analogue television signals

2 Protection ratios for wanted analogue terrestrial television signals interfered with by unwanted ISDB-T digital terrestrial television signals

Tables 80 and 81 shows protection ratios for a 525-line and a 625-line wanted analogue television signals interfered with by an ISDB-T digital terrestrial television signal, respectively.

The protection ratio values given in Table 80 are related to a spectrum shoulder attenuation of the unwanted digital signal of 38 dB. The protection ratio values given in Tables 81, 82 and 83 are related to an out-of-channel spectrum attenuation of the unwanted digital signal of 40 dB.

Tropospheric and continuous interference correspond to quality impairment grades 3 and 4, respectively. (See Table 107 of Annex 6.)

2.1 **Protection ratios for 525-line television systems**

2.1.1 Protection for NTSC vision signals interfered with by an ISDB-T digital television signal

TABLE 80

Protection ratios (dB) for analogue vision signal (NTSC, 6 MHz) interfered with by ISDB-T signal

Unwanted digital channel	Tropospheric interference	Continuous interference
N-1 (lower)	-6	-3
N (co-channel)	39	44
N+1 (upper)	-6	-3

- 2.2 **Protection ratios for 625-line television systems**
- 2.2.1 Protection for PAL vision signals interfered with by an ISDB-T digital television signal
- 2.2.1.1 Protection from co-channel interference

TABLE 81

Protection ratios (dB) for wanted analogue vision signals (I/PAL and G/PAL, 8 MHz) interfered with by an unwanted ISDB-T 8 MHz signal

Unwanted digital channel	Tropospheric interference	Continuous interference
I/PAL	37	41
G/PAL	34	40

2.2.1.2 **Protection from lower adjacent channel interference**

TABLE 82

Protection ratios (dB) for wanted analogue vision signals (I/PAL and G/PAL, 8 MHz) interfered with by an wanted ISDB-T 8 MHz signal (lower adjacent channel)

Unwanted digital channel	Tropospheric interference	Continuous interference
I/PAL	-9	-5
G/PAL	-9	-5

2.2.1.3 Protection from upper adjacent channel interference

TABLE 83

Protection ratios (dB) for wanted analogue vision signals (I/PAL and G/PAL, 8 MHz) interfered with by an wanted ISDB-T 8 MHz signal (upper adjacent channel)

Unwanted digital channel	Tropospheric interference	Continuous interference
I/PAL	-8	-5
G/PAL	-8	-5

3 Protection ratios for sound signals of wanted analogue terrestrial television systems interfered with by ISDB-T unwanted digital terrestrial television system

3.1 Protection for NTSC sound signals interfered with by an ISDB-T digital television signal

As shown in Table 84, the sound signal of NTSC broadcasting is robust compared with the vision signal when interfered with by an ISDB-T signal. Therefore protection ratios for NTSC broadcasting are determined by the protection ratios for the vision signal, which are shown in Table 80.

TABLE 84

	Measurement condition (see Note 3)	Sound quality
Co-channel interference	D/U = 39 dB	> grade 4 ($S/N = 54$ dB)
Upper adjacent channel interference	D/U = -6 dB	> grade 4 ($S/N = 53$ dB)
Lower adjacent channel interference	D/U = -6 dB	> grade 4 (S/N = 52 dB)

Sound quality related to the vision protection ratio of grade 3 when NTSC 6 MHz signal interfered with by ISDB-T 6 MHz signal

NOTE 1 – The sound carrier level is 6 dB lower than NTSC vision carrier level.

NOTE 2 – The reference FM sound signal level corresponds to a maximum frequency deviation of ±25 kHz.

NOTE 3 - D/U ratio that gives vision quality of grade 3 (corresponding to protection ratio for tropospheric interference).

3.2 Protection for FM sound signals of I/PAL and G/PAL analogue television systems interfered with by an ISDB-T digital terrestrial television signal

Table 85 shows protection ratios for wanted FM sound signals of I/PAL and G/PAL analogue television systems interfered with by an unwanted ISDB-T digital terrestrial television signal.

All protection ratios in this section refer to the level of the wanted television sound carriers. The reference level of the sound carriers is the r.m.s. value of the unmodulated carrier.

The sound quality for tropospheric interference corresponds to grade 3, for continuous interference to grade 4.

The reference (S/Ns) for FM sound signals are:

- 40 dB (approximates to impairment grade 3) tropospheric case;
- 48 dB (approximates to impairment grade 4) continuous case.

The reference S/Ns are measured as S/N peak-to-peak weighted, given in Recommendation ITU-R BS.468 and Recommendation ITU-R BS.412.

TABLE 85

Co-channel protection ratios (dB) for a wanted sound signal interfered with by an ISDB-T digital terrestrial television signal

	Protection ratio related to the wanted sound carrier	Unwanted signal			
	Wanted sound signal	ISDB-T 8 MHz			
FM	Tropospheric case	5			
(I, G/PAL)	Continuous case	15			

4 Minimum field strengths for ISDB-T terrestrial digital television, fixed reception

To reduce the number of tables for the minimum field strengths of an ISDB-T system, the derivation of minimum field strengths is made with the typical transmission modes shown in Tables 86 and 87. The minimum field strengths for the different modes of a 6 MHz and an 8 MHz system can be calculated from the given values in Tables 86 and 87, respectively.

5 Minimum median field strength for hand-held pedestrian indoor, pedestrian outdoor and mobile ISDB-T reception

The equations for calculating the minimum median field strength are given in Appendix 1 to this Annex, and the values that were used in the calculation are in this section and Annex 5. To calculate the minimum median field strength for pedestrian indoor, pedestrian outdoor, and mobile ISDB-T reception, the value of the location probability should be determined by the administration that has the transmitting stations on its territory.

5.1 Channel models for hand-held pedestrian indoor and outdoor reception

The pedestrian indoor (PI) and the pedestrian outdoor (PO) channel models are used as channel models for hand-held reception. Definitions of the taps for the channels are given in Tables 58 and 59. The Doppler spectra of various taps are defined in Table 57.

		Low VHF High VHF											
Frequency		Low V	/HF			Hig	h VHF		UHF				
(MHz)		100)			200				600			
System	DQPSK 1/2	QPSK 1/2	16- QAM 3/4	64- QAM 7/8	DQPSK 1/2	QPSK 1/2	16-QAM 3/4	64-QAM 7/8	DQPSK 1/2	QPSK 1/2	16-QAM 3/4	64-QAM 7/8	
Noise bandwidth, <i>B</i> (MHz)	5.6	5.6	5.6	5.6	5.6	5.6	5.6	5.6	5.6	5.6	5.6	5.6	
Receiver noise figure, F (dB)	5	5	5	5	5	5	5	5	7	7	7	7	
Receiver noise input voltage, $U_N^{(1)}$ (dB(μ V))	7.1	7.1	7.1	7.1	7.1	7.1	7.1	7.1	9.1	9.1	9.1	9.1	
Receiver carrier/ noise ratio ⁽²⁾ (<i>C</i> / <i>N</i>) (dB)	6.2	4.9	14.6	22.0	6.2	4.9	14.6	22.0	6.2	4.9	14.6	22.0	
Urban noise (dB)	1	1	1	1	1	1	1	1	0	0	0	0	
Minimum receiver input voltage, U_{min} $(dB(\mu V))^{(1)}$	14.3	13.0	22.7	30.1	14.3	13.0	22.7	30.1	15.3	14.0	23.7	31.1	
Conversion factor ⁽¹⁾ K (dB)	6.4	6.4	6.4	6.4	12.4	12.4	12.4	12.4	21.9	21.9	21.9	21.9	

TABLE 86

Calculation of minimum field strengths for ISDB-T 6 MHz system

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TABLE 86 (end)	
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Frequency		Low V	HF			High VHF				UHF			
(MHz)	100					200					600		
System	DQPSK 1/2	QPSK 1/2	16- QAM 3/4	64- QAM 7/8	DQPSK 1/2	QPSK 1/2	16-QAM 3/4	64-QAM 7/8	DQPSK 1/2	QPSK 1/2	16-QAM 3/4	64-QAM 7/8	
Feeder loss, $L_f(dB)$	3	3	3	3	3	3	3	3	3	3	3	3	
Antenna gain, <i>G</i> (dB)	3	3	3	3	5	5	5	5	10	10	10	10	
Minimum field strength for fixed reception, E_{min} (dB $(\mu V/m))^{(1)}$	20.7	19.4	29.1	36.5	24.7	23.4	33.1	40.5	30.2	28.9	38.6	46.0	

⁽¹⁾ For formula, see Appendix 1 to Annex 3.

⁽²⁾ For noise bandwidth noted above.

TABLE 87

Calculation of minimum field strengths for ISDB-T 8 MHz system

Frequency		Lov	VHF			High	n VHF		UHF			
(MHz)		1	100		200				600			
System	DQPSK 1/2	QPSK 1/2	16-QAM 3/4	64-QAM 7/8	DQPSK 1/2	QPSK 1/2	16-QAM 3/4	64-QAM 7/8	DQPSK 1/2	QPSK 1/2	16-QAM 3/4	64-QAM 7/8
Noise bandwidth, <i>B</i> (MHz)	7.4	7.4	7.4	7.4	7.4	7.4	7.4	7.4	7.4	7.4	7.4	7.4
Receiver noise figure, F (dB)	5	5	5	5	5	5	5	5	7	7	7	7
Receiver noise input voltage, $U_N^{(1)}$ (dB(μ V))	8.4	8.4	8.4	8.4	8.4	8.4	8.4	8.4	10.4	10.4	10.4	10.4
Receiver carrier/noise ratio ⁽²⁾ (C/N) (dB)	6.2	4.9	14.6	22.0	6.2	4.9	14.6	22.0	6.2	4.9	14.6	22.0
Urban noise (dB)	1	1	1	1	1	1	1	1	0	0	0	0
Minimum receiver input voltage, U_{min} $(dB(\mu V))^{(1)}$	15.5	14.2	23.9	31.3	15.5	14.2	23.9	31.3	16.5	15.2	24.9	32.3
Conversion factor ⁽¹⁾ K (dB)	6.4	6.4	6.4	6.4	12.4	12.4	12.4	12.4	21.9	21.9	21.9	21.9

Frequency	Low VHF				High VHF				UHF			
(MHz)	100				200					6	500	
System	DQPSK 1/2	QPSK 1/2	16-QAM 3/4	64-QAM 7/8	DQPSK 1/2	QPSK 1/2	16-QAM 3/4	64-QAM 7/8	DQPSK 1/2	QPSK 1/2	16-QAM 3/4	64-QAM 7/8
Feeder loss, $L_f(dB)$	3	3	3	3	3	3	3	3	3	3	3	3
Antenna gain, G (dB)	3	3	3	3	5	5	5	5	10	10	10	10
Minimum field strength for fixed reception, E_{min} $(dB(\mu V/m))^{(1)}$	21.9	20.6	30.3	37.7	25.9	24.6	34.3	41.7	31.4	30.1	39.8	47.2

TABLE 87 (end)

⁽¹⁾ For formula, see Appendix 1 to Annex 3.

⁽²⁾ For noise bandwidth noted above.

5.2 Channel model for mobile reception

The typical urban model is used as the channel model for mobile reception. The channel model for mobile reception is given in Table 56.

5.3 Required average *C*/*N* for hand-held indoor and outdoor reception

The ISDB-T receiver shall have the performance given in Table 88 when noise (N) is applied together with the wanted carrier (C) in a signal bandwidth of 5.57 MHz. The values for the C/N ratio in both the non-diversity case and the diversity case are shown in Table 88. Degradation point criterion is an erroneous second ratio (ESR) of 5%.

TABLE 88

Mada	Madadada	Code and a	For the non-d	liversity case	For the div	versity case
Mode	Modulation	Code rate	PI	РО	PI	РО
	QPSK	1/2	10	10.5	5	5
	QPSK	2/3	13	13.5	7.5	7.5
	16-QAM	1/2	15.5	16	11	11
2 k	16-QAM	2/3	19	20	13.5	13.5
	64-QAM	1/2	20.5 20.5		16	16
	64-QAM	2/3	24.5	24.5	19	19
	64-QAM	3/4	27	27	20.5	20.5
	QPSK	1/2	10	10	5	5.5
	QPSK	2/3	13	13	7.5	8
	16-QAM	1/2	15.5	15.5	10.5	11
4 k	16-QAM	2/3	19	19.5	13	13.5
	64-QAM	1/2	20.5	20.5	16	16
	64-QAM	2/3	24.5	25	19	19
	64-QAM	3/4	27	27	20.5	20.5

C/N (dB) for 5% ESR in PI and PO channel

Mode	Madulation	Code rate	For the non-d	liversity case	For the diversity case		
Widue	Modulation	Code rate	PI	РО	PI	РО	
	QPSK	1/2	10	10	5	5.5	
	QPSK	2/3	13.5	13.5	7.5	7.5	
	16-QAM	1/2	15.5	16	11	11	
8 k	16-QAM	2/3	19.5	19.5	13.5	13.5	
	64-QAM	1/2	20.5	21	16	16	
	64-QAM	2/3	24.5	24.5	19	19	
	64-QAM	3/4	27	27	20.5	21	

TABLE 88 (end)

5.4 Required average *C*/*N* for mobile reception

The ISDB-T receiver shall have the performance given in Table 89 when noise (*N*) and Doppler shift (F_d) is applied together with the wanted carrier (*C*) in the mobile channel based on the channel profile, "TYPICAL URBAN", which is shown in Table 56. The speed limits for $C/N_{min} + 3$ dB are given for two frequencies (470 and 770 MHz). The average C/N value, $C/N_{min} + 3$ dB, is suitable for calculating the required field strength. The values for the required average C/N ratio and the speed limits in the non-diversity case are shown in Table 90a), and the corresponding values for the diversity case are shown in Table 90b). The figures are given for a guard interval of 1/8. Degradation point criterion is given by an ESR of 5%.

TABLE 89

ISDB-T C/N (dB) in mobile channel for 5% ESR

Guard inte 1/8	erval =	21	ζ.	Speed 3 dB l		4]	k	30	at F _d , dB n/h	8	k	Speed 3 o kn	iB
Modula- tion	Code rate	C/N _{min} dB	<i>F</i> _d , 3 dB Hz	470 MHz	770 MHz	C/N _{min} dB	Fd, 3 dB Hz	470 MHz	770 MHz	C/N _{min} dB	<i>F</i> _d , 3 dB Hz	470 MHz	770 MHz
QPSK	1/2	8	360	827	505	8.5	170	391	238	8.5	89	205	125
QPSK	2/3	11.5	310	712	435	12	140	322	196	11.5	74	170	104
16-QAM	1/2	13.5	270	620	379	13.5	130	299	182	14.5	67	154	94
16-QAM	2/3	17.5	200	460	281	17.5	100	230	140	18	50	115	70
64-QAM	1/2	19	180	414	252	19	89	205	125	19.5	42	97	59
64-QAM	2/3	23.5	110	253	154	24	60	138	84	24.5	28	64	39
64-QAM	3/4	26.5	100	230	140	27	49	113	69	27.5	23	53	32

a) Non diversity case

Guard inte	erval =			Speed	at F.		-	Speed				Speed		
	$\frac{1}{8}$		2 k		3 dB km/h		4 k		3 dB km/h		8 k		3 dB km/h	
Modula- tion	Code rate	C/N _{min} dB	<i>F</i> _d 3 dB Hz	470 MHz	770 MHz	C/N _{min} dB	<i>F_d</i> , 3 dB Hz	470 MHz	770 MHz	C/N _{min} dB	<i>F_d</i> , 3 dB Hz	470 MHz	770 MHz	
QPSK	1/2	4	420	965	589	4	210	483	295	4	100	230	140	
QPSK	2/3	6	390	896	547	6.5	190	437	266	6	96	221	135	
16-QAM	1/2	9	350	804	491	9	170	391	238	9.5	85	195	119	
16-QAM	2/3	12	280	643	393	12	140	322	196	12	70	161	98	
64-QAM	1/2	14.5	230	529	323	14.5	110	253	154	15	57	131	80	
64-QAM	2/3	18.5	180	414	252	18	91	209	128	18.5	43	99	60	
64-QAM	3/4	20	160	368	224	20	79	182	111	20	38	87	53	

TABLE 89 (end)

b) Diversity case

The performance in a mobile channel depends to a large extent on the design of the ISDB-T receiver. Using receivers designed for mobile reception may lead to a higher level of performance.

5.5 Receiver noise figure

The values of the noise figure are 5 dB in the VHF band and 7 dB in the UHF band for ISDB-T receivers.

Appendix 1 to Annex 3

Calculation of minimum field strength and minimum median equivalent field strength

The minimum field strength and minimum median equivalent field-strength values were calculated by using the following equations:

$$P_{n} = F + 10 \log (k T_{0} B)$$

$$U_{N} = P_{n} + 120 + 10 \log R$$

$$P_{s \min} = C/N + P_{n}$$

$$U_{\min} = P_{s \min} + 120 + 10 \log R$$

$$A_{a} = G + 10 \log (1.64 \lambda^{2}/4 \pi)$$

$$\varphi_{\min} = P_{s \min} - A_{a} + L_{f}$$

$$E_{\min} = \varphi_{\min} + 120 + 10 \log (120 \pi)$$

$$= \varphi_{\min} + 145.8$$

$$= P_{s \min} - A_a + L_f + 120 + 10 \log (120 \pi)$$

$$= U_{\min} -10 \log R - G - 10 \log (1.64 \lambda^2/4 \pi) + L_f + 10 \log (120 \pi)$$

$$= U_{\min} + 20 \log (2 \pi/\lambda) - G + L_f$$

$$= U_{\min} + K - G + L_f \qquad K = 20 \log (2 \pi/\lambda)$$

$$E_{med} = E_{\min} + P_{mnn} + C_1 \qquad \text{for rooftop level fixed reception}$$

$$E_{med} = E_{\min} + P_{mnn} + C_1 + L_h \qquad \text{for portable outdoor and mobile reception}$$

$$E_{med} = E_{\min} + P_{mmn} + C_1 + L_h + L_b \qquad \text{for portable indoor and mobile hand-held reception}$$

$$C_l = \mu \cdot \sigma_l$$

$$\sigma_l = \sqrt{\sigma_b^2 + \sigma_m^2}$$

where:

 P_n : receiver intrinsic noise power (dBW)

F : receiver noise figure (dB)

k: Boltzmann's constant ($k = 1.38 \times 10^{-23}$ (J/K))

 T_0 : absolute temperature ($T_0 = 290$ (K))

B: receiver noise bandwidth ($B = 5.57 \times 10^6$, 6.50×10^6 , 7.43×10^6 (Hz))

 U_n : receiver noise input voltage (dB(μ V))

R: antenna inpedance $(R = 73.1(\Omega))$

 $P_{s min}$: minimum receiver input power (dBW)

$$U_{min}$$
: minimum receiver input voltage (dB(μ V))

C/N: RF S/N at the receiver input required by the system (dB)

 A_a : effective antenna aperture (dBm²)

G: antenna gain related to half dipole (dBd)

 λ : wavelength of signal (m)

 φ_{min} : minimum pfd at receiving place (dB(W/m²))

 L_f : feeder loss (dB)

 E_{min} : equivalent minimum field strength at receiving place (dB(μ V/m))

K: conversion factor (dB)

 E_{med} : minimum median equivalent field strength, planning value (dB(μ V/m))

 P_{mmn} : allowance for man-made noise (dB) (median values of man-made noise power are shown in Recommendation ITU-R P.372-10)

- L_h : height loss (reception point at 1.5 m above ground level) (dB)
- L_b : building or vehicle entry loss (dB)
- C_l : location correction factor (dB)
- σ_t : total standard deviation (dB)
- σ_m : standard deviation macro-scale ($\sigma_m = 5.5$ (dB))
- σ_b : standard deviation building entry loss (dB)
- μ : distribution factor being 0.52 for 70%, 1.28 for 90%, 1.64 for 95% and 2.33 for 99%.

Annex 4

Planning criteria for DTMB digital television systems in the VHF/UHF bands

1 Protection ratios for DTMB wanted digital terrestrial television signals

Tables 90 to 92, 93 to 95 show protection ratios for the DTMB wanted signals interfered with:

- by DTMB signals;
- by analogue terrestrial television signals;

respectively.

1.1 Protection of a DTMB signal interfered with by a DTMB signal

TABLE 90

Co-channel protection ratios (dB) for a DTMB 8 MHz signal interfered with by a DTMB signal

Modulation	Code rate	Gaussian channel	Ricean channel	Rayleigh channel
4-QAM	0.4	3	4	5
16-QAM	0.4	9	10	11
64-QAM	0.4	15	16	17
4-QAM	0.6	5	6	8
16-QAM	0.6	12	13	15
64-QAM	0.6	17	18	20
4-QAM-NR	0.8	3	4	5
4-QAM	0.8	7	8	13
16-QAM	0.8	14	15	19
32-QAM	0.8	16	17	21
64-QAM	0.8	22	23	29

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Protection ratios are given for three types of propagation channels (i.e. Gaussian, Ricean and Rayleigh). For fixed and portable reception, the values relevant to the Ricean and Rayleigh channels, respectively, should be adopted.

TABLE 91

Modulation	Code rate	Gaussian channel	Ricean channel	Rayleigh channel
4-QAM	0.4	-36	-35	-33
16-QAM	0.4	-31	-30	-29
64-QAM	0.4	-27	-26	-24
4-QAM	0.6	-33	-33	-31
16-QAM	0.6	-30	-28	-27
64-QAM	0.6	-23	-23	-22
4-QAM-NR	0.8	-36	-35	-33
4-QAM	0.8	-30	-30	-27
16-QAM	0.8	-28	-27	-24
32-QAM	0.8	-25	-24	-22
64-QAM	0.8	-20	-20	-17

Protection ratios (dB) for a DTMB 8 MHz signal interfered with by a DTMB 8 MHz signal in the lower (N - 1) and upper (N + 1) adjacent channels

The protection ratio is given in dB and applies to both continuous and tropospheric interference.

The values given apply to the case where wanted and unwanted DTMB signals have the same channel width. Other combinations of channel width need further studies.

It is known from measurements of existing receivers that they permit lower protection ratios.

But for planning purposes it is an advantage to have this value.

1.2 Protection of DTMB signal interfered with by analogue terrestrial television

1.2.1 Protection from co-channel interference

TABLE 92

Modulation	Code rate	Gaussian channel	Ricean channel	Rayleigh channel
4-QAM	0.4	-8	-7	-6
16-QAM	0.4	-6	-5	-3
64-QAM	0.4	-4	0	2
4-QAM	0.6	-5	-4	-3
16-QAM	0.6	-4	-2	3
64QAM	0.6	2	5	10
4-QAM-NR	0.8	-8	-7	-6
4-QAM	0.8	-1	0	1
16-QAM	0.8	2	3	5
32-QAM	0.8	4	5	7
64-QAM	0.8	13	14	20

Co-channel protection ratios (dB) for DTMB 8 MHz signal interfered with by analogue television (non-controlled frequency condition) signals

According to the available measurements, the same protection ratio values are applicable for singleand multi-carrier modes.

1.2.2 Protection from lower adjacent channel (N - 1) interference

TABLE 93

Protection ratios (dB) for lower adjacent channel (N - 1) interference for DTMB 8 MHz signal interfered with by analogue television signals including sound

Wanted	signal	Unwanted signal PAL-D				
Constellation	Code rate	Gaussian channel	Ricean channel	Rayleigh channel		
4-QAM	0.4	-46	-45	-41		
16-QAM	0.4	-46	-45	-41		
64-QAM	0.4	-46	-45	-41		
4-QAM	0.6	-46	-45	-41		
16-QAM	0.6	-46	-45	-41		
64-QAM	0.6	-42	-42	-40		
4-QAM-NR	0.8	-46	-45	-41		
4-QAM	0.8	-46	-45	-41		
16-QAM	0.8	-44	-43	-38		
32-QAM	0.8	-39	-39	-33		
64-QAM	0.8	-39	-37	-30		

All values are applicable for fixed and portable reception conditions.

1.2.3 Protection from upper adjacent channel (N + 1) interference

TABLE 94

Protection ratios (dB) for upper adjacent channel (N + 1) interference for DTMB 8 MHz signal interfered with by an analogue television signal

Wanted	signal	Unwanted signal PAL-D (dB)				
Constellation	Code rate	Gaussian channel	Ricean channel	Rayleigh channel		
4QAM	0.4	-53	-52	-51		
16QAM	0.4	-51	-50	-49		
64QAM	0.4	-47	-46	-45		
4QAM	0.6	-53	-52	-51		
16QAM	0.6	-49	-48	-46		
64QAM	0.6	-43	-43	-40		
4QAM-NR	0.8	-53	-52	-51		
4QAM	0.8	-50	-49	-43		
16QAM	0.8	-45	-44	-40		
32QAM	0.8	-43	-42	-37		
64QAM	0.8	-38	-36	-30		

2 Protection ratios for wanted analogue terrestrial television signals interfered with by unwanted DTMB 8 MHz signals

Tables 95 to 98 show protection ratios for a wanted analogue television signal interfered with by a DTMB signal.

2.1 Protection of wanted vision signals interfered with by DTMB 8 MHz signal

In this section, the protection ratios for an analogue wanted signal compatible fully compatible with Chinese Standard GB3174-1995 interfered by an unwanted DTMB signal relate only to the interference to the vision signal.

2.1.1 **Protection from co-channel interference**

TABLE 95

Protection ratios (dB) for a wanted analogue vision signal interfered with by an unwanted DTMB 8 MHz signal

Wanted signal:	Unwanted signal: DTMB, 8 MHz				
analogue system	Tropospheric interference	Continuous interference			
PAL-D	34	40			
D/SECAM	34	40			

2.1.2 Protection from lower adjacent channel interference

TABLE 96

Protection ratios (dB) for a wanted analogue vision signal interfered with by DTMB 8 MHz signal (lower adjacent channel)

Wanted signal:	Unwanted signal: DTMB 8 MHz (lower adjacent channel)				
analogue system	Tropospheric interference	Continuous interference			
PAL-D	-9	-5			
D/SECAM	-13	-9			

2.1.3 Protection from upper adjacent channel interference

TABLE 97

Protection ratios (dB) for a wanted analogue vision signal interfered with by DTMB 8 MHz signal (upper adjacent channel)

Wanted signal:	Unwanted signal: DTMB 8 MHz (upper adjacent channel)				
analogue system	Tropospheric interference	Continuous interference			
PAL-D	-8	-5			
D/SECAM	-15	-12			

2.1.4 **Protection from image channel interference**

TABLE 98

Protection ratios (dB) for a wanted analogue vision signal interfered with by a DTMB 8 MHz signal (image channel)

Wanted signal:	Unwanted signal: DTMB 8 MHz (N + 9 channel)				
analogue system	Tropospheric interference	Continuous interference			
PAL-D	-19	-15			
D/SECAM	-16	-11			

2.1.5 Protection from adjacent and overlapping channel interference

TABLE 99

Protection ratios (dB) for an analogue vision signal interfered with by a DTMB signal (overlapping channels)

Centre frequency of the unwanted DTMB signal	Protecti	on ratio
minus the vision carrier frequency of the wanted analogue television signal (MHz)	Tropospheric interference	Continuous interference
-8.25	-20	-15
(<i>N</i> -1) -5.25	-13	-9
-4.75	-11	-4
-4.25	5	13
-3.75	24	30
-3.25	29	36
-2.25	33	39
-1.25	34	40
(<i>N</i>) 2.75	34	40
4.75	34	40
5.75	30	37
6.75	27	34
7.75	25	32
8.75	5	11
(<i>N</i> +1) 10.75	-15	-12
12.75	-15	-12

3 Minimum field strengths for DTMB fixed reception

The formula for calculating minimum field strength is given in Appendix 1.

Frequency (MHz)	65			200	200		500		700			
Receiver noise figure, F (dB)	5	5	5	5	5	5	7	7	7	7	7	7
Receiver carrier/noise ratio ⁽¹⁾ (C/N) (dB)	8	14	20	8	14	20	8	14	20	8	14	20
Feeder loss Af (dB)	1	1	1	3	3	3	3	3	3	5	5	5
Antenna gain, G (dB)	3	3	3	5	5	5	10	10	10	12	12	12
Minimum field strength for fixed reception, Emin $(dB(\mu V/m))^{(1)}$	17	23	29	27	33	39	33	39	45	35	41	47

TABLE 100

Calculation of minimum field strength DTMB 8 MHz system

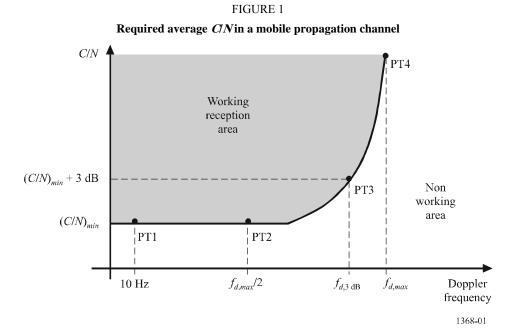
⁽¹⁾ For formula, see Appendix 1.

4 Minimum median field strength for mobile DTMB reception

The equations for calculating the minimum median field strength are given in Appendix 1 to this Annex. The input values to the calculation are found in this section and in Appendix 1. Mobile reception should be calculated with a location probability of 99%.

4.1 Required average *C*/*N* for mobile reception

For a given DTMB mode the required average C/N for a certain quality level is a function of Doppler frequency only, and a graph like the one presented in Figure 1.



The minimum required average C/N values (C/N_{min}) , Doppler frequency for an average C/N equal to $C/N_{min} + 3$ dB and the maximum Doppler (speed) limits for mobile reception without diversity are given in Table 100. The speed limits for $C/N_{min} + 3$ dB are given for four frequencies (65 MHz,

200 MHz, 500 MHz and 700 MHz). The average C/N value, C/N_{min} + 3 dB, is suitable for calculation of required field strength. The values are based on the typical channel profile "typical urban" shown in Table 101. Quality criterion is the subjective failure point (SFP) corresponding to erroneous seconds ratio, -ESR = 5% with 5 minutes.

TABLE 101

Required average C/N, speed limits for mobile reception for the non-diversity case

	~ .	-	C/Nmin	F_d at		Speed at F_d	, 3 dB (km/h)
Modulation	Code rate	Bit rate (Mbit/s)	(dB) at Cf = 762 MHz, Fd = 70 Hz	762 MHz, + 3 Db		200 MHz	500 MHz	700 MHz
4-QAM	0.4	5.414	6	162	2 692	875	350	250
16-QAM	0.4	10.829	12	134	2 2 2 2 6	724	290	207
4-QAM	0.6	8.122	10	148	2 459	799	320	228
16-QAM	0.6	16.243	17	116	1 927	626	251	179
4-QAM-NR	0.8	5.414	6	162	2 692	875	350	250
4-QAM	0.8	10.829	14	123	2 044	664	266	190

TABLE 102

Channel profile for measurement of required average *C/N* for mobile reception of DTMB reception "typical urban"

Tap number	Delay (µs)	Power (dB)	Doppler category
1	0	-3	Ricean
2	0.2	0	Ricean
3	0.5	-2	Ricean
4	1.6	-6	Ricean
5	2.3	-8	Ricean
6	5	-10	Ricean

The performance in a mobile channel depends to large extent on the design of the DTMB receiver. Improvements may be achieved with receivers particularly designed for mobile reception.

4.2 Receiver noise figure

Noise figure of 7 dB is for integrated vehicle mobile receivers.

Appendix 1 to Annex 4

Calculation of minimum field strength and minimum median equivalent field strength

The minimum field strength and minimum median equivalent field strength values calculated using the following equations:

• •			
P_n	=	$F + 10 \log (k T_0 B)$	
P _{s min}	=	$C/N + P_n$	
A_a	=	$G + 10 \log (1.64 \lambda^2 / 4 \pi)$	
ϕ_{min}	=	$P_{s\min} - A_a + L_f$	
E_{min}	=	$\varphi_{min} + 120 + 10 \log (120 \pi)$	
	=	$\varphi_{min} + 145.8$	
E_{med}	=	$E_{min} + P_{mmn} + C_1$	for roof top level fixed reception
E_{med}	=	$E_{min} + P_{mmn} + C_1 + L_h$	for portable outdoor and mobile reception
E_{med}	=	$E_{min} + P_{mmn} + C_1 + L_h + L_b$	for portable indoor and mobile hand-held reception
C_1	=	$\mu \cdot \sigma_t$	
σ_t	=	$\sqrt{\sigma_b^2 + \sigma_m^2}$	

 P_n : receiver noise input power (dBW)

- F: receiver noise figure (dB)
- k: Boltzmann's constant ($k = 1.38 \times 10^{-23}$ (J/K))
- T_0 : reference temperature expressed in absolute temperature ($T_0 = 290$ (K))
- *B*: receiver noise bandwidth ($B = 7.56 \times 10^6$ (Hz))

 $P_{s min}$: minimum receiver input power (dBW)

C/N: RF S/N at the receiver input required by the system (dB)

- A_a : effective antenna aperture (dBm²)
- G: antenna gain related to half dipole (dBd)
- λ : wavelength of the signal (m)
- φ_{min} : minimum pfd at receiving place (dB(W/m²))
- L_f : feeder loss (dB)
- E_{min} : equivalent minimum field strength at receiving place (dB(μ V/m))
- E_{med} : minimum median equivalent field strength, planning value (dB(μ V/m))
- P_{mmn} : allowance for man-made noise (dB)
 - L_h : height loss (reception point at 1.5 m above ground level) (dB)
 - L_b : building or vehicle entry loss (dB)

- C_1 : location correction factor (dB)
- σ_t : total standard deviation (dB)
- σ_m : standard deviation macro-scale ($\sigma_m = 5.5$ (dB))
- σ_b : standard deviation building entry loss (dB)
- μ : distribution factor being 0.52 for 70%, 1.28 for 90%, 1.64 for 95% and 2.33 for 99%.

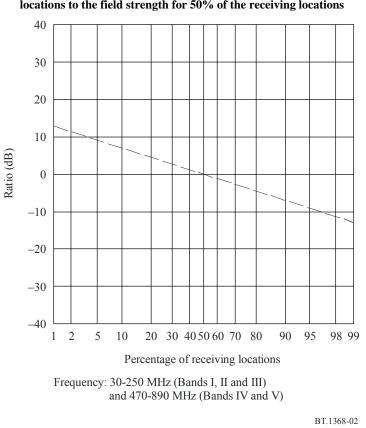
Annex 5

Other planning factors

1 Field strength distribution with location

It is to be expected that the distributions of field strength with location for digital television signals will not be the same as those applicable to analogue television signals. Recommendation ITU-R P.1546 includes the standard deviation for the analogue and for the digital case in Table 1, 2 and 3 for 100 MHz, 600 MHz and 2 000 MHz, respectively.

The results of propagation studies for digital systems are given in Fig. 2 for the VHF and UHF bands. The figure corresponds to a standard deviation of 5.5 dB. These results may also be used to derive propagation prediction curves for location percentages other than 50%. Refer to Recommendation ITU-R P.1546 for the location percentages other than 50% for analogue and digital systems, where the digital system bandwidth is greater than 1.5 MHz.



Ratio (dB) of the field strength for a given percentage of the receiving locations to the field strength for 50% of the receiving locations

FIGURE 2

2 Reception using portable equipment inside buildings and vehicles

2.1 Height loss: L_h

For land paths, the curves in Recommendation ITU-R P.1546 give field-strength values for a receiving antenna height above ground equal to the *representative height* of ground cover around the receiving antenna location. Subject to a minimum height value of 10 m, examples of reference heights are 20 m for an urban area, 30 m for a dense urban area and 10 m for a suburban area. (For sea paths, the notional value is 10 m.)

If the receiving antenna height is different from the representative height, a correction is applied to the field strength taken from the curves of Recommendation ITU-R P.1546 according to a procedure given in the Recommendation.

2.2 Building entry loss: *L*_b

Losses due to penetration into a building depend significantly on the building material, angle of incidence and frequency. Consideration should also be given as to whether reception is in an interior room or in one located near an exterior wall. The building entry loss is defined as the difference (dB) between the mean field strength inside a building at a given height above ground level and the mean field strength outside the same building at the same height above ground level. Whilst no single comprehensive formula is available for computing building entry loss, useful statistical information based on measured losses in several types of building, at frequencies from about 500 MHz to 5 GHz, are given in Recommendation ITU-R P.679. Once inside the building, propagation loss due to walls and floors are dealt with in Recommendation ITU-R P.1238.

A large spread of building entry losses have been measured. Table 103 gives three classes of the relative possibilities to achieve indoor reception and the corresponding mean and standard deviation values of the building entry losses, for the same outdoor field strength, based on UHF measurements.

TABLE 103

Building entry loss variations in the UHF Bands IV/V

Classification of the relative possibilities to achieve indoor reception	Mean building entry loss (dB)	Standard deviation (dB)
High	7	5
Medium	11	6
Low	15	7

Examples of buildings with different relative possibilities to achieve indoor reception:

High:

- suburban residential building without metallized glass windows,

- room with a window on the exterior wall in an apartment in an urban environment.

Medium:

- exterior rooms in an urban environment with metallized glass windows,
- inner rooms in an apartment in an urban environment.

Low:

inner rooms in office buildings.

If more precise values based on local measurements are available, these could be used as a basis for planning a specific service.

2.3 Vehicle entry loss: L_v

For reception with a hand-held device inside a vehicle, the vehicle body loss should be taken into account. A typical vehicle entry loss for the UHF Bands IV/V, based on cellular radio experience, is 6 dB.

3 Receiving antenna discrimination

Information concerning the directivity and polarization discrimination of domestic receiving antennas is given in Recommendation ITU-R BT.419.

4 Antennas for portable and mobile receivers

4.1 Antennas for portable reception

A spread in antenna gain has been measured for different types of antenna. The following antenna gain values are typical:

Rec. ITU-R BT.1368-9

TABLE	104
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Antenna gain (dBd) for portable reception

Band	Gain (dBd)
VHF Band III	-2
UHF Band IV	0
UHF Band V	0

No polarization discrimination is expected.

4.2 Antennas for hand-held reception

The antenna in a small hand-held terminal has to be an integral part of the terminal construction and will therefore be small when compared to the wavelength. Current understanding of the design problem indicates that the worst-case antenna gain is in the lowest part of the UHF band. The antenna gain for three frequencies in the UHF band is given in Table 105. Nominal antenna gain between these frequencies can be obtained by linear interpolation.

TABLE 105

Antenna gain (dBd) for hand-held reception

Frequency (MHz)	Gain (dBd)
474	-12
698	-9
858	-7

Generally, no polarization discrimination is expected from this type of portable reception antenna and the radiation pattern in the horizontal plane is omnidirectional.

4.3 Antennas for mobile reception

The practical standard antenna for vehicle reception is 1/4 monopole, which uses the metallic roof as a ground plane. The antenna gain for conventional incident wave angles depends on the position of the antenna on the roof. For passive antenna systems the values in Table 106 can be expected.

TABLE 106

Antenna gain (dBd) for mobile reception

Band	Gain (dBd)
VHF Band III	-5
UHF Band IV	-2
UHF Band V	-1

The polarization discrimination is theoretically about 4 to 10 dB depending on the roof position of the antenna.

Annex 6

Subjective comparison method (SCM) with a reference interferer for assessment of protection ratios for analogue television systems

1 Introduction

Subjective methods for assessment of impairment grades involve extensive tests, are time consuming, require large numbers of observers and consider the full impairment grade range.

For assessing protection ratios only two fixed impairment types are necessary, approximately grade 3 for tropospheric and grade 4 for continuous, see Table 107.

This Annex gives a method of assessing protection ratios for wanted analogue TV systems based on the subjective comparison of the impairment of an interferer with that of a reference interferer. Usable and reliable results are produced with only a small number of observers and one still picture.

This subjective comparison method is appropriate for the evaluation of interference from any unwanted digital or analogue transmission system into a wanted analogue television channel. The application of a defined fixed reference interferer results in a reproducible set of figures with a low deviation (approximately ± 1 dB standard deviation). Only a small number of observers – three to five experts or non-experts – is necessary.

There are two reference interferers which may be used:

- sine-wave interference
- Gaussian-noise interferer.

Tests have shown that for unwanted digital television systems a noise reference interferer can improve the assessment decision by the observer. The use of noise reference interferer shows the same results as the defined sine-wave interferer. The disadvantage is that a more complicated test arrangement may be necessary. Further tests are necessary, especially by fixing the equivalent noise reference.

(For the time being the sine-wave reference interferer should be used until an agreement on a common test procedure and an agreement on a harmonized unified noise reference figure has been obtained.)

2 SCM for assessment of protection ratios using a sine-wave reference

2.1 General description

Figure 3 shows the test arrangement for the subjective comparison method with sine-wave interferer. The lower three blocks are the main signal path, the wanted video source, the television transmitter and the TV receiver under test. The reference video interferer is a simple sine-wave signal. The amplitude of the sine-wave generator is switchable between tropospheric interference and continuous interference. The unwanted RF interferer is added to the wanted signal path. The amplitude and frequency of the interferer are calculated from the RF reference interferer given in Recommendation ITU-R BT.655, Annex 1, § 2.3.

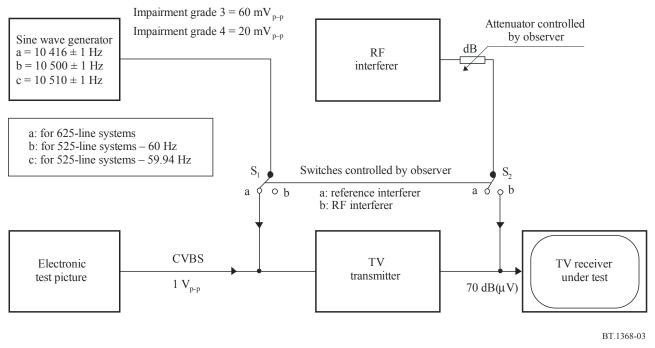


FIGURE 3

SCM for assessment of protection ratios

The intensity of the RF interferer can be changed with an attenuator controlled by the observer. The RF interferer is adjusted to produce the same impairment grade as the reference interferer by comparing the interfered pictures on the TV screen.

The RF protection ratio is the difference between the wanted and the unwanted signal levels at the receiver input. The test arrangement can be adjusted in such a way that the value in dB shown at the attenuation box gives, directly, the protection ratio.

2.2 Realization of the reference interferer

For 625-line systems the reference impairment levels are those which correspond to co-channel protection ratios of 30 dB and 40 dB with a frequency offset between the wanted and unwanted vision carriers close to two-thirds of the line frequency but adjusted for maximum impairment. The precise frequency difference is 10 416 Hz. These conditions approximate impairment grades 3 (slightly annoying) and 4 (perceptible, but not annoying) and apply to tropospheric (1% of time) and continuous interference (50% of time), respectively. The impairment grade of the given video baseband reference interferer is independent of the analogue television system and independent of the RF modulation parameters such as modulation polarity, residual carrier, etc.

The RF reference interferer can be realized as a simple sine-wave signal at baseband frequency as shown in Fig. 3. The sine-wave reference interferer has a fixed frequency of 10 416 Hz for 625-line systems or 10 500 Hz for 525-line systems –60 Hz and 10 510 Hz for 525-line systems –59.94 Hz, an amplitude of either 60 mV_{p-p} or 20 mV_{p-p} referring to a black-to-white level of 700 mV_{p-p} or a CVBS level of 1 V_{p-p}. These amplitudes correspond to the RF protection ratios of 30 dB and 40 dB respectively (2/3 line offset). The frequency stability of the sine-wave generator must be within ±1 Hz.

2.3 Test conditions

Wanted video signal: only an electronic test picture is required (e.g. FuBK, Philips or others).

Viewing conditions: as given in Recommendation ITU-R BT.500.

Viewing distance:five times the picture height.Test receiver:up to five different domestic sets, not older than five years, for co-channel
measurements a professional receiver can be used.Receiver input signal: $-39 \text{ dBm} (70 \text{ dB}(\mu \text{V}) \text{ at } 75 \Omega)$.Observers:five observers, experts or non-experts, are necessary. For initial tests less than
five observers are possible. Each single test should be made with one

observer only. Observers should be introduced to the method of assessment.

2.4 Presentation of the results

The results should be presented together with the following information:

- mean and standard deviation of the statistical distribution of the protection ratio values;
- test configuration, test picture, type of picture source;
- number of observers;
- reference interferer type;
- the spectrum of the unwanted signal (RF interferer), including the out-of-channel range;
- the used RF level for the wanted signal at the receiver input (for domestic receivers an input voltage of -39 dBm (70 dB(μ V) at 75 Ω should be used);
- when domestic sets are used, type, display size and year of production.

3 Table of important parameters

TABLE 107

Basic terms and relations for the SCM

Quality impairment	Grade 3	Grade 4
Interference type	Tropospheric	Continuous
Time allowance	1% to 5% of time	50% of time
Subjective impairment	Slightly annoying	Perceptible, but not annoying
Reference interferer (mV _{p-p})	60	20
RF protection ratio (dB)	30	40

Annex 7

Failure point assessment methods

1 Background

Initial studies of the protection ratios for the DVB-T system were based on a target BER of 2×10^{-4} measured between the inner and outer codes, before Reed-Solomon decoding. For the case of a noise-like interferer, this has been taken to correspond to a quasi-error-free (QEF) picture quality with the BER < 1×10^{-11} at the input of the MPEG-2 demultiplexer.

2 Subjective failure point (SFP) method for protection ratio measurements

For domestic receivers it may not be possible to measure the BER and therefore a new method called the SFP method has been proposed for protection ratio measurements in a unified manner. The quality criterion for protection ratio measurements is to find a limit for a just error-free picture at the TV screen. The RF protection ratio for the wanted DVB-T signal is a value of wanted-to-unwanted signal ratio at the receiver input, determined by the SFP method, and rounded to the next higher integer value.

The SFP method corresponds to the picture quality where no more than one error is visible in the picture for an average observation time of 20 s. The adjustment of the wanted and unwanted signal levels for the SFP method is to be carried out in small steps, usually in steps of 0.1 dB. For a "noise-like" interferer the difference in a value of wanted-to-unwanted signal ratio between the QEF method with a BER of 2×10^{-4} and the SFP method is less than 1 dB. Historically, protection ratio values for wanted digital TV signals are measured with a receiver input power of -60 dBm. Where possible, protection ratios for digital TV systems are derived from measurements using a range of signal levels.

It is proposed that the SFP method should be adopted for assessment of all DTTB systems. (For the digital system ISDB-T this method will be studied in Japan.)

Annex 8

Tropospheric and continuous interference

When using the protection ratios in planning, it is necessary to determine whether, in particular circumstances, the interference should be considered as tropospheric or continuous. This can be done by comparing the nuisance fields for the two conditions, the nuisance field being defined as the field strength of the interfering transmitter (at its pertinent e.r.p.) enlarged by the relevant protection ratio.

Thus, the nuisance field for continuous interference:

$$E_C = E(50, 50) + P + A_C$$

and the nuisance field for tropospheric interference:

$$E_T = E(50, t) + P + A_T$$

where:

E(50, t): field strength (dB(μ V/m)) of the interfering transmitter, normalized to 1 kW, and exceeded during t% of the time

- P: e.r.p. (dB(1 kW)) of the interfering transmitter
- A: protection ratio (dB)
- *C* and *T*: continuous and tropospheric interference, respectively.

The protection ratio for continuous interference is applicable when the resulting nuisance field is stronger than that resulting from tropospheric interference, that is, when $E_C > E_T$.

This means that A_C should be used in all cases when:

$$E(50, 50) + A_C > E(50, t) + A_T$$