



Report ITU-R BT.2467-0
(07/2019)

Methods for the evaluation of the quality of service of second generation DTTB systems

BT Series
Broadcasting service
(television)



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REPORT ITU-R BT.2467-0

Methods for the evaluation of the quality of service of second generation DTTB systems

(Question ITU-R 132-4/6)

(2019)

Objective

The objective of this Report is to introduce methods that have been used for evaluating the quality of service of 2nd generation digital television broadcasting systems using the VHF and UHF bands.

Recommendation ITU-R BT.1735 [1] provides two methods for digital objective reception quality assessment for DVB-T, one for multi-frequency networks (MFN) and one for single frequency networks (SFN).

This Report gives some details about the relevant parameters for DVB-T2 and the results of some measurements, in order to identify a possible method for objective reception quality assessment for this DTTB system.

The final goal would be to obtain criteria that, even without knowing exactly all the useful signals and the interferences¹ but looking only at a limited number of parameters, could indicate if a requested level of *C/I* is satisfied and quantify the available “margin” with respect to the QEF threshold.

Measurements in the field should be performed in a known controlled order to validate the proposed method(s) in real world environments.

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¹ E.g. using “impulse response” or similar methods, in case of SFN.

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PART 1

Study for the definition of a method for the assessment of DVB-T2 reception quality

1 Introduction

Laboratory and field measurements were done by different companies (EiTowers/Elettronica Industriale (I), IRT (D), Rai Way (I), TDF (F)) in order to define a method for assessment of DVB-T2 reception quality.

Different tests have been carried out in order to identify a possible method for objective reception quality assessment. The DVB-T2 system parameters, MER, BER Before LDPC decoder, BER Before BCH (outer) decoder, and the Number of LDPC Iterations have been investigated and a criterion based on the evaluation of MER has been established. The starting point of this method is to indicate if a requested level of C/I is satisfied and to provide the value of the available margin above the threshold point of the QEF signal. In this Report the description of the technique, laboratory tests and results of measurements in service area are reported.

2 Assumptions for DVB-T2

DVB-T2 offers additional possibilities with respect to DVB-T: for example, a selection of FFT-variants (from 1K to 32k), different modulation schemes (QPSK, ..., 256 QAM), Guard Intervals (1/128, ..., 1/4) and the possibility to use different Physical Layer Pipes² (PLPs).

The parameters used in Recommendation ITU-R BT.1735 for the assessment of the quality of service, BER Before Viterbi and BER Before Reed Solomon, are not available for DVB-T2 [2]. Similar parameters, BER Before LDPC (inner) decoder, BER Before BCH (outer) decoder and the Number of LDPC Iterations in DVB-T2 could be used for this purpose. The method for digital objective reception quality and for evaluation of quality of service performance has to take this into account.

The “quality of coverage” could be regarded as an “operative margin” with respect to the “picture failure point” because there is no smooth degradation of the received signal quality at the failure point, in particular in case of DVB-T2 reception (see § 4.5.10 of [3]). In fact, this “margin” gives an idea of “how many dB” the signal is above the “picture failure point”.

This margin depends on the received field strength, E, and on the possible presence of interferences. It is important to point out that this study is carried out for a fixed roof-top scenario in the case of MFN and SFN. If the received level is too low, the noise might overcome the interference and, in this case, a requirement on the received field strength E remains valid to qualify the assessment of the DVB-T2 received signal.

The described criteria to evaluate the margin assume that all relevant parameters (RF level, BER, MER, etc.) are available. In this Annex, no indications are given on the method to perform the measurements of these parameters. Finally, the margin could be also considered as an indicator of the quality of the received signal and of the quality of the coverage for a specific receiving condition in a given location.

² Each PLP may require a different C/N and, therefore, may have a different level of “margin” at any receiving point.

3 Overview on the reference parameters

This section describes the reference parameters that have been considered in this study and have to be measured “on field” for DVB-T2 systems.

Field strength (level), E

The received field E should be $>E_{\text{med}}$, where E_{med} is the sum of E_{min} plus an appropriate additional “location correction factor”.

Minimum field strength, E_{min} , is the minimum signal level needed to overcome the noise. It represents the sensitivity of the receiver plus other contributions depending on the feeder loss, on the antenna gain, on the noise figure of the receiver, on C/N , on the frequency, on the modulation scheme, etc. (see §§ 3.1, 3.2 and 3.3 of [4]).

If the standard deviation is 5.5 dB, the “location correction factor” to be used for coverage predictions for fixed reception is 9 dB for 95% of locations covered and 3 dB for 70% of locations.

In [1], E_{med} is also indicated as E_{xx} . In this case, E_{xx} may represent the planning value for the percentage of location for the wanted service chosen by administrations (e.g. E_{95} indicates the field strength planning value to have 95% of the location covered and includes the 9 dB margin to the minimum value E_{50}).

BER Before LDPC (inner) decoder

This value of BER is calculated before the LDPC decoder and depends on the transmission channel and not on the codes (FEC). It is affected by the receiving conditions and by the occurrences of interferences. In case of SFN, the impulse response analysis gives the details of the amplitudes and the relative delays of each received signal coming from the transmitters of the SFN and helps in detecting possible interferences.

BER Before BCH (outer) decoder

This BER is calculated after the LDPC decoder (or before the BCH decoder) and, therefore, depends on the mod-codes. A value of 1E-7 is required to have the reception of the video without errors or visible “artefacts” (see Table 5.1 of [5]) but the transition to the picture failure point is very fast.

Thus, this parameter gives a precise measure of the possibility to receive and decode the DVB-T2 signal, but it is possible to use it for the evaluation of the quality of signal due to its fast transition from the perfect reception to the picture failure point.

Number of LDPC Iterations

As indicated in ETSI TR 101 290 [6], this measurement:

“Gives an in-service indication of the quality of the received signal and the computational resources activated for the LDPC decoder. Since the results of these measurements are largely dependent on the actual LDPC decoder implementation, results can only be compared when taken from the same test instrument”

This parameter could be used in the assessment of the service quality but its dependency on the specific LDPC decoder implementation limits its application.

MER (Modulation Error Ratio)

MER is described in [1] and in [5]

As indicated in [6], MER is measured:

“To provide a “figure of merit” for L1 Signalling data³ and each PLP⁴ of the T2 signal, typically at a transmitter output (for assessing the quality of the transmitted signal) or in a fixed location in a SFN for identifying severe distortions in the set-up of the transmitters forming the SFN.”

“The sensitivity of the measurement, the typical magnitude of measured values and the units of measurement combine to give MER an immediate familiarity for those who have previous experience of C/N or SNR measurement.

MER can be regarded as a form of Signal-to-Noise ratio measurement that will give an accurate indication of a receiver's ability to demodulate the signal, because it includes not just Gaussian noise, but all other uncorrectable impairments of the received constellation as well.

If the only significant impairment present in the signal is Gaussian noise then MER and SNR are equivalent.”

Therefore, MER gives an indication⁵ of the C/I , e.g. expressed in dB.

As described in [6], MER is measured before PLP selection, i.e. before LDPC decoding, and so it does not depend on the adopted mod-code.

At this regard, practical measurements of DVB-T2 signals shows a non-perfect linearity of MER with respect to the receiving conditions (C/N or C/I)⁶. Furthermore, and exactly as expected, when one (or more) PLP is under its “failure point” but it is still possible to decode L1, the measured MER of this PLP is not available while MER for L1 is given.

Finally, in case of SFNs, MER depends also on the number of the received paths, their relative delays and attenuations.

Therefore, MER can be used for the evaluation of the quality of service but, the knowledge of some other additional parameters is required in order to have a proper assessment. In § 4.2 some SFN measurements are described for this purpose.

³ The Layer-1 (L1) signalling has two main functions. First, it provides receiver a means for fast signal detection and hence enables fast signal scanning. Secondly, it provides all information that receiver needs to access the Layer-2 signalling and the services themselves within the current (and possibly also the next) frame.

The L1 signalling is divided into L1-pre signalling and L1-post signalling. The modulation and code rate of the L1-pre signalling is BPSK 1/2 and the number of signalling bits in L1-pre is constant. The number of signalling bits in L1-post signalling depends on the number of PLPs, number of auxiliary streams, the use of FEFs and the possible future use of TFS. The L1-post signalling can be modulated using BPSK, QPSK, 16-QAM or 64-QAM. The FEC code rate is always 1/2. The modulation for the L1-post signalling is chosen so that the L1 signalling is always more robust than any PLP.

⁴ MER of PLP is measured at interface C2 (i.e. after equalisation), as described in [6] and it is not dependent from the modulation and code (FEC).

⁵ The Protection Ratio PR (C/I) is the difference between the wanted and unwanted signal, given in dB. If no interferers are present, only noise is considered as the unwanted signal and C/I becomes C/N . (see Recommendation ITU-R SM.1875).

⁶ Document [6A/352](#) “The use of MER to assess impact of anomalous propagations on co-channel interference”.

4 Description of the laboratory measurements done to define the method

Laboratory measurements were done by different companies (EiTowers/Elettronica Industriale (I), IRT (D), Rai Way (I), TDF (F)) in order to simulate the typical conditions of reception, especially for SFNs, where many signals may be present inside or outside the guard interval, together with interferences external to the SFN.

The measurement system included a multi-standard signal generator with Noise and Fading simulator and a reference radio receiver with DVB-T2 real-time signal analysis. The “Indirect objective and subjective quality measurement procedure” (see [7]) was also used making measurements and watching the decoded video for 30 seconds. The embedded measurements of BER before BCH (or after LDPC) provided by the receiver was adopted to identify the failure point.

Two main values of level at the input of the receiver were used: -60 dBm (see [8]) and -50 dBm (see [7]). The results obtained with these two values are comparable.

In addition, the behaviour of the system with lower levels of the useful signal at the input of the receiver was also measured, when the effect of the (Gaussian) noise became relevant.

Most tests were carried out at 610 MHz (Channel 38) with some specific trials having been performed in Band III.

A system with two different code rates ($2/3$ and $3/5$) was considered:

- FFT: 32k not extended
- Pilot pattern: PP2
- Guard Interval (GI): $1/16$ ($224\ \mu s$)
- Modulation: 256 QAM.

This system could be adopted for a fixed reception SFN, replacing a typical DVB-T mode (64 QAM, GI $1/4$, code rates $3/4$ and $2/3$ respectively, see [3]). A configuration with Pilot Pattern PP2 rather than PP4 was selected due to smoother transition in presence of signals arriving outside the GI. The results for these two pilot patterns⁷ are comparable.

Results for some other system variants are presented in the Annexes.

4.1 Description of the laboratory measurements (MFN)

For MFN purposes, the values of the relevant parameters were measured in two different ways: decreasing the input level (“noise limited”) and arising the noise (“interference limited”). This latter method could also be used in the simulation of a co-channel interference in SFNs when only a single signal is perceivable.

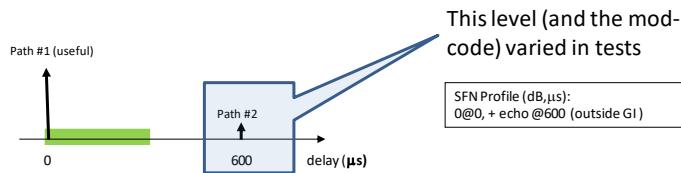
4.2 Description of the laboratory measurements (SFN)

For SFN purposes, different simulations have been tested in order to cover some of the possible scenarios.

Figure 1 shows the case with only one signal inside the GI plus an additional one outside it.

⁷ There is only a little difference (of the order of 0.5 dB) in terms of C/N and Sensitivity in favour of PP4.

FIGURE 1
Example of one SFN profile used for the tests



In this test, the amplitude of the path #2 was changed and the *C/I* varied accordingly.

Figure 2 shows a more complex situation where more than one signal was present inside the GI. In this case, the amplitude and the delay of the signal outside the GI vary. Figure 3 is an example of measured impulse response for this SFN profile, without interferences.

FIGURE 2
A second example of SFN profile

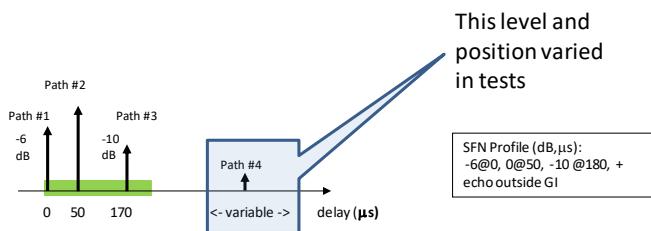
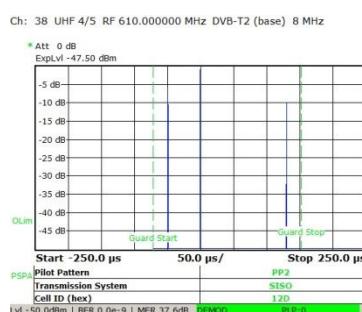


FIGURE 3
Example of typical measured impulse response for the useful path in Fig. 2



In detail, SFN measurements have been performed in the following conditions:

- SFN with 1, 2, 3 and 4 useful paths (inside GI) and one interfering path (outside GI). For each of these configurations, the interference is placed at three different time distances: “near” the end of GI; just “before” the end of the equalization interval (Nyquist time); “far” from the end of GI.
- SFN with 2 useful paths with “comparable” value (2 dB) in order to simulate a measuring condition similar to “echo 0dB” and one interfering path.

The values of useful level, interference level, BER before LDPC, BER before LDPC, number of iterations, PLP MER and L1 MER were measured for each of the tested conditions.

The results are reported in Annex 2 to Part 1.

4.3 Description of some results of the laboratory measurements for the MFN

Tables 1.1 and 1.2 show the results of “noise limited”⁸ and “interference limited” measurements for one of the considered DVB-T2 modes (code 2/3).

In these examples, MER at failure point is 18.3 dB for both cases. In the case of “interference limited” a level of -50 dBm at the input of the receiver was used and measurements done at lower input levels, e.g. -65, -68, -70 dBm, confirmed this result (see Table 2). For values lower than -70 dBm this MER value is increased by a fraction of a dB (i.e. from 18.3 to 18.9 dB).

TABLE 1.1

Noise limited
(Typical measured values)

| Level (dBm) | Iter numb. | BER Before LDPC | MER PLP (dB) | margin (dB) |
|------------------|---------------|-----------------------|-----------------|----------------|
| -30 | 2.5 | 5.9E-05 | 43.5 | |
| -40 | 2.5 | 5.9E-05 | 43.2 | |
| -50 | 2.5 | 5.9E-05 | 41.5 | |
| -55 | 2.6 | 5.9E-05 | 38.8 | |
| -60 | 2.7 | 6.1E-05 | 34.8 | |
| -61 | 2.8 | 6.2E-05 | 33.9 | |
| -62 | 2.8 | 6.5E-05 | 33 | |
| -63 | 2.8 | 7.4E-05 | 32 | |
| -64 | 2.9 | 1.0E-04 | 31.1 | |
| -65 | 3 | 1.9E-04 | 30.2 | |
| -66 | 3.1 | 5.2E-04 | 29.2 | |
| -67 | 3.5 | 1.3E-03 | 28.2 | |
| -68 | 3.7 | 3.0E-03 | 27.2 | |
| E _{95%} | | | | 9 |
| -69 | 4.3 | 6.2E-03 | 26.2 | |
| -70 | 4.8 | 1.0E-02 | 25.3 | |
| -71 | 5.2 | 1.7E-02 | 24.3 | |
| -72 | 6 | 2.6E-02 | 23.2 | |
| ... | ... | ... | ... | |
| ... | ... | ... | ... | |
| E _{70%} | | | | 3 |
| -75 | 9.5 | 5.0E-02 | 21 | |
| -76 | 11.8 | 6.4E-02 | 19.9 | |
| -77 | 16 | 7.8E-02 | 18.9 | |
| E _{50%} | | | | 0 |
| -78 | 23 | 8.7E-02 | 18.3 | |
| -79 | ... | ... | ... | |

TABLE 1.2

Interference limited
(Level = -50 dBm)

| C/I (dB) | Iter numb. | BER Before LDPC | MER PLP (dB) | margin (dB) |
|--------------|---------------|-----------------------|-----------------|----------------|
| Add. Noise=0 | 2.5 | 5.9E-05 | 41.5 | |
| 40 | 2.5 | 6.0E-05 | 36.9 | 20 |
| 39 | 2.6 | 6.1E-05 | 36.2 | 19 |
| 38 | 2.6 | 6.1E-05 | 35.4 | 18 |
| 37 | 2.6 | 6.1E-05 | 34.7 | 17 |
| 36 | 2.65 | 6.1E-05 | 33.9 | 16 |
| 35 | 2.7 | 6.5E-05 | 33 | 15 |
| 34 | 2.75 | 6.8E-05 | 32.2 | 14 |
| 33 | 2.8 | 8.9E-05 | 31.3 | 13 |
| 32 | 2.8 | 1.7E-04 | 30.4 | 12 |
| 31 | 2.9 | 4.0E-04 | 29.5 | 11 |
| 30 | 3.2 | 1.0E-03 | 28.5 | 10 |
| 29 | 3.4 | 2.4E-03 | 27.6 | 9 |
| 28 | 3.8 | 4.8E-03 | 26.6 | 8 |
| 27 | 4.4 | 8.9E-03 | 25.6 | 7 |
| 26 | 4.9 | 1.5E-02 | 24.6 | 6 |
| 25 | 5.8 | 2.3E-02 | 23.6 | 5 |
| 24 | 6.6 | 3.2E-02 | 22.5 | 4 |
| 23 | 7.7 | 4.3E-02 | 21.4 | 3 |
| 22 | 9.3 | 5.5E-02 | 20.2 | 2 |
| 21 | 12.3 | 6.8E-02 | 19.1 | 1 |
| 20.5 | 14.9 | 7.5E-02 | 18.7 | 0.5 |
| 20 | 19.5 | 8.2E-02 | 18.3 | 0 |

⁸ Failure point is in line with Report ITU-R BT.2254, AWGN Profile sensitivity, -78.7 dBm (Ricean -78.4 dBm).

TABLE 2

**Results “interference limited” with different input levels
(Mode 32k, 1/16, PP2, 256 QAM, 2/3)**

| | | ref. MER (dB) | | 18.3 | | | | | | | | | | | | | | | | | | | | | | | | |
|----------|-------------|-----------------|--------------|-------------|--------------|-------------------------|-----------------|--------------|-------------|--------------|-------------------------|-----------------|--------------|-------------|--------------|-------------------------|-----------------|--------------|-------------|--------------|-------------------------|-----------------|--------------|-------------|--------------|-------------------------|--|--|
| | | level (dBm) | | -50 | | | | | -65 | | | | | -68 | | | | | -70 | | | | | -72 | | | | |
| C/I (dB) | margin (dB) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER (dB) | delta (x - margin) (dB) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER (dB) | delta (x - margin) (dB) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER (dB) | delta (x - margin) (dB) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER (dB) | delta (x - margin) (dB) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER (dB) | delta (x - margin) (dB) | | |
| 70 | 5.7E-05 | 41.4 | | 1.8E-04 | 50.3 | | 2.9E-03 | 27.3 | | 9.7E-03 | 25.4 | | 2.5E-02 | 23.4 | | | | | | | | | | | | | | |
| 40 | 20 | 6.0E-05 | 36.9 | 20 | 18.6 | -1.4 | 3.5E-04 | 29.6 | 19.5 | 11.3 | -8.2 | 3.6E-03 | 27 | 19 | 8.7 | -10.3 | 1.1E-02 | 25.2 | 19 | 6.9 | -12.1 | 2.6E-02 | 23.2 | 18 | 4.9 | -13.1 | | |
| 39 | 19 | 6.1E-05 | 36.2 | 19 | 17.9 | -1.1 | 3.9E-04 | 29.5 | 18.5 | 11.2 | -7.3 | 3.9E-03 | 26.9 | 18 | 8.6 | -9.4 | | | | | | | | | | | | |
| 38 | 18 | 6.1E-05 | 35.4 | 18 | 17.1 | -0.9 | 4.8E-04 | 29.3 | 17.5 | 11 | -6.5 | 4.1E-03 | 26.8 | 17 | 8.5 | -8.5 | | | | | | | | | | | | |
| 37 | 17 | 6.1E-05 | 34.7 | 17 | 16.4 | -0.6 | 5.6E-04 | 29.1 | 16.5 | 10.8 | -5.7 | 4.5E-03 | 26.7 | 16 | 8.4 | -7.6 | | | | | | | | | | | | |
| 36 | 16 | 6.1E-05 | 33.9 | 16 | 15.6 | -0.4 | 7.4E-04 | 28.9 | 15.5 | 10.6 | -4.9 | 4.9E-03 | 26.6 | 15 | 8.3 | -6.7 | | | | | | | | | | | | |
| 35 | 15 | 6.5E-05 | 33 | 15 | 14.7 | -0.3 | 9.6E-04 | 28.6 | 14.5 | 10.3 | -4.2 | 5.5E-03 | 26.4 | 14 | 8.1 | -5.9 | 1.3E-02 | 24.8 | 14 | 6.5 | -7.5 | 2.8E-02 | 22.9 | 13 | 4.6 | -8.4 | | |
| 34 | 14 | 6.8E-05 | 32.2 | 14 | 13.9 | -0.1 | 1.3E-03 | 28.3 | 13.5 | 10 | -3.5 | 6.3E-03 | 26.2 | 13 | 7.9 | -5.1 | 1.4E-02 | 24.7 | 13 | 6.4 | -6.6 | 3.0E-02 | 22.8 | 12 | 4.5 | -7.5 | | |
| 33 | 13 | 8.9E-05 | 31.3 | 13 | 13 | 0 | 1.8E-03 | 27.9 | 12.5 | 9.6 | -2.9 | 7.3E-03 | 25.9 | 12 | 7.6 | -4.4 | 1.5E-02 | 24.5 | 12 | 6.2 | -5.8 | 3.0E-02 | 22.7 | 11 | 4.4 | -6.6 | | |
| 32 | 12 | 1.7E-04 | 30.4 | 12 | 12.1 | 0.1 | 2.6E-03 | 27.4 | 11.5 | 9.1 | -2.4 | 8.7E-03 | 25.7 | 11 | 7.4 | -3.6 | 1.7E-02 | 24.3 | 11 | 6 | -5 | 3.2E-02 | 22.5 | 10 | 4.2 | -5.8 | | |
| 31 | 11 | 4.0E-04 | 29.5 | 11 | 11.2 | 0.2 | 3.8E-03 | 27 | 10.5 | 8.7 | -1.8 | 1.0E-02 | 25.3 | 10 | 7 | -3 | 2.0E-02 | 23.9 | 10 | 5.6 | -4.4 | 3.4E-02 | 22.3 | 9 | 4 | -5 | | |
| 30 | 10 | 1.0E-03 | 28.5 | 10 | 10.2 | 0.2 | 5.6E-03 | 26.4 | 9.5 | 8.1 | -1.4 | 1.3E-02 | 24.9 | 9 | 6.6 | -2.4 | 2.2E-02 | 23.6 | 9 | 5.3 | -3.7 | 3.6E-02 | 22.2 | 8 | 3.9 | -4.1 | | |
| 29.5 | 9.5 | 6.7E-03 | 26.1 | 9 | 7.8 | 0.3 | 6.7E-03 | 26.1 | 9 | 7.8 | -1.2 | 1.4E-02 | 24.7 | 8.5 | 6.4 | -2.1 | 2.4E-02 | 23.4 | 9 | 5.1 | -3.9 | | | | | | | |
| 29 | 9 | 2.4E-03 | 27.6 | 9 | 9.3 | 0.3 | 8.1E-03 | 25.8 | 8.5 | 7.5 | -1 | 1.6E-02 | 24.4 | 8 | 6.1 | -1.9 | 2.6E-02 | 23.2 | 8 | 4.9 | -3.1 | 3.9E-02 | 21.8 | 7 | 3.5 | -3.5 | | |
| 28.5 | 8.5 | | | | | | 9.9E-03 | 25.4 | 8 | 7.1 | -0.9 | 1.8E-02 | 24.2 | 7.5 | 5.9 | -1.6 | 2.7E-02 | 23 | 7.5 | 4.7 | -2.8 | 4.0E-02 | 21.7 | 6.5 | 3.4 | -3.1 | | |
| 28 | 8 | 4.8E-03 | 26.6 | 8 | 8.3 | 0.3 | 1.2E-02 | 25.1 | 7.5 | 6.8 | -0.7 | 2.0E-02 | 23.9 | 7.5 | 5.6 | -1.4 | 2.9E-02 | 22.8 | 7 | 4.5 | -2.5 | 4.2E-02 | 21.5 | 6 | 3.2 | -2.8 | | |
| 27.5 | 7.5 | 6.6E-03 | 26.1 | 7.5 | 7.8 | 0.3 | 1.4E-02 | 24.7 | 7 | 6.4 | -0.6 | 2.2E-02 | 23.7 | 6.5 | 5.4 | -1.1 | 3.2E-02 | 22.6 | 6.5 | 4.3 | -2.2 | 4.4E-02 | 21.3 | 5.5 | 3 | -2.5 | | |
| 27 | 7 | 8.9E-03 | 25.6 | 7 | 7.3 | 0.3 | 1.7E-02 | 24.3 | 6.5 | 6 | -0.5 | 2.5E-02 | 23.3 | 6 | 5 | -1 | 3.4E-02 | 22.3 | 6 | 4 | -2 | 4.6E-02 | 21.1 | 5 | 2.8 | -2.2 | | |
| 26.5 | 6.5 | 1.2E-02 | 25.1 | 6.5 | 6.8 | 0.3 | 1.9E-02 | 24 | 6 | 5.7 | -0.3 | 2.8E-02 | 23 | 5.5 | 4.7 | -0.8 | 3.7E-02 | 22.1 | 5.5 | 3.8 | -1.7 | 4.9E-02 | 20.8 | 4.5 | 2.5 | -2 | | |
| 26 | 6 | 1.5E-02 | 24.6 | 6 | 6.3 | 0.3 | 2.3E-02 | 23.6 | 5.5 | 5.3 | -0.2 | 3.1E-02 | 22 | 5 | 4.4 | 0.6 | 3.9E-02 | 21.6 | 5 | 3.5 | -3.5 | 5.1E-02 | 20.6 | 4 | 2.3 | -1 | | |
| 25.5 | 5.5 | 1.8E-02 | 24.1 | 5.5 | 5.8 | 0.3 | 2.6E-02 | 23.1 | 5 | 4.8 | -0.2 | 3.4E-02 | 22.3 | 4.5 | 4 | -0.5 | 4.3E-02 | 21.4 | 4.5 | 3.1 | -3.4 | 5.4E-02 | 20.3 | 3.5 | 2 | -1.5 | | |
| 25 | 5 | 2.3E-02 | 23.6 | 5 | 5.3 | 0.3 | 3.0E-02 | 22.7 | 4.5 | 4.4 | -0.1 | 3.8E-02 | 21.9 | 4 | 3.6 | -0.4 | 4.6E-02 | 21.1 | 4 | 2.8 | -2 | 5.7E-02 | 20.1 | 3 | 1.8 | -1.2 | | |
| 24.5 | 4.5 | 2.7E-02 | 23.1 | 4.5 | 4.8 | 0.3 | 3.5E-02 | 22.2 | 4 | 3.9 | -0.1 | 4.2E-02 | 21.5 | 3.5 | 3.2 | -0.3 | 5.0E-02 | 20.7 | 3.5 | 2.4 | -1.1 | 6.0E-02 | 19.8 | 2.5 | 1.5 | -1 | | |
| 24 | 4 | 3.2E-02 | 22.5 | 4 | 4.2 | 0.2 | 3.9E-02 | 21.8 | 3.5 | 3.5 | 0 | 4.6E-02 | 21.1 | 3 | 2.8 | -0.2 | 5.4E-02 | 20.3 | 3 | 2 | -1 | 6.4E-02 | 19.5 | 2 | 1.2 | -0.8 | | |
| 23.5 | 3.5 | 3.8E-02 | 22 | 3.5 | 3.7 | 0.2 | 4.4E-02 | 21.3 | 3 | 3 | 0 | 5.1E-02 | 20.6 | 2.5 | 2.3 | -0.2 | 5.8E-02 | 20 | 2.5 | 1.7 | -0.8 | 6.7E-02 | 19.2 | 1.5 | 0.9 | -0.6 | | |
| 23 | 3 | 4.3E-02 | 21.4 | 3 | 3.1 | 0.1 | 5.0E-02 | 20.7 | 2.5 | 2.4 | -0.1 | 5.6E-02 | 20.1 | 2 | 1.8 | 0.2 | 6.2E-02 | 19.6 | 2 | 1.3 | -0.7 | 7.1E-02 | 18.9 | 1 | 0.6 | -0.4 | | |
| 22.5 | 2.5 | 4.9E-02 | 20.8 | 2.5 | 2.5 | 0 | 5.5E-02 | 20.2 | 2 | 1.9 | -0.1 | 6.1E-02 | 19.7 | 1.5 | 1.4 | -0.1 | 6.7E-02 | 19.2 | 1.5 | 0.9 | -0.6 | 7.5E-02 | 18.7 | 0.5 | 0.4 | -0.1 | | |
| 22 | 2 | 5.5E-02 | 20 | 2 | 1.9 | -0.1 | 6.1E-02 | | 1.5 | 1.4 | -0.1 | 6.6E-02 | 19.3 | 1 | 1 | 0 | 7.2E-02 | 18.7 | 1 | 0.6 | 0.4 | 8.0E-02 | 18.9 | 0 | 0.6 | 0.6 | | |
| 21.5 | 1.5 | 6.2E-02 | 19.6 | 1.5 | 1.3 | -0.2 | 6.7E-02 | 19.2 | 1 | 0.9 | -0.1 | 7.2E-02 | 18.9 | 0.5 | 0.6 | 0.1 | 7.7E-02 | 18.6 | 0.5 | 0.3 | -0.2 | | | | | | | |
| 21 | 1 | 6.8E-02 | 19.1 | 1 | 0.8 | -0.2 | 7.3E-02 | 18.8 | 0.5 | 0.5 | 0 | 7.8E-02 | 18.5 | 0 | 0.2 | 0.2 | 8.2E-02 | 18.3 | 0 | 0 | 0 | | | | | | | |
| 20.5 | 0.5 | 7.5E-02 | 18.7 | 0.5 | 0.4 | -0.1 | 7.9E-02 | 18.4 | 0 | 0.1 | 0.1 | | | | | | | | | | | | | | | | | |
| 20 | 0 | 8.2E-02 | 18.3 | 0 | 0 | 0 | | | | | | | | | | | | | | | | | | | | | | |

The MER measured at the failure point could be regarded as the “reference MER” (18.3 dB). The difference between the measured MER and this “reference MER” might be used as a starting point to quantify the margin when the received level is at least -63 dBm.

$$\text{margin} = \text{MER} - \text{“reference MER”} \quad (1)$$

Note that this formula (1), by definition, gives margin = 0 at the failure point and, as a possible improvement, a further adjustment like the addition of a constant “b” might also be used, e.g. to minimize the “average” error, rather than the error “near the failure point”⁹.

For levels lower than -63 dBm, the results of C/I calculations are more influenced by the presence of the noise and the maximum BER and MER values that it's possible to measure are limited (see Table 2). This effect leads to an underestimation of the margin to the threshold.

However, for MFN, knowing the received input level, it's possible to identify a “Level correction factor”, Lc_{mf}, as a function of the received level and the measured BER, that could be applied to obtain a better approximation.

Table 3 summarizes the results for the “Level correction factor” obtained by the measurements presented in Table 2 and Fig. 4 shows the curves.

⁹ The results of the measurements show that the more appropriate adjustment is dependent from the adopted mode.

This Lc_{mfn} can be added to the margin obtaining the following formula (2):

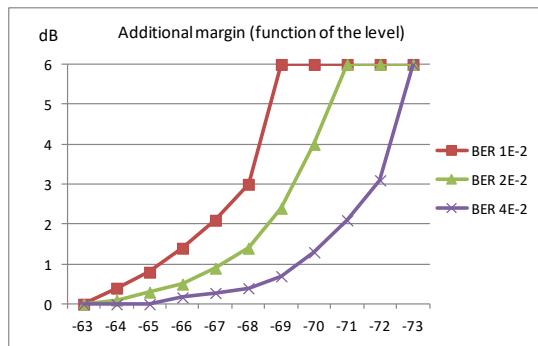
$$A2.6\text{margin} = \text{MER} - \text{"reference MER"} + Lc_{mfn} \quad (2)$$

The maximum value of the “Level correction factor” is limited to 6 dB and, if BER is worse than 4E-2, the factor is assumed equal to zero (no additional margin is added).

TABLE 3

| Lc_{mfn} | BER | | |
|------------|--------|--------|--------|
| | $1e-2$ | $2e-2$ | $4e-2$ |
| -63 | 0 | 0 | 0 |
| -64 | 0.5 | 0.18 | 0 |
| -65 | 0.85 | 0.28 | 0 |
| -66 | 1.35 | 0.65 | 0.25 |
| -67 | 2.1 | 0.9 | 0.28 |
| -68 | 3 | 1.4 | 0.4 |
| -69 | 6 | 2.2 | 0.7 |
| -70 | 6 | 3.5 | 1.2 |
| -71 | 6 | 6 | 1.9 |
| -72 | 6 | 6 | 3.1 |
| -73 | 6 | 6 | 6 |

FIGURE 4



4.4 Description of some results of the laboratory measurements for the SFN

Table 4 shows some results related to the profile of Fig. 1 for the chosen system variant with the two code rates (FEC 2/3 and FEC 3/5).

As expected, for each value of C/I , BER before LDPC and PLP MER do not depend on the code rate, while the margin and the iteration number change.

TABLE 4
Results of measurements (code rate 3/5, code rate 2/3)

| code 3/5 | | | | code 2/3 | | | |
|-----------|-------------|-----------------|----------------|----------------|----------------|-----------------|----------------|
| C/I (dB) | Iter numb. | BER Before LDPC | BER Before BCH | C/I (dB) | Iter numb. | BER Before LDPC | BER Before BCH |
| 40 | 3 | 4.9E-05 | 35.5 | 20 | 4.9E-05 | 35.6 | 18.5 |
| 39 | 3.1 | 5.0E-05 | 34.8 | 19 | 4.9E-05 | 34.8 | 17.5 |
| 38 | 3.1 | 5.0E-05 | 34 | 18 | 5.0E-05 | 34 | 16.5 |
| 37 | 3.1 | 5.1E-05 | 33.2 | 17 | 5.1E-05 | 33.2 | 15.5 |
| 36 | 3.1 | 5.2E-05 | 32.3 | 16 | 5.1E-05 | 32.3 | 14.5 |
| 35 | 3.2 | 5.5E-05 | 31.5 | 15 | 5.5E-05 | 31.5 | 13.5 |
| 34 | 3.3 | 7.4E-05 | 30.6 | 14 | 7.5E-05 | 30.5 | 12.5 |
| 33 | 3.3 | 1.7E-04 | 29.6 | 13 | 1.7E-04 | 29.6 | 11.5 |
| 32 | 3.6 | 5.2E-04 | 28.8 | 12 | 5.2E-04 | 28.8 | 10.5 |
| 31 | 3.9 | 1.5E-03 | 27.8 | 11 | 1.5E-03 | 27.8 | 9.5 |
| 30 | 4.5 | 3.6E-03 | 26.8 | 10 | 3.6E-03 | 26.8 | 8.5 |
| 29 | 5.2 | 7.4E-03 | 25.8 | 9 | 7.4E-03 | 25.8 | 7.5 |
| 28 | 6.2 | 1.3E-02 | 24.7 | 8 | 1.3E-02 | 24.7 | 6.5 |
| 27 | 7.5 | 2.1E-02 | 23.7 | 7 | 2.1E-02 | 23.7 | 5.5 |
| 26 | 9.1 | 3.0E-02 | 22.4 | 6 | 3.0E-02 | 22.5 | 4.5 |
| 25 | 11.1 | 4.0E-02 | 21.2 | 5 | 4.0E-02 | 21.3 | 3.5 |
| 24.5 | 12.3 | 4.6E-02 | 20.5 | 4.5 | 4.6E-02 | 20.5 | 3 |
| 24 | 13.6 | 5.1E-02 | 19.8 | 4 | 5.1E-02 | 19.8 | 2.5 |
| 23.5 | 15 | 5.7E-02 | 19.1 | 3.5 | 5.7E-02 | 19.1 | 2 |
| 23 | 16.9 | 6.3E-02 | 18.6 | 3 | 6.3E-02 | 18.6 | 1 |
| 22.5 | 19 | 6.9E-02 | 18.1 | 2.5 | 6.9E-02 | 18.2 | 0.5 |
| 22 | 21.7 | 7.6E-02 | 17.8 | 2 | 7.6E-02 | 17.8 | 0 |
| 21.5 | 24.8 | 8.2E-02 | 17.3 | 1.5 | 8.2E-02 | 17.3 | |
| 21 | 28.7 | 8.9E-02 | - | 1 | - | - | |
| 20.5 | 33.2 | 9.6E-02 | 16.4 | 0.5 | - | - | |
| 20.1 | 35.7 | 1.0E-01 | 9.0E-09 | 16 | - | - | |
| 20 | 36 | 1.0E-01 | 6.3E-08 | 15.9 | 0 | - | |
| limit -> | 19.9 | 36.1 | 1.1E-01 | 3.0E-07 | 15.8 | <0 | |

Table 5 shows some results for the two modes 3/5 and 2/3 for the profile of Fig. 2.

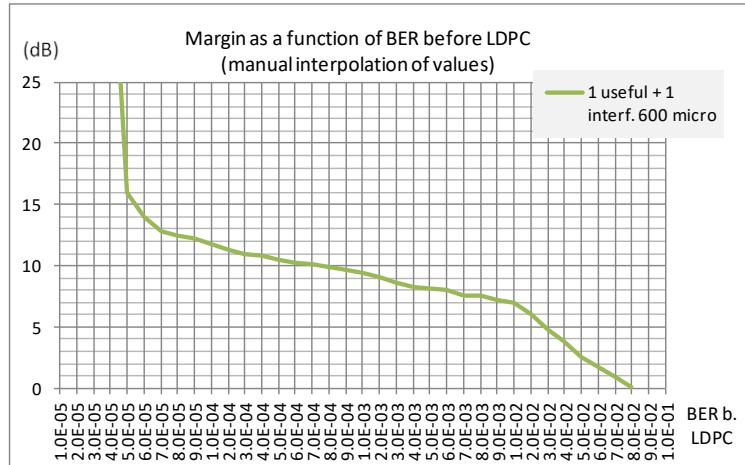
TABLE 5
Results of measurements using the SFN profile of Fig. 2

| code 3/5 | | | code 2/3 | | | | | |
|----------|-----------|----------------------|----------|-----------|----------------------|---------|---------|------|
| C/I (dB) | Iter num. | BER Before LDPC (dB) | C/I (dB) | Iter num. | BER Before LDPC (dB) | | | |
| 1 + 0 | 3.1 | 5.5E-05 | 41.2 | 1 + 0 | 2.7 | 5.3E-05 | 41.2 | |
| 40 | 7 | 1.0E-03 | 33.2 | 40 | 4.9 | 1.0E-03 | 33.2 | |
| 39 | 7 | 1.3E-03 | 32.6 | 39 | 5 | 1.3E-03 | 32.6 | |
| 38 | 7 | 1.7E-03 | 32 | 38 | 5.1 | 1.7E-03 | 32 | |
| 37 | 7 | 2.3E-03 | 31.3 | 37 | 5.1 | 2.3E-03 | 31.3 | |
| 36 | 7.1 | 3.0E-03 | 30.6 | 36 | 5.1 | 3.0E-03 | 30.6 | |
| 35 | 7.3 | 3.9E-03 | 30 | 35 | 5.2 | 3.9E-03 | 30 | |
| | | | | 34.5 | 5.3 | 4.5E-03 | 29.6 | |
| | | | | 34 | 5.3 | 5.1E-03 | 29.3 | |
| 34 | 7.3 | 5.1E-03 | 29.3 | 33.5 | 5.4 | 5.9E-03 | 29 | |
| | | | | 33 | 5.4 | 6.7E-03 | 28.6 | |
| 33 | 7.4 | 6.7E-03 | 28.6 | 32.5 | 5.4 | 7.7E-03 | 28.3 | |
| | | | | 32 | 5.5 | 8.8E-03 | 27.9 | |
| 32 | 7.9 | 8.8E-03 | 27.9 | 31.5 | 5.5 | 1.0E-02 | 27.5 | |
| | | | | 31 | 5.9 | 1.1E-02 | 27.1 | |
| 31 | 8.1 | 1.1E-02 | 27.1 | 30.5 | 5.9 | 1.3E-02 | 26.7 | |
| | | | | 30 | 6 | 1.5E-02 | 26.3 | |
| 30 | 8.4 | 1.5E-02 | 26.3 | 29.5 | 6.1 | 1.7E-02 | 25.8 | |
| | | | | 29 | 6.3 | 1.9E-02 | 25.4 | |
| 29 | 9 | 1.9E-02 | 25.4 | 28.5 | 6.5 | 2.2E-02 | 24.9 | |
| | | | | 28 | 6.7 | 2.5E-02 | 24.4 | |
| 28 | 9.7 | 2.5E-02 | 24.4 | 27.5 | 6.8 | 2.8E-02 | 23.8 | |
| | | | | 27 | 7.1 | 3.1E-02 | 23.2 | |
| 27 | 10.5 | 3.1E-02 | 23.2 | 26.5 | 7.4 | 3.5E-02 | 22.5 | |
| | | | | 26 | 7.7 | 3.9E-02 | 21.6 | |
| 26 | 11.5 | 3.9E-02 | 21.5 | 25.5 | 8.1 | 4.4E-02 | 20.5 | |
| | | | | 25 | 8.7 | 4.8E-02 | 19.3 | |
| 25 | 13.1 | 4.8E-02 | 19.3 | 24.5 | 9.2 | 5.3E-02 | 18.4 | |
| 24.5 | 14 | 5.3E-02 | 18.4 | 24 | 10 | 5.9E-02 | 17.7 | |
| 24 | 15 | 5.9E-02 | 17.7 | 23.5 | 10.8 | 6.4E-02 | 17.1 | |
| 23.5 | 16.2 | 6.4E-02 | 17.1 | 23 | 11.8 | 7.0E-02 | 16.5 | |
| 23 | 17.7 | 7.0E-02 | 16.5 | 22.5 | 13.3 | 7.6E-02 | 16 | |
| 22.5 | 19.2 | 7.6E-02 | 16 | 22 | 15.9 | 8.3E-02 | 15.3 | |
| 22 | 21.1 | 8.3E-02 | 15.4 | 1.5 | 21.5 | 20.8 | 8.9E-02 | 14.7 |
| 21.5 | 23.6 | 8.9E-02 | 14.7 | 21 | - | - | - | |
| 21 | 26.6 | 9.6E-02 | 14.1 | 20.5 | - | - | - | |
| 20.5 | 30.6 | 1.0E-01 | 13.5 | 20 | - | - | - | |
| 20 | 35.2 | 1.1E-01 | 12.8 | | | | | |

Again, for each value of C/I , BER before LDPC and PLP MER do not depend on the code rate (FEC). Note that, in comparison with Table 4 and for any value of MER, the values of BER before LDPC are changed.

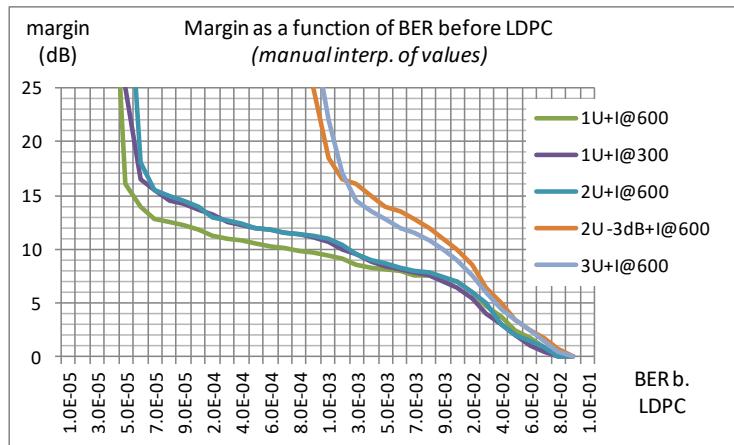
Plotting the results of the margin presented in Table 4 for code 2/3 as a function of BER before LDPC, it is possible to obtain the curve in Fig. 5.

FIGURE 5
Margin (dB) as a function of BER before LDPC (1 useful path+ 1 interference @600 µs)



Repeating the measurements for different SFN configurations, it is possible to obtain Fig. 6, which summarizes the results of the margin in function of the number of BER before LDPC, for some measured conditions.

FIGURE 6
Margin (dB) as a function of BER before LDPC



In Fig. 6:

- “1U+I@600” is the result using the profile showed in Fig. 1 with 1 useful signal and 1 interference @ 600 µs. This is the case with the minimum margin as a function of the measured BER. A very similar result can be obtained also with one interference “I” at a greater delay, e.g. 1 500 µs.
- “1U+I@300” is the result with 1useful signal and 1 interference @300 µs, just outside the GI.
- “2U+ I@600” is the case with two useful signals inside GI and 1 interference @600 µs.

- “2U (-3 dB) + I@600” is the case with two useful signals inside GI, one main plus a second that is attenuated 3 dB and 1 interference @600 μ s. This case is close to the example of one “0 dB echo” plus the interference.
- “3U+ I@600” is the result using the profile showed in Fig. 2.

Figure 6 shows that:

- The measured margin is the minimum (having equal BER), if there is a single useful contribution “far to the end of GI”.
- In the case of conditions similar to “0 dB echo” BER underestimates the available margin.
- In the case of echo outside the GI and “near to the end of GI” (e.g. 1 path+I@300), the measured margin as a function of BER is similar to the case with echo “far to the end of GI”.

Table 6 summarizes some cases with the minimum margin as a function of the measured BER. Looking at Fig. 6, if BER is equal or better than 1E-3, the margin will be at least 9 dB.

TABLE 6

| BER before LDPC | margin |
|-----------------|--------|
| <= 8E-2 | >= 0 |
| <= 6E-2 | >= 2 |
| <= 4E-2 | >= 3 |
| <= 1E-2 | >= 6 |
| <= 1E-3 | >= 9 |
| <= 1E-4 | >= 11 |

Figure 7 summarizes the results of the margin value in function of LDPC iterations, for some measured conditions.

FIGURE 7
Margin as a function of LDPC iterations

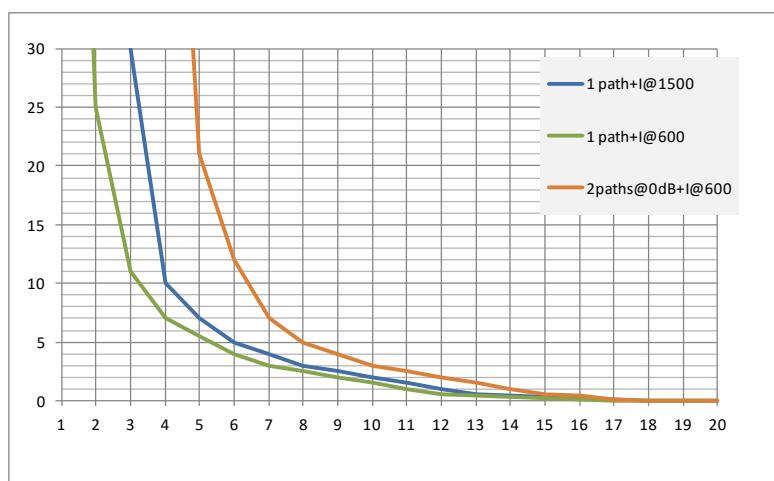


Figure 7 shows that:

- As a function of number of useful contribution (and path configuration), there is a different asymptotical (minimum) value of LDPC iterations.
- Having the same number of LDPC iterations, the margin is the minimum when there is a single useful contribution.

Table 7 summarizes some cases with the minimum margin as a function of the measured iterations. Looking at Fig. 7, if the iterations are equal or less than 6, the margin will be at least 4 dB.

TABLE 7

| LDPC iterations | margin |
|-----------------|--------|
| <= 20 | >= -1 |
| <= 15 | >= 0 |
| <= 10 | >= 2 |
| <= 6 | >= 4 |
| <= 5 | >= 6 |
| <= 3 | >= 10 |

It is to be noted that the results related to LDPC iterations depend on the chipset inside the receiver that is used for the tests.

In light of the results, in case of SFN:

- BER before BCH is not useful to identify the margin; and
- none of the parameters mentioned above (BER, MER, LDPC and received level) could be used alone to identify the margin.

For example, looking at the data listed in Table 8, extrapolated from the tests, BER before LDPC is the same in the two cases: the iteration number is better in the example #2 but example #1 has 11 dB of margin while the example #2 has only 7 dB. The use of PLP MER can help to better identify these margins.

TABLE 8

Two indicative examples of measurements with the same BER before LDPC

| example | SFN x2 (0dB) + AWGN | | | | |
|--------------------|---------------------|------------|-----------------|--------------|-------------|
| | C/I (dB) | Iter numb. | BER Before LDPC | MER PLP (dB) | margin (dB) |
| 1 | 33 | 6 | 1.1E-02 | 28.1 | 11 |
| SFN x2 +600 | | | | | |
| 2 | C/I (dB) | Iter numb. | BER Before LDPC | MER PLP (dB) | margin (dB) |
| | 29 | 4.8 | 1.1E-02 | 25.7 | 7 |

Vice-versa, in the example of Table 9, a SFN with 4 signals inside GI of which 2 near to the “0 dB echo” condition, the MER is very low, under the “reference MER”, while the margin is 1.5 dB.

TABLE 9

Example of measurement of MER lower than the “reference MER” and margin > 0 dB

| 10 | SFN x4 (0dB) + 600 | | | | |
|----|--------------------|------------|-----------------|------|-------------|
| | C/I (dB) | Iter numb. | BER Before LDPC | MER | margin (dB) |
| | 22 | 12 | 6.9E-02 | 16.7 | 1.5 |

These preliminary measurements show that the usage of PLP MER, BER and the number of LDPC iterations together can help to identify a possible criterion to be used for objective reception quality assessment of a DVB-T2 signal.

Finally, formula (1) defined for the MFN case could be adopted as a starting point to identify the margin also for SFN where the “reference MER” at failure point can remain the same as for the MFN case.

In fact, in the case of a SFN with a single contribution, the results are similar to the ones of the MFN case and, at least as a first approximation, this value is accurate enough and does not overestimate the margin. At least for the considered modes, Formula (2) could be used also for SFN with a slight modification that takes into account the BER before LDPC (see Table 6) and the iterations number (see Table 7). In § 5.2 a detailed description of the criteria is reported.

4.4.1 Dependency on the received level for the SFN case

Similar to the MFN case, it is possible to identify a dependency on the received level also for SFN.

The SFN profile “1U+I@600” shown in Fig. 1 was used and the value of the interference varied in test.

Table 10 shows the results and Table 11 summarizes the results for the “Level correction factor”, $L_{C_{sfn}}$, derived by these measurements. Figure 8 shows the curves.

It can be noted that the values of margin presented in Table 6 and Table 7 are conservative with respect to possible variations of the input.

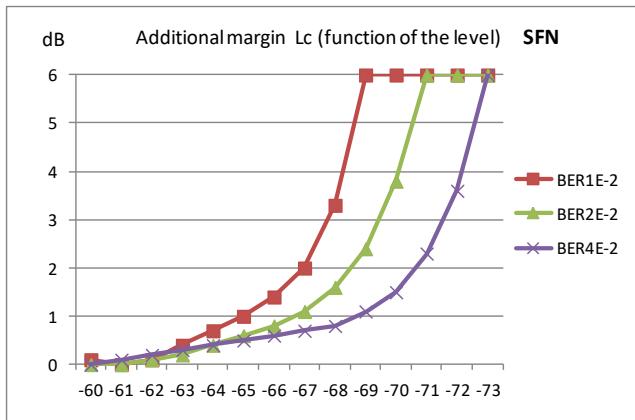
TABLE 10

Results with different Input levels (SFN) (Mode “32k not extended, PP2, 256 OAM, 2/3)

TABLE 11

| level (dBm) | BER | | |
|-------------|------|------|------|
| | 1e-2 | 2e-2 | 4e-2 |
| -60 | 0.1 | 0 | 0 |
| -61 | 0 | 0 | 0.1 |
| -62 | 0.1 | 0.1 | 0.2 |
| -63 | 0.4 | 0.2 | 0.3 |
| -64 | 0.7 | 0.4 | 0.4 |
| -65 | 1 | 0.6 | 0.5 |
| -66 | 1.4 | 0.8 | 0.6 |
| -67 | 2 | 1.1 | 0.7 |
| -68 | 3.3 | 1.6 | 0.8 |
| -69 | 6 | 2.4 | 1.1 |
| -70 | 6 | 3.8 | 1.5 |
| -71 | 6 | 6 | 2.3 |
| -72 | 6 | 6 | 3.6 |
| -73 | 6 | 6 | 6 |

FIGURE 8



5 Criteria for DVB-T2

As a result of the described measurements, the type of the broadcasting network (MFN-SFN) and the receiving conditions have to be considered in determining the criterion for the estimation of the available “margin to failure” and, therefore, the reception quality.

The criteria hereafter described are valid for fixed reception which implies a roof-top mounted antenna and an appropriate measuring time¹⁰ and it is preferable to not overestimate the value of the margin.

For simplicity, only the profile 32k not extended, GI 1/16, PP2, 256 QAM, code rate 2/3 is considered for both MFN¹¹ and SFN.

At this regard, it is to be noted that the results of measurements using different DVB-T2 modes (like those adopted for portable reception, e.g. 16k, 64 QAM, code rate 1/2) show that the difference between the measured MER and the “reference MER” may also lead to overestimation of the margin in a wide range of values. Therefore, in these cases, a different correction value has to be applied to the method.

Table 12 summarizes the *C/N* values and the sensitivity for the selected mode as per Report ITU-R BT.2254 [4] and the Italian HD-Book 3.0¹².

¹⁰ Note that the “BER reset time” of any test set-up instruments is typically over 2 seconds.

¹¹ For MFN purposes, in a real network, a different configuration of Pilot Patterns e.g. PP4 can be selected.

¹² HD Book 3.0 was published in 2014 and is in line with EBU TECH 3348 rev.4 and NorDig requirements for Gaussian and “echo 0dB” profiles (ref. NorDig-Unified_ver_2_6 and NorDig Unified Test plan, ver. 2.5.0). There are only differences of the order of 0.1 dB between the values presented in these documents, due to different rounding of the terms that contribute to give the overall *C/N* values and, therefore, the Minimum input levels (dBm) that are required at the input of the receivers.

TABLE 12

| 32k PP2 | C/N (dB) | | | | Sensitivity 8MHz, noise figure = 6 dB | | | |
|-------------|----------|------------------|--------------------|------|---------------------------------------|------------------|--------------------|-------|
| | AWGN | RC20 (Ricean) | RL20 (Rayleigh) | 0dB | AWGN | RC20 (Ricean) | RL20 (Rayleigh) | 0dB |
| 256-QAM 2/3 | 20.8 | 21.1 | 23.3 | 25.1 | -78.2 | -77.9 | -75.8 | -73.9 |

Table 13 summarizes the description of Quality Grades as in [1].

TABLE 13
Quality Grades

| Quality Grade | Description |
|---------------|--|
| Q1 | Signal level is below minimum planning target |
| Q2 | Signal level is below minimum planning target or margin to failure is too low (reception may be possible, but signal is very susceptible to failure) |
| Q3 | Signal level and margin to failure have some margin above minimum planning targets |
| Q4 | Signal level and margin to failure above planning target |
| Q5 | No measureable defects can be reasonably detected |

5.1 MFN Networks

In case of MFN¹³, where the interference is uncorrelated, equation (3) could be applied to identify the margin to the failure point and in the case of DVB-T2 profile 32k not extended, GI 1/16, PP2, 256 QAM, code rate 2/3, the “reference MER” is assumed as 18.3 dB and the Lc_{mfn} factor is obtained from the Table 14 and Fig. 9, as described in § 4.3.

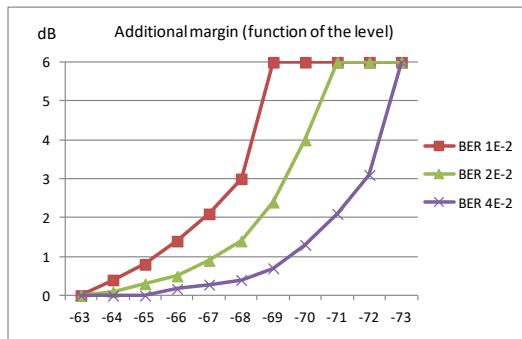
$$\text{margin} = \text{MER} - \text{“reference MER”} + Lc_{mfn} \quad (3)$$

TABLE 14

| Lc_{mfn} | BER | | |
|------------|------|------|------|
| | 1e-2 | 2e-2 | 4e-2 |
| -63 | 0 | 0 | 0 |
| -64 | 0.5 | 0.18 | 0 |
| -65 | 0.85 | 0.28 | 0 |
| -66 | 1.35 | 0.65 | 0.25 |
| -67 | 2.1 | 0.9 | 0.28 |
| -68 | 3 | 1.4 | 0.4 |
| -69 | 6 | 2.2 | 0.7 |
| -70 | 6 | 3.5 | 1.2 |
| -71 | 6 | 6 | 1.9 |
| -72 | 6 | 6 | 3.1 |
| -73 | 6 | 6 | 6 |

¹³ The same considerations and results should be valid in case of a SFN with a single useful signal or when the effect of the other transmitters are negligible.

FIGURE 9



The following examples show how to consider this factor.

Example 1

Measured data: RF level = -68 dBm; MER = 23.9 dB; BER 2E-2

Using equation (1), the margin "m" would be $23.9 - 18.3 = 5.6$ dB and comparing this value with the one of Table A1 in Annex 1, where the margin is 7 dB and C/I is 28 dB, there is an underestimation of 1.4 dB.

As the level is -68 dBm and BER is 2E-2, the L_{cmfn} is 1.4 dB and, applying equation (3),

$$m = 23.9 - 18.3 + 1.4 = 7 \text{ dB, in line with the laboratory tests.}$$

Example 2

Measured data: RF Level -69 dBm; MER = 21.9 dB; BER 3.8E-2

From Table A3.2 in Annex 3: $C/I = 25.5$ dB; margin = 4.5 dB

Using equation (1), the margin "m" would be $21.9 - 18.3 = 3.6$ dB and therefore 0.9 dB of difference.

As the level is -69 dBm and BER is 3.8E-2, the L_{cmfn} is 0.7 dB and, applying equation (3)

$$m = 21.9 - 18.3 + 0.7 = 4.3 \text{ dB, in line with the laboratory tests.}$$

Example 3

Measured data: RF Level -72 dBm; MER = 21.8 dB; BER 3.9E-2

From Table A1 in Annex 1: $C/I = 29$ dB; margin = 7 dB

Using equation (1), the margin "m" = $21.8 - 18.3 = 3.5$ dB and therefore 3.5 dB of underestimation.

As the level is -72 dBm and BER is 3.9E-2, the L_{cmfn} is 3.2 dB and applying equation (3)

$$m = 21.8 - 18.3 + 3.2 = 6.7 \text{ dB, in line with the laboratory tests.}$$

For MFN fixed reception, a possible "quality scale" could be:

TABLE 15

Quality scale for MFN

| Quality | 1 | 2 | 3 | 4 | 5 |
|------------|--------------|-----------------|-----------------|-----------------|-----------------|
| level E | $E < E_{70}$ | $E \geq E_{70}$ | $E \geq E_{95}$ | $E \geq E_{95}$ | $E \geq E_{95}$ |
| Margin "m" | — | $m \geq 0$ dB | $m \geq 4$ dB | $m \geq 8$ dB | $m \geq 12$ dB |

To have a certain “grade” in the scale, both requirements on level and margin have to be satisfied.
E.g.:

- if $E \geq E_{50}$ **and** $E < E_{70}$ (irrespectively of the margin “m”), then $Q = 1$
- if $E \geq E_{70}$ **and** margin $m < 0$ dB, then $Q = 1$.

At this stage of work, all the values of margins and field strengths in this Table 15 are only indicative and the results presented here still have to be compared with the results valid for DVB-T in [1].

It is noted that when using of strong modulation, e.g. 64 QAM, an additional correction factor, $f(BER)$, which depends on the value of the measured BER, should be included to take into account the non-linearity of the PLP MER. In this case, the formula becomes:

$$\text{margin} = \text{MER} - \text{“reference MER”} + L_{\text{mfn}} + f(BER) \quad (4)$$

In Table A3.1 in Annex 3 to Part 1 values for the $f(BER)$ factor are reported.

5.1.1 Dependency of the MFN method on the model of the receiver

Previous results are obtained using a professional receiver “A” that has its own documentation of calibration values from the manufacturer and is subject to a periodical calibration procedure.

However, this method could be used also with receivers (or semi-professional probes that e.g. are used for installation of receiving antennas for end-users) without a specific calibration procedure.

It has to be noted that, for a number of these equipment, the values of some parameters (like PLP MER and others) are not given when the received level is under a certain threshold (e.g. -60 dBm). Therefore, in this case, a different method has to be identified, e.g. using “L1 MER” as the reference parameter.

Table 16a shows the results @ -50 dBm of input level for the professional receiver “A” and Table 16b the equivalent results for a semi-professional receiver “B”.

In this case the results in terms of measured MER are equivalent and this equivalence remains true at least for input levels greater than -65 dBm.

If the PLP MER is not available, the L1-MER can be used to obtain the margin but in this case equation (1) has to be modified and the addition of the “Level correction factor” is not applied.

Note that Table 16b for receiver B is obtained with an input level of -50 dBm and the results for PLP MER are available. For lower levels (e.g. <-65 dBm), PLP MER is not available and only L1 MER is given.

TABLE 16a
Receiver A @ -50 dBm

| Mod-Code | C/I (dB) | Iter num. | ref. MER | | |
|--------------|--------------|-----------|----------------------|--------------|-------------|
| | | | BER Before LDPC (dB) | MER PLP (dB) | margin (dB) |
| 256 QAM, 2/3 | Add. Noise=0 | 2.5 | 5.9E-05 | 41.5 | |
| PP4, IG=1/16 | 40 | 2.5 | 6.0E-05 | 36.9 | 20 |
| | | 3.9 | 2.6 | 6.1E-05 | 36.2 |
| | | 38 | 2.6 | 6.1E-05 | 35.4 |
| | | 37 | 2.6 | 6.1E-05 | 34.7 |
| | | 36 | 2.65 | 6.1E-05 | 33.9 |
| | | 35 | 2.7 | 6.5E-05 | 33 |
| | | 34 | 2.75 | 6.8E-05 | 32.2 |
| | | 33 | 2.8 | 8.9E-05 | 31.3 |
| | | 32 | 2.8 | 1.7E-04 | 30.4 |
| | | 31 | 2.9 | 4.0E-04 | 29.5 |
| | | 30 | 3.2 | 1.0E-03 | 28.5 |
| | | 29 | 3.4 | 2.4E-03 | 27.6 |
| | | 28 | 3.8 | 4.8E-03 | 26.6 |
| | | 27.5 | 4 | 6.6E-03 | 26.1 |
| | | 27 | 4.4 | 8.9E-03 | 25.6 |
| | | 26.5 | 4.6 | 1.2E-02 | 25.1 |
| | | 26 | 4.9 | 1.5E-02 | 24.6 |
| | | 25.5 | 5.4 | 1.8E-02 | 24.1 |
| | | 25 | 5.8 | 2.2E-02 | 23.6 |
| | | 24.5 | 6.2 | 2.7E-02 | 23.1 |
| | | 24 | 6.6 | 3.2E-02 | 22.5 |
| | | 23.5 | 7.1 | 3.8E-02 | 22 |
| | | 23 | 7.7 | 4.3E-02 | 21.4 |
| | | 22.5 | 8.4 | 4.9E-02 | 20.8 |
| | | 22 | 9.3 | 5.5E-02 | 20.2 |
| | | 21.5 | 10.6 | 6.2E-02 | 19.6 |
| | | 21 | 11.3 | 6.8E-02 | 19.1 |
| | | 20.5 | 14.9 | 7.5E-02 | 18.7 |
| | | 20 | 19.5 | 8.2E-02 | 18.3 |

TABLE 16b
Receiver B @ -50 dBm

| Mod-Code | C/I (dB) | Iter num. | ref. MER | | |
|--------------|--------------|-----------|----------------------|--------------|-------------|
| | | | BER Before LDPC (dB) | MER PLP (dB) | margin (dB) |
| 256 QAM, 2/3 | Add. Noise=0 | 1 | 1.0E-04 | 41.2 | |
| PP4, IG=1/16 | 40 | 1 | 1.0E-04 | 36.4 | 20 |
| | | 39 | 1 | 1.0E-04 | 35.9 |
| | | 38 | | | 18 |
| | | 37 | 1 | 1.0E-04 | 34.4 |
| | | 36 | | | 16 |
| | | 35 | 1 | 1.0E-04 | 32.8 |
| | | 34 | | | 14 |
| | | 33 | | | 13 |
| | | 32 | 1 | 1.0E-04 | 30 |
| | | 31 | | | 11 |
| | | 30 | 2 | 1.0E-03 | 28.2 |
| | | 29 | 2 | 2.0E-03 | 27.2 |
| | | 28 | 2 | 4.0E-03 | 26.2 |
| | | 27.5 | 4 | 6.6E-03 | 26.1 |
| | | 27 | 3 | 7.0E-03 | 25.2 |
| | | 26.5 | 3 | 1.0E-02 | 24.2 |
| | | 26 | | | 6 |
| | | 25.5 | 3 | 1.0E-02 | 23.3 |
| | | 25 | | | 5 |
| | | 24.5 | | | 4.5 |
| | | 24 | 5 | 2.0E-02 | 22.2 |
| | | 23.5 | 6 | 3.0E-02 | 21.6 |
| | | 23 | 6 | 3.0E-02 | 21.3 |
| | | 22.5 | 6 | 4.0E-02 | 20.8 |
| | | 22 | 7 | 4.0E-02 | 20.3 |
| | | 21.5 | 8 | 5.0E-02 | 19.8 |
| | | 21 | 10 | 6.0E-02 | 19.3 |
| | | 20.5 | 11 | 6.0E-02 | 18.5 |
| | | 20 | 14 | 7.0E-02 | 18.3 |

5.2 SFN Networks

In the case of SFN, the proposed criterion for MFN is also applicable. A further assumption is that the “Impulse response” is not available, therefore the number and nature of the received SFN paths is “unknown”.

Step 1) If the level $E < E_{70}$, identifying the margin is not relevant because the quality is low due to the low level.

Step 2) If the level $E > E_{70}$, the following equation (5) is applied

$$\text{margin} \geq \text{MER} - \text{“reference MER”} + L_{\text{csfn}} + f(\text{BER})_{\text{sfm}} \quad (5)$$

where, in the case of DVB-T2 profile 32k not extended, GI 1/16, PP2, 256 QAM, code rate 2/3:

- the “reference MER” is the same value of the “reference MER” as for the MFN case, 18.3 dB;
- L_{csfn} is obtained from the Table 17 and Fig. 10. E.g. if the input level P_s is $-67 \text{ dBm} < P_s \leq -66 \text{ dBm}$ and BER (before LDPC) is “ $1e-2$ ” $< \text{BER} \leq “2e-2”$, then L_{csfn} is 0.8 dB;
- $f(\text{BER})_{\text{sfm}}$ is an empirical correction, based on the results of the measurements with different SFN profiles, depending on BER as shown in Fig. 11. $f(\text{BER})_{\text{sfm}}$ is equal to 0 when the input level is equal or lower than a certain value (e.g. -60 dBm in this case) and the predominant correction is done with the parameter L_{csfn} .

TABLE 17

| level (dBm) | BER | | |
|-------------|------|------|------|
| | 1e-2 | 2e-2 | 4e-2 |
| -60 | 0.1 | 0 | 0 |
| -61 | 0 | 0 | 0.1 |
| -62 | 0.1 | 0.1 | 0.2 |
| -63 | 0.4 | 0.2 | 0.3 |
| -64 | 0.7 | 0.4 | 0.4 |
| -65 | 1 | 0.6 | 0.5 |
| -66 | 1.4 | 0.8 | 0.6 |
| -67 | 2 | 1.1 | 0.7 |
| -68 | 3.3 | 1.6 | 0.8 |
| -69 | 6 | 2.4 | 1.1 |
| -70 | 6 | 3.8 | 1.5 |
| -71 | 6 | 6 | 2.3 |
| -72 | 6 | 6 | 3.6 |
| -73 | 6 | 6 | 6 |

FIGURE 10

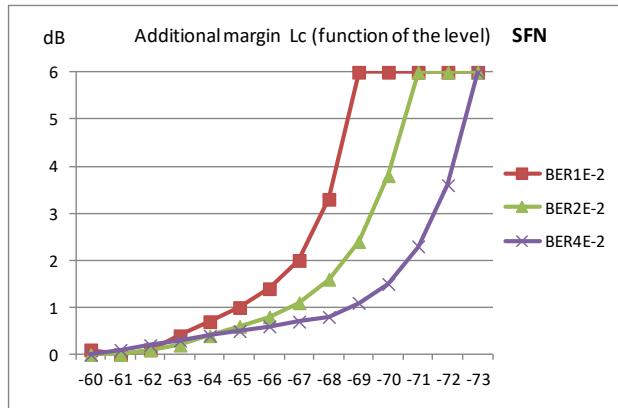
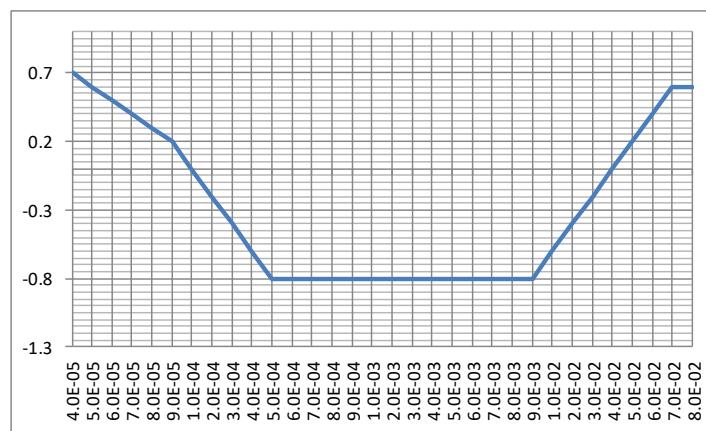


FIGURE 11

$f(BER)_{sfm}$ for mode “32k not extended, GI 1/16, PP2, 256 QAM, 2/3”



Step 3) The values in Table 18 can be used to further check and correct the margin.

TABLE 18

| BER before LDPC | margin |
|-----------------|-----------|
| $\leq 8E-2$ | ≥ 0 |
| $\leq 6E-2$ | ≥ 2 |
| $\leq 4E-2$ | ≥ 3 |
| $\leq 1E-2$ | ≥ 6 |
| $\leq 1E-3$ | ≥ 9 |
| $\leq 1E-4$ | ≥ 11 |

Step 4) As a further approximation, the margin can also be checked and corrected, if necessary, using the values in Table 19. These values depend on the implementation of the receiver and, therefore, are only indicative.

TABLE 19

| LDPC iterations | margin |
|-----------------|-----------|
| ≤ 20 | ≥ -1 |
| ≤ 15 | ≥ 0 |
| ≤ 10 | ≥ 2 |
| ≤ 6 | ≥ 4 |
| ≤ 5 | ≥ 6 |
| ≤ 3 | ≥ 10 |

Step 5) The margin is the highest values obtained from step 2, step 3 and step 4¹⁴.

Table 20 could be used to define the quality of service.

TABLE 20

Quality Scale for SFN

| Quality | 1 | 2 | 3 | 4 | 5 |
|------------|--------------|-----------------------|-----------------------|-----------------------|------------------------|
| level E | $E < E_{70}$ | $E \geq E_{70}$ | $E \geq E_{95}$ | $E \geq E_{95}$ | $E \geq E_{95}$ |
| margin "m" | – | $m \geq 0 \text{ dB}$ | $m \geq 4 \text{ dB}$ | $m \geq 8 \text{ dB}$ | $m \geq 12 \text{ dB}$ |

To have a certain “grade” in the scale, both requirements on level and margin have to be satisfied. E.g.:

- if $E \geq E_{50}$ **and** $E < E_{70}$ (irrespectively of the margin “m”), then $Q = 1$
- If $E \geq E_{70}$ **and** margin $m < 0 \text{ dB}$, then $Q = 1$.

¹⁴ For more “robust” modes, like those adopting 16k FFT and 64 QAM modulation for portable reception, a different correction has to be applied in order not to overestimate the margin.

The proposed “quality scale” for SFN is the same as for the MFN case. The values of margins and Field Strengths are only indicative, at this stage of work, and the results presented here still have to be compared with those valid for DVB-T in [1].

5.2.1 Dependency of the SFN method on the model of receiver

At this stage of work, the dependency of the SFN method on the model of receiver has still to be fully checked.

5.2.2 Examples of application of the SFN criteria

In Table 21 some examples of SFN configurations are listed for mode 32 k not extended, GI 1/16, PP2, 256 QAM, 2/3 with the respective margin and values of the measured parameters. These data are coming from the laboratory measurements and, therefore, the expected values of the margin to the failure point and the quality “Q” are known.

The margin and the quality are evaluated using the proposed criteria and the obtained results are compared with the expected values. The reported discrepancies are limited to a fraction of a dB.

TABLE 21
Examples of SFN configurations: margin and evaluated Quality

| # | SFN profile | interf. C/I (dB) | Results of measurements and margin | | | | Application of the method to obtain the margin | | | | | | | Quality | Evaluated Quality |
|----|------------------------|------------------------|------------------------------------|-----------------------|-----------------|----------------|--|----------------|--------------------------------|---------------------------------|----------------------------------|------------------------------------|---------------|---------|-------------------|
| | | | Iter numb. | BER Before LDPC | MER PLP (dB) | margin (dB) | MER - Ref. MER (dB) | f(BER) (dB) | formula (4) (step2) (dB) | table BER (step 3 *) (dB) | table ITER (step 4 *) (dB) | evaluation of margin (dB) ** | error (dB) | | |
| 1 | 2U (-3dB) + AWGN | 33 | 6 | 1.1E-02 | 28.1 | 11 | 9.8 | -0.6 | 9.2 | 3 | 2 | 9.2 | -1.8 | 4 | 4 |
| 2 | 2U + Interf 600 | 29 | 4.8 | 1.1E-02 | 25.7 | 7 | 7.4 | -0.6 | 6.8 | 3 | 6 | 6.8 | -0.2 | 3 | 3 |
| 3 | 2U + Interf 600 | 36 | 3.5 | 1.1E-04 | 31.8 | 14 | 13.5 | 0 | 13.5 | 9 | 6 | 13.5 | -0.5 | 5 | 5 |
| 4 | 1U + Interf 600 | 24.5 | 7.9 | 4.6E-02 | 20.5 | 3 | 2.2 | 0 | 2.2 | 2 | 2 | 2.2 | -0.8 | 2 | 2 |
| 5 | 1U + Interf 600 | 33 | 2.9 | 1.7E-04 | 29.6 | 11.5 | 11.3 | 0 | 11.3 | 9 | 10 | 11.3 | -0.2 | 4 | 4 |
| 6 | 1U + Interf 300 | 17 | 3.5 | 2.0E-03 | 28.9 | 10 | 10.6 | -0.8 | 9.8 | 6 | 6 | 9.8 | -0.2 | 4 | 4 |
| 7 | 1U + Interf 1500 | 27 | 5.1 | 1.6E-02 | 24.7 | 6 | 6.4 | -0.6 | 5.8 | 3 | 4 | 5.8 | -0.2 | 4 | 4 |
| 8 | 2U (3dB) + interf 350 | 13 | 9.3 | 5.1E-02 | 20.6 | 3.5 | 2.3 | 0.2 | 2.5 | 2 | 2 | 2.5 | -1 | 2 | 2 |
| 9a | 3U + Interf 600 | 30 | 5.9 | 1.5E-02 | 26.1 | 8.5 | 7.8 | -0.6 | 7.2 | 3 | 4 | 7.2 | -1.3 | 4 | 3 |
| 9b | 3U + Interf 600 | 29 | 6.2 | 2.0E-02 | 25.2 | 7.5 | 6.9 | -0.4 | 6.5 | 3 | 2 | 6.5 | -1 | 3 | 3 |
| 10 | 4U (3dB) + interf 600 | 22 | 12 | 6.9E-02 | 16.7 | 1.5 | -1.6 | 0.4 | -1.2 | 0 | 0 | 0 | -1.5 | 2 | 2 |
| 11 | 4U (3dB) + interf 1500 | 35 | 5.5 | 2.2E-03 | 31 | 15.5 | 12.7 | -0.8 | 11.9 | 6 | 4 | 11.9 | -3.6 | 5 | 4 |
| 12 | 1U + Interf 600 | 28 | 4.6 | 1.3E-02 | 24.7 | 6.5 | 6.4 | -0.6 | 5.8 | 3 | 6 | 6 | -0.5 | 2 | 2 |
| 13 | 1U + Interf 600 | 21.5 | 21.3 | 8.2E-02 | 17.3 | 0 | -1 | 0.6 | -0.4 | 0 | -2 | 0 | 0 | 2 | 2 |

* margin has to be better than ...

** Evaluated margin is the better value between the three results of step 2, step 3 and step 4.

TABLE 22
Reference parameters (mode 32k, GI 1/16, PP2, 256 QAM, code 2/3)

| reference MER (dB) 18.3 | BER before LDPC | margin | LDPC iterations | margin |
|--------------------------------------|--------------------|--------|--------------------|--------|
| | <= 8E-2 | >= 0 | <= 20 | >= -1 |
| | <= 6E-2 | >= 2 | <= 15 | >= 0 |
| | <= 4E-2 | >= 3 | <= 10 | >= 2 |
| | <= 1E-2 | >= 6 | <= 6 | >= 4 |
| | <= 1E-3 | >= 9 | <= 5 | >= 6 |
| | <= 1E-4 | >= 11 | <= 3 | >= 10 |

6 Conclusions

Some of the parameters that are commonly used for DVB-T assessment of the quality of service (e.g. BER before Viterbi and BER before Reed Solomon) are no longer available for DVB-T2, while there are some additional ones like PLP MER, BER before LDPC (inner) decoder, BER before BCH (outer) decoder and Number of LDPC Iterations.

At this regard, laboratory measurements show that the difference between the measured MER and the MER at the failure point, when only noise is added, can be used as a preliminary approximation of the margin available in a specific location of reception.

This is valid in case of the modes (using 32 k, 256 QAM modulation) that are treated in this study, while, in case of more robust modes (e.g. 16 k, 16 QAM), an additional correction has to be introduced in order to not over-estimate the margin.

The evaluation of PLP MER, BER before LDPC, and also the number of LDPC iterations together can be used for the objective reception quality assessment for the DVB-T2 signals, for both MFNs and SFNs.

The study should be extended considering additional modes, including those used for portable reception. Moreover, an analysis on the applicability of the method when using different model of receivers should be considered as well as the study of multiple interferences.

On field measurements should be performed in order to validate the proposed method(s) in real world environments.

7 References

- [1] Recommendation ITU-R BT.1735 – Methods for objective reception quality assessment of digital terrestrial television broadcasting signal of System B specified in Recommendation ITU-R BT.1306
- [2] ETSI TR 101 290 V.1.3.1 – 2014-07 (DVB-M) – Measurement guidelines for DVB system
- [3] ETSI TS 102 831 V1.2.1 Digital Video Broadcasting (DVB) – Implementation guidelines for a second generation digital terrestrial television broadcasting system (DVB-T2)
- [4] Report ITU-R BT.2254 – Frequency and network planning aspects of DVB-T2
- [5] Report ITU-R BT.2389 – Guidelines on measurements for digital terrestrial television broadcasting systems
- [6] ETSI TR 101 290 Digital Video Broadcasting (DVB) – Measurement guidelines for DVB systems
- [7] NorDig Unified Test Plan for Integrated Receiver Decoders for use in cable, satellite, terrestrial and IP-based networks
- [8] Recommendation [ITU-R BT.2033](#) – Planning criteria, including protection ratios, for second generation of digital terrestrial television broadcasting systems in the VHF/UHF bands

**Annex 1
to Part 1****Example of the method to obtain the additional margin $L_{C_{MFN}}$**

MFN C/I (I = co-channel interference, equivalent to Gaussian noise) indicates the ratio between the useful signal and the added noise. The results in Table A1.1 are obtained with the professional receiver “A1” for the mode 32 k not extended, 256 QAM, PP2, 256 QAM, 2/3 and, in this case, “Reference MER” (the MER at failure point, with input level –50 dBm and when only noise is added) is 18.3 dB.

Using these results, e.g. if the level is –68 dBm and BER Before LDPC is 2.0E-2, the margin should be 7 dB, while the difference “MER – Reference MER” is 5.6 dB. Therefore the “delta” to add as a function of the level is –1.4 dB and this value (with positive sign) is placed in Table A1.2.

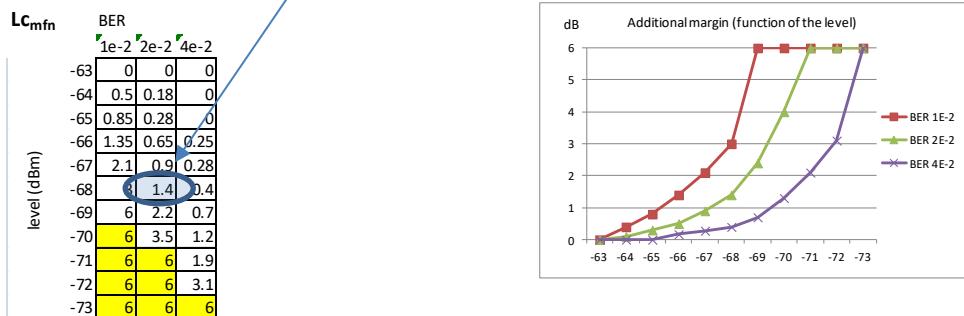
TABLE A1.1
Results with different Input levels
Mode 32k not extended, 256 QAM, PP2, 256 QAM, 2/3

TABLE A1.2

FIGURE A1

Level correction factor, Lc_{mfn}

Level correction factor, L_{cmfn}



Annex 2 to Part 1

Results of DVB-T2 laboratory measurements (SFN)

DVB T2 Bands IV-V

This Annex illustrates the results of some laboratory measurements and derived parameters, obtained using different SFN profiles for mode 32 k not extended, PP2, GI 1/16, 256 QAM, code rate 2/3. In particular, this Annex gives an example of comparison of results between two different receivers of

the same model and show the results of the measurements used to obtain the Fig. 6 “Margin as a function of BER Before LDPC”.

TABLE A2.1

SFN: 1 Useful signal + 1 interference @600 μs (comparison between instruments A1 and A2)

| Instrument "A1" | | | | | | | | | | Instrument "A2" | | | | | | | | | | Comparison | |
|-------------------------|------------|-----------------|---------|----------------|---|--------------|------|-------------|--|-------------------------|--------------|----------|---------|------------|------|-----------------------|--------------|----------|------|--------------------------|------|
| Results of Measurements | | | | | | | | | | Results of Measurements | | | | | | | | | | | |
| C/I (dB) | Iter. num. | BER Before LDPC | | BER Before BCH | | MER PLP (dB) | | MER L1 (dB) | | C/I - MER margin (dB) | MER-ref (dB) | MER (dB) | | delta (dB) | | C/I - MER margin (dB) | MER-ref (dB) | MER (dB) | | delta A1 - delta A2 (dB) | |
| | | I=0 | 2.5 | 5.9E-05 | | 41.5 | 39.4 | | | | | 4.4 | 19.5 | 17.3 | -1.2 | | | 4.7 | 18.4 | 17 | -1.5 |
| 40 | 2.5 | 4.9E-05 | | | | 35.6 | | | | 4.2 | 17.5 | 16.5 | -1 | | | 4.4 | 17.5 | 16.3 | -1.2 | 0.2 | |
| 39 | 2.6 | 4.9E-05 | | | | 34.8 | | | | 4 | 16.5 | 15.7 | -0.8 | | | 4.1 | 16.4 | 15.6 | -0.9 | 0.1 | |
| 38 | 2.6 | 5.0E-05 | | | | 34 | | | | 3.8 | 15.5 | 14.9 | -0.6 | | | 3.9 | 15.5 | 14.8 | -0.7 | 0.1 | |
| 37 | 2.6 | 5.1E-05 | | | | 33.2 | | | | 3.7 | 14.5 | 14 | -0.5 | | | 3.8 | 14.4 | 13.9 | -0.6 | 0.1 | |
| 36 | 2.7 | 5.1E-05 | | | | 32.3 | | | | 3.5 | 13.5 | 13.2 | -0.3 | | | 3.6 | 13.5 | 13.1 | -0.4 | 0.1 | |
| 35 | 2.7 | 5.5E-05 | | | | 31.5 | | | | 3.5 | 12.5 | 12.2 | -0.3 | | | 3.5 | 12.5 | 12.2 | -0.3 | 0 | |
| 34 | 2.8 | 7.5E-05 | | | | 30.5 | | | | 3.4 | 11.5 | 11.3 | -0.2 | | | 3.4 | 11.5 | 11.3 | -0.2 | 0 | |
| 33 | 2.9 | 1.7E-04 | | | | 29.6 | | | | 3.2 | 10.5 | 10.5 | 0 | | | 3.3 | 10.5 | 10.4 | -0.1 | 0.1 | |
| 32 | 3.1 | 5.2E-04 | | | | 28.8 | | | | 3.2 | 9.5 | 9.5 | 0 | | | 3.2 | 9.5 | 9.5 | 0 | 0 | |
| 31 | 3.3 | 1.5E-03 | | | | 27.8 | | | | 3.2 | 8.5 | 8.5 | 0 | | | 3.2 | 8.5 | 8.5 | 0 | 0 | |
| 30 | 3.6 | 3.6E-03 | | | | 26.8 | | | | 3.2 | 7.5 | 7.5 | 0 | | | 3.3 | 7.5 | 7.4 | -0.1 | 0.1 | |
| 29 | 4.2 | 7.4E-03 | | | | 25.8 | | | | 3.1 | 6.5 | 6.4 | -0.1 | | | 3.3 | 6.5 | 6.4 | -0.1 | 0 | |
| 28 | 4.6 | 1.3E-02 | | | | 24.7 | | | | 3.1 | 5.5 | 5.4 | -0.1 | | | 3.3 | 5.5 | 5.4 | -0.1 | 0 | |
| 27 | 5.5 | 2.1E-02 | | | | 23.7 | | | | 3.0 | 4.5 | 4.2 | -0.3 | | | 3.5 | 4.5 | 4.2 | -0.3 | 0 | |
| 26 | 6.3 | 3.0E-02 | | | | 22.5 | | | | 2.9 | 3.5 | 3 | -0.5 | | | 3.6 | 3.5 | 2.9 | -0.6 | 0.1 | |
| 25 | 7.3 | 4.0E-02 | | | | 21.3 | | | | 2.9 | 3 | 2.2 | -0.8 | | | 4 | 3 | 2.2 | -0.8 | 0 | |
| 24.5 | 7.9 | 4.6E-02 | | | | 20.5 | 20.9 | | | 2.8 | 2.5 | 1.5 | -1 | | | 4.2 | 2.5 | 1.5 | -1 | 0 | |
| 24 | 8.6 | 5.1E-02 | | | | 19.8 | 20.4 | | | 2.8 | 2 | 0.8 | -1.2 | | | 4.3 | 2 | 0.5 | -1.1 | -0.1 | |
| 23.5 | 9.5 | 5.7E-02 | | | | 19.1 | 19.9 | | | 2.8 | 1.5 | 0.3 | -1.2 | | | 4.4 | 1.5 | 0.3 | -1.2 | 0 | |
| 23 | 10.7 | 6.3E-02 | | | | 18.6 | 19.4 | | | 2.8 | 1 | -0.1 | -1.1 | | | 4.4 | 1 | -0.2 | -1.2 | 0.1 | |
| 22.5 | 12.6 | 6.9E-02 | | | | 18.2 | 18.9 | | | 2.8 | 0.5 | -0.5 | -1 | | | 4.3 | 0.5 | -0.6 | -1.1 | 0.1 | |
| 22 | 15.5 | 7.6E-02 | | | | 17.8 | 18.4 | | | 2.8 | 15.5 | 7.6E-02 | | | | 4.2 | 1.4 | -0.6 | -1 | 0 | |
| ok | 21.5 | 21.3 | 8.2E-02 | | | 17.3 | 17.9 | | | 2.8 | 21.4 | 8.2E-02 | | | | 4.2 | 0 | -1 | -1 | 0 | |
| ko | 21.4 | 24.3 | 8.3E-02 | 6.1E-04 | - | 17.8 | | | | 2.8 | 24.2 | 8.4E-02 | 6.2E-04 | 17.2 | 17.8 | 21 | - | - | - | 17.4 | |
| | 21 | - | - | - | - | - | - | | | | | | | | | | | | | | |

* visual failure point: where the picture is only just good (due to ESR5) in 0.1 dB steps
 ** receiver failure point: where measured values are still there (even only for a short time)

Table A2.1 shows the outcomes of measurements performed by two different companies, which used two professional receivers “A1” and “A2” of the same model type “A” and two different signal generators. The differences of the results is lower than 0.3 dB.

TABLE A2.2

SFN: 1 Useful signal + 1 interference @600 µs (measurement repeated for instrument A1)

| | | date 04.09.2018 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|--|-----------|-------------------------|----------------|--------------|-------------|----------------------------------|-------------|------------------|------------------|--|--|----------|-----------|-----------------|----------------|--------------|-------------|--------------------|-------------|------------------|------------|-----|-----|---------|--|------|------|-----|------|------|------|----|-----|---------|--|------|------|-----|------|------|----|----|-----|---------|--|------|------|---|------|------|------|----|-----|---------|--|----|------|-----|------|------|------|----|-----|---------|--|------|------|-----|------|----|------|----|-----|---------|--|------|------|-----|------|------|------|----|---|---------|--|------|------|-----|----|------|------|------|---|---------|--|----|------|-----|------|------|------|----|---|---------|--|------|------|-----|----|------|------|------|---|---------|--|------|------|-----|------|------|------|----|-----|---------|--|------|----|---|----|------|----------------|------|-----|---------|--|------|------|-----|------|------|---|----|-----|---------|--|------|------|-----|----|----|---|------|-----|---------|--|------|------|-----|-----|-----|---|----|-----|---------|--|------|------|-----|---|---|---|------|-----|---------|--|------|------|-----|-----|-----|---|----|-----|---------|--|------|------|-----|---|---|---|------|-----|---------|--|------|------|-----|-----|-----|---|----|-----|---------|--|------|------|-----|---|-----|------|------|-----|---------|--|------|------|-----|-----|-----|------------------|----|-----|---------|--|------|------|-----|---|-----|------|------|-----|---------|--|------|------|-----|-----|-----|------|----|-----|---------|--|------|------|-----|---|-----|------|------|-----|---------|--|------|------|-----|-----|-----|------|----|-----|---------|--|------|------|-----|---|-----|------|------|-----|---------|--|------|------|-----|-----|-----|------|----|-----|---------|--|------|------|---|---|-----|------|------|-----|---------|--|------|------|-----|-----|-----|----|----|-----|---------|--|------|------|-----|---|-----|-----------------|------|-----|---------|--|------|------|-----|-----|-----|------|----|------|---------|--|------|------|-----|---|------|------|------|------|---------|--|------|------|-----|-----|------|------|----|------|---------|--|------|------|-----|---|----|----|------|------|---------|--|------|------|--|--|--|--|----|---|---|---|---|------|--|--|--|--|
| | | time | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | generator SFU | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| receiver A1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| MFN/SFN | | SFN | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Measur. type | | Pr. Ratio * | | | | useful "C" = 0 @ 0 microseonds | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| CH | | 38 | | | | interf. "I" = @ 600 microseconds | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| level | | -50 | | dBm | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| FFT, PP | | 32kn, PP2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| GI | | 1/16 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| GI duration | | 224 | | µs | | (nominal value) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| PLP Code | | 2/3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| L1 mod | | 16 QAM | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| reference MER ** | | 18.3 dB | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1"> <thead> <tr> <th colspan="10">results of measurements</th> </tr> <tr> <th>C/I (dB)</th> <th>Iter numb</th> <th>BER Before LDPC</th> <th>BER Before BCH</th> <th>MER PLP (dB)</th> <th>MER L1 (dB)</th> <th>C/I - MER plp (dB)</th> <th>margin (dB)</th> <th>MER-ref MER (dB)</th> <th>delta (dB)</th> </tr> </thead> <tbody> <tr><td>I=0</td><td>2.5</td><td>5.3E-05</td><td></td><td>41.2</td><td>39.2</td><td>4.4</td><td>18.5</td><td>17.3</td><td>-1.2</td></tr> <tr><td>40</td><td>2.8</td><td>5.6E-05</td><td></td><td>35.6</td><td>34.6</td><td>4.2</td><td>17.5</td><td>16.5</td><td>-1</td></tr> <tr><td>39</td><td>2.8</td><td>5.6E-05</td><td></td><td>34.8</td><td>33.9</td><td>4</td><td>16.5</td><td>15.7</td><td>-0.8</td></tr> <tr><td>38</td><td>2.8</td><td>5.6E-05</td><td></td><td>34</td><td>33.2</td><td>3.8</td><td>15.5</td><td>14.9</td><td>-0.6</td></tr> <tr><td>37</td><td>2.8</td><td>5.6E-05</td><td></td><td>33.2</td><td>32.4</td><td>3.7</td><td>14.5</td><td>14</td><td>-0.5</td></tr> <tr><td>36</td><td>2.9</td><td>5.8E-05</td><td></td><td>32.3</td><td>31.6</td><td>3.5</td><td>13.5</td><td>13.2</td><td>-0.3</td></tr> <tr><td>35</td><td>3</td><td>6.1E-05</td><td></td><td>31.5</td><td>30.7</td><td>3.5</td><td>13</td><td>12.7</td><td>-0.3</td></tr> <tr><td>34.5</td><td>3</td><td>6.6E-05</td><td></td><td>31</td><td>30.3</td><td>3.4</td><td>12.5</td><td>12.3</td><td>-0.2</td></tr> <tr><td>34</td><td>3</td><td>7.9E-05</td><td></td><td>30.6</td><td>29.9</td><td>3.4</td><td>12</td><td>11.8</td><td>-0.2</td></tr> <tr><td>33.5</td><td>3</td><td>1.1E-04</td><td></td><td>30.1</td><td>29.4</td><td>3.4</td><td>11.5</td><td>11.3</td><td>-0.2</td></tr> <tr><td>33</td><td>3.1</td><td>1.7E-04</td><td></td><td>29.6</td><td>29</td><td>3</td><td>11</td><td>11.2</td><td>0.2 example #5</td></tr> <tr><td>32.5</td><td>3.1</td><td>2.9E-04</td><td></td><td>29.5</td><td>28.5</td><td>3.2</td><td>10.5</td><td>10.5</td><td>0</td></tr> <tr><td>32</td><td>3.2</td><td>5.2E-04</td><td></td><td>28.8</td><td>28.1</td><td>3.2</td><td>10</td><td>10</td><td>0</td></tr> <tr><td>31.5</td><td>3.3</td><td>8.8E-04</td><td></td><td>28.3</td><td>27.6</td><td>3.2</td><td>9.5</td><td>9.5</td><td>0</td></tr> <tr><td>31</td><td>3.5</td><td>1.5E-03</td><td></td><td>27.8</td><td>27.2</td><td>3.2</td><td>9</td><td>9</td><td>0</td></tr> <tr><td>30.5</td><td>3.6</td><td>2.4E-03</td><td></td><td>27.3</td><td>26.7</td><td>3.2</td><td>8.5</td><td>8.5</td><td>0</td></tr> <tr><td>30</td><td>3.7</td><td>3.6E-03</td><td></td><td>26.8</td><td>26.2</td><td>3.2</td><td>8</td><td>8</td><td>0</td></tr> <tr><td>29.5</td><td>3.9</td><td>5.3E-03</td><td></td><td>26.3</td><td>25.8</td><td>3.2</td><td>7.5</td><td>7.5</td><td>0</td></tr> <tr><td>29</td><td>4.2</td><td>7.4E-03</td><td></td><td>25.8</td><td>25.3</td><td>3.3</td><td>7</td><td>6.9</td><td>-0.1</td></tr> <tr><td>28.5</td><td>4.5</td><td>1.0E-02</td><td></td><td>25.2</td><td>24.8</td><td>3.3</td><td>6.5</td><td>6.4</td><td>-0.1 example #12</td></tr> <tr><td>28</td><td>4.7</td><td>1.3E-02</td><td></td><td>24.7</td><td>24.3</td><td>3.3</td><td>6</td><td>5.9</td><td>-0.1</td></tr> <tr><td>27.5</td><td>5.1</td><td>1.7E-02</td><td></td><td>24.2</td><td>23.8</td><td>3.3</td><td>5.5</td><td>5.4</td><td>-0.1</td></tr> <tr><td>27</td><td>5.5</td><td>2.1E-02</td><td></td><td>23.7</td><td>23.3</td><td>3.4</td><td>5</td><td>4.8</td><td>-0.2</td></tr> <tr><td>26.5</td><td>5.9</td><td>2.5E-02</td><td></td><td>23.1</td><td>22.8</td><td>3.5</td><td>4.5</td><td>4.2</td><td>-0.3</td></tr> <tr><td>26</td><td>6.3</td><td>3.0E-02</td><td></td><td>22.5</td><td>22.3</td><td>3.6</td><td>4</td><td>3.6</td><td>-0.4</td></tr> <tr><td>25.5</td><td>6.8</td><td>3.5E-02</td><td></td><td>21.9</td><td>21.9</td><td>3.8</td><td>3.5</td><td>2.9</td><td>-0.6</td></tr> <tr><td>25</td><td>7.3</td><td>4.0E-02</td><td></td><td>21.2</td><td>21.4</td><td>4</td><td>3</td><td>2.2</td><td>-0.8</td></tr> <tr><td>24.5</td><td>7.9</td><td>4.6E-02</td><td></td><td>20.5</td><td>20.9</td><td>4.2</td><td>2.5</td><td>1.5</td><td>-1</td></tr> <tr><td>24</td><td>8.6</td><td>5.1E-02</td><td></td><td>19.8</td><td>20.4</td><td>4.4</td><td>2</td><td>0.8</td><td>-1.2 example #4</td></tr> <tr><td>23.5</td><td>9.5</td><td>5.7E-02</td><td></td><td>19.1</td><td>19.9</td><td>4.4</td><td>1.5</td><td>0.3</td><td>-1.2</td></tr> <tr><td>23</td><td>10.7</td><td>6.3E-02</td><td></td><td>18.6</td><td>19.4</td><td>4.4</td><td>1</td><td>-0.2</td><td>-1.2</td></tr> <tr><td>22.5</td><td>12.7</td><td>6.9E-02</td><td></td><td>18.1</td><td>18.9</td><td>4.3</td><td>0.5</td><td>-0.6</td><td>-1.1</td></tr> <tr><td>22</td><td>15.5</td><td>7.6E-02</td><td></td><td>17.7</td><td>18.4</td><td>4.2</td><td>0</td><td>-1</td><td>-1</td></tr> <tr><td>21.5</td><td>21.4</td><td>8.2E-02</td><td></td><td>17.3</td><td>17.9</td><td></td><td></td><td></td><td></td></tr> <tr><td>21</td><td>-</td><td>-</td><td>-</td><td>-</td><td>17.4</td><td></td><td></td><td></td><td></td></tr> </tbody> </table> | | results of measurements | | | | | | | | | | C/I (dB) | Iter numb | BER Before LDPC | BER Before BCH | MER PLP (dB) | MER L1 (dB) | C/I - MER plp (dB) | margin (dB) | MER-ref MER (dB) | delta (dB) | I=0 | 2.5 | 5.3E-05 | | 41.2 | 39.2 | 4.4 | 18.5 | 17.3 | -1.2 | 40 | 2.8 | 5.6E-05 | | 35.6 | 34.6 | 4.2 | 17.5 | 16.5 | -1 | 39 | 2.8 | 5.6E-05 | | 34.8 | 33.9 | 4 | 16.5 | 15.7 | -0.8 | 38 | 2.8 | 5.6E-05 | | 34 | 33.2 | 3.8 | 15.5 | 14.9 | -0.6 | 37 | 2.8 | 5.6E-05 | | 33.2 | 32.4 | 3.7 | 14.5 | 14 | -0.5 | 36 | 2.9 | 5.8E-05 | | 32.3 | 31.6 | 3.5 | 13.5 | 13.2 | -0.3 | 35 | 3 | 6.1E-05 | | 31.5 | 30.7 | 3.5 | 13 | 12.7 | -0.3 | 34.5 | 3 | 6.6E-05 | | 31 | 30.3 | 3.4 | 12.5 | 12.3 | -0.2 | 34 | 3 | 7.9E-05 | | 30.6 | 29.9 | 3.4 | 12 | 11.8 | -0.2 | 33.5 | 3 | 1.1E-04 | | 30.1 | 29.4 | 3.4 | 11.5 | 11.3 | -0.2 | 33 | 3.1 | 1.7E-04 | | 29.6 | 29 | 3 | 11 | 11.2 | 0.2 example #5 | 32.5 | 3.1 | 2.9E-04 | | 29.5 | 28.5 | 3.2 | 10.5 | 10.5 | 0 | 32 | 3.2 | 5.2E-04 | | 28.8 | 28.1 | 3.2 | 10 | 10 | 0 | 31.5 | 3.3 | 8.8E-04 | | 28.3 | 27.6 | 3.2 | 9.5 | 9.5 | 0 | 31 | 3.5 | 1.5E-03 | | 27.8 | 27.2 | 3.2 | 9 | 9 | 0 | 30.5 | 3.6 | 2.4E-03 | | 27.3 | 26.7 | 3.2 | 8.5 | 8.5 | 0 | 30 | 3.7 | 3.6E-03 | | 26.8 | 26.2 | 3.2 | 8 | 8 | 0 | 29.5 | 3.9 | 5.3E-03 | | 26.3 | 25.8 | 3.2 | 7.5 | 7.5 | 0 | 29 | 4.2 | 7.4E-03 | | 25.8 | 25.3 | 3.3 | 7 | 6.9 | -0.1 | 28.5 | 4.5 | 1.0E-02 | | 25.2 | 24.8 | 3.3 | 6.5 | 6.4 | -0.1 example #12 | 28 | 4.7 | 1.3E-02 | | 24.7 | 24.3 | 3.3 | 6 | 5.9 | -0.1 | 27.5 | 5.1 | 1.7E-02 | | 24.2 | 23.8 | 3.3 | 5.5 | 5.4 | -0.1 | 27 | 5.5 | 2.1E-02 | | 23.7 | 23.3 | 3.4 | 5 | 4.8 | -0.2 | 26.5 | 5.9 | 2.5E-02 | | 23.1 | 22.8 | 3.5 | 4.5 | 4.2 | -0.3 | 26 | 6.3 | 3.0E-02 | | 22.5 | 22.3 | 3.6 | 4 | 3.6 | -0.4 | 25.5 | 6.8 | 3.5E-02 | | 21.9 | 21.9 | 3.8 | 3.5 | 2.9 | -0.6 | 25 | 7.3 | 4.0E-02 | | 21.2 | 21.4 | 4 | 3 | 2.2 | -0.8 | 24.5 | 7.9 | 4.6E-02 | | 20.5 | 20.9 | 4.2 | 2.5 | 1.5 | -1 | 24 | 8.6 | 5.1E-02 | | 19.8 | 20.4 | 4.4 | 2 | 0.8 | -1.2 example #4 | 23.5 | 9.5 | 5.7E-02 | | 19.1 | 19.9 | 4.4 | 1.5 | 0.3 | -1.2 | 23 | 10.7 | 6.3E-02 | | 18.6 | 19.4 | 4.4 | 1 | -0.2 | -1.2 | 22.5 | 12.7 | 6.9E-02 | | 18.1 | 18.9 | 4.3 | 0.5 | -0.6 | -1.1 | 22 | 15.5 | 7.6E-02 | | 17.7 | 18.4 | 4.2 | 0 | -1 | -1 | 21.5 | 21.4 | 8.2E-02 | | 17.3 | 17.9 | | | | | 21 | - | - | - | - | 17.4 | | | | |
| results of measurements | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| C/I (dB) | Iter numb | BER Before LDPC | BER Before BCH | MER PLP (dB) | MER L1 (dB) | C/I - MER plp (dB) | margin (dB) | MER-ref MER (dB) | delta (dB) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| I=0 | 2.5 | 5.3E-05 | | 41.2 | 39.2 | 4.4 | 18.5 | 17.3 | -1.2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 40 | 2.8 | 5.6E-05 | | 35.6 | 34.6 | 4.2 | 17.5 | 16.5 | -1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 39 | 2.8 | 5.6E-05 | | 34.8 | 33.9 | 4 | 16.5 | 15.7 | -0.8 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 38 | 2.8 | 5.6E-05 | | 34 | 33.2 | 3.8 | 15.5 | 14.9 | -0.6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 37 | 2.8 | 5.6E-05 | | 33.2 | 32.4 | 3.7 | 14.5 | 14 | -0.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 36 | 2.9 | 5.8E-05 | | 32.3 | 31.6 | 3.5 | 13.5 | 13.2 | -0.3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 35 | 3 | 6.1E-05 | | 31.5 | 30.7 | 3.5 | 13 | 12.7 | -0.3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 34.5 | 3 | 6.6E-05 | | 31 | 30.3 | 3.4 | 12.5 | 12.3 | -0.2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 34 | 3 | 7.9E-05 | | 30.6 | 29.9 | 3.4 | 12 | 11.8 | -0.2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 33.5 | 3 | 1.1E-04 | | 30.1 | 29.4 | 3.4 | 11.5 | 11.3 | -0.2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 33 | 3.1 | 1.7E-04 | | 29.6 | 29 | 3 | 11 | 11.2 | 0.2 example #5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 32.5 | 3.1 | 2.9E-04 | | 29.5 | 28.5 | 3.2 | 10.5 | 10.5 | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 32 | 3.2 | 5.2E-04 | | 28.8 | 28.1 | 3.2 | 10 | 10 | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 31.5 | 3.3 | 8.8E-04 | | 28.3 | 27.6 | 3.2 | 9.5 | 9.5 | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 31 | 3.5 | 1.5E-03 | | 27.8 | 27.2 | 3.2 | 9 | 9 | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 30.5 | 3.6 | 2.4E-03 | | 27.3 | 26.7 | 3.2 | 8.5 | 8.5 | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 30 | 3.7 | 3.6E-03 | | 26.8 | 26.2 | 3.2 | 8 | 8 | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 29.5 | 3.9 | 5.3E-03 | | 26.3 | 25.8 | 3.2 | 7.5 | 7.5 | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 29 | 4.2 | 7.4E-03 | | 25.8 | 25.3 | 3.3 | 7 | 6.9 | -0.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 28.5 | 4.5 | 1.0E-02 | | 25.2 | 24.8 | 3.3 | 6.5 | 6.4 | -0.1 example #12 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 28 | 4.7 | 1.3E-02 | | 24.7 | 24.3 | 3.3 | 6 | 5.9 | -0.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 27.5 | 5.1 | 1.7E-02 | | 24.2 | 23.8 | 3.3 | 5.5 | 5.4 | -0.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 27 | 5.5 | 2.1E-02 | | 23.7 | 23.3 | 3.4 | 5 | 4.8 | -0.2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 26.5 | 5.9 | 2.5E-02 | | 23.1 | 22.8 | 3.5 | 4.5 | 4.2 | -0.3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 26 | 6.3 | 3.0E-02 | | 22.5 | 22.3 | 3.6 | 4 | 3.6 | -0.4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 25.5 | 6.8 | 3.5E-02 | | 21.9 | 21.9 | 3.8 | 3.5 | 2.9 | -0.6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 25 | 7.3 | 4.0E-02 | | 21.2 | 21.4 | 4 | 3 | 2.2 | -0.8 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 24.5 | 7.9 | 4.6E-02 | | 20.5 | 20.9 | 4.2 | 2.5 | 1.5 | -1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 24 | 8.6 | 5.1E-02 | | 19.8 | 20.4 | 4.4 | 2 | 0.8 | -1.2 example #4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 23.5 | 9.5 | 5.7E-02 | | 19.1 | 19.9 | 4.4 | 1.5 | 0.3 | -1.2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 23 | 10.7 | 6.3E-02 | | 18.6 | 19.4 | 4.4 | 1 | -0.2 | -1.2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 22.5 | 12.7 | 6.9E-02 | | 18.1 | 18.9 | 4.3 | 0.5 | -0.6 | -1.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 22 | 15.5 | 7.6E-02 | | 17.7 | 18.4 | 4.2 | 0 | -1 | -1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 21.5 | 21.4 | 8.2E-02 | | 17.3 | 17.9 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 21 | - | - | - | - | 17.4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| * 1 useful signal plus 1 interference outside GI | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ** MER "at failure" (1 useful @ level -50 dBm + noise) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |



| 'derived' parameters | | | | |
|----------------------|-------------|------------------|------------------|--|
| C/I - MER plp (dB) | margin (dB) | MER-ref MER (dB) | delta (dB) | |
| 4.4 | 18.5 | 17.3 | -1.2 | |
| 4.2 | 17.5 | 16.5 | -1 | |
| 4 | 16.5 | 15.7 | -0.8 | |
| 3.8 | 15.5 | 14.9 | -0.6 | |
| 3.7 | 14.5 | 14 | -0.5 | |
| 3.5 | 13.5 | 13.2 | -0.3 | |
| 3.5 | 13 | 12.7 | -0.3 | |
| 3.4 | 12.5 | 12.3 | -0.2 | |
| 3.4 | 12 | 11.8 | -0.2 | |
| 3.4 | 11.5 | 11.3 | -0.2 | |
| 3 | 11 | 11.2 | 0.2 example #5 | |
| 3.2 | 10.5 | 10.5 | 0 | |
| 3.2 | 10 | 10 | 0 | |
| 3.2 | 9.5 | 9.5 | 0 | |
| 3.2 | 9 | 9 | 0 | |
| 3.2 | 8.5 | 8.5 | 0 | |
| 3.2 | 8 | 8 | 0 | |
| 3.2 | 7.5 | 7.5 | 0 | |
| 3.3 | 7 | 6.9 | -0.1 | |
| 3.3 | 6.5 | 6.4 | -0.1 example #12 | |
| 3.3 | 6 | 5.9 | -0.1 | |
| 3.3 | 5.5 | 5.4 | -0.1 | |
| 3.4 | 5 | 4.8 | -0.2 | |
| 3.5 | 4.5 | 4.2 | -0.3 | |
| 3.6 | 4 | 3.6 | -0.4 | |
| 3.8 | 3.5 | 2.9 | -0.6 | |
| 4 | 3 | 2.2 | -0.8 | |
| 4.2 | 2.5 | 1.5 | -1 | |
| 4.4 | 2 | 0.8 | -1.2 example #4 | |
| 4.4 | 1.5 | 0.3 | -1.2 | |
| 4.4 | 1 | -0.2 | -1.2 | |
| 4.3 | 0.5 | -0.6 | -1.1 | |
| 4.2 | 0 | -1 | -1 | |

C/I = 33 is used in example #5

C/I = 28 is used in example #12

C/I = 24.5 is used in example #4

FIGURE A2.1
SFN: 1 Useful signal + 1 interference @600 µs
(data from Table A2.2)

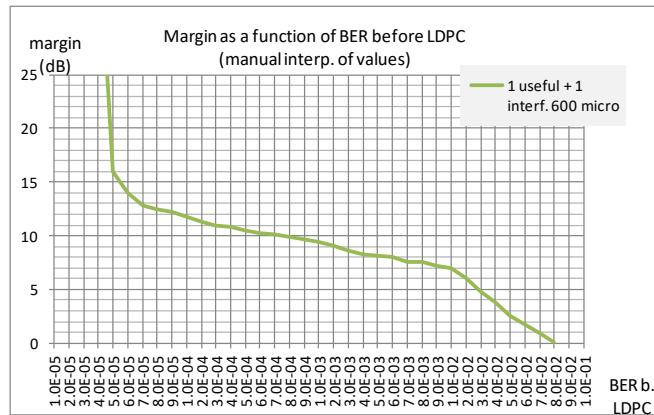


TABLE A2.3
SFN: 1 Useful signal + 1 interference @300 µs
(just outside the GI)

| date 05.02.2018 | | | |
|-------------------------|-------------|--------------------|----------------|
| time | | | |
| generator SFU | | | |
| receiver A1 | | | |
| MFN/SFN | SFN | | |
| Measurement type | Pr. Ratio * | | |
| CH | 38 | | |
| Level | -50 | dBm | |
| IFT, PP | 32kn, PP2 | | |
| GI | 1/16 | | |
| GI duration | 224 | us (nominal value) | |
| P LP Mod | 256QAM | | |
| P LP Code | 2/3 | | |
| L1 mod | 16QAM | | |
| difference MER ** | 18.3 dB | | |
| results of measurements | | | |
| C/I (dB) | Iter. | BER Before LDPC | BER Before BCH |
| 40 | 2.5 | 4.9E-05 | 36.4 |
| 39 | 2.5 | 4.9E-05 | 37.1 |
| 29 | 2.5 | 4.9E-05 | 37.5 |
| 28 | 2.7 | 5.0E-05 | 37.4 |
| 27 | 2.6 | 5.1E-05 | 36.8 |
| 26 | 2.6 | 5.2E-05 | 36.2 |
| 25 | 2.7 | 5.2E-05 | 35.5 |
| 24 | 2.8 | 5.5E-05 | 34.8 |
| 23 | 2.8 | 6.2E-05 | 34 |
| 22 | 2.9 | 7.5E-05 | 33.2 |
| 21 | 3 | 1.2E-04 | 32.3 |
| 20 | 3 | 2.2E-04 | 31.4 |
| 19 | 3.1 | 4.6E-04 | 30.5 |
| 18 | 3.3 | 9.9E-04 | 29.6 |
| 17 | 3.5 | 2.0E-03 | 28.9 |
| 16 | 3.8 | 3.7E-03 | 28 |
| 15 | 4.3 | 6.4E-03 | 27.1 |
| 14 | 4.7 | 1.0E-02 | 26.2 |
| 13 | 5.4 | 1.6E-02 | 25.4 |
| 12 | 6.2 | 2.3E-02 | 24.5 |
| 11 | 7.1 | 3.1E-02 | 23.6 |
| 10 | 8.2 | 4.0E-02 | 22.6 |
| 9 | 9.9 | 5.2E-02 | 21.3 |
| 8 | 12.6 | 6.3E-02 | 19.6 |
| 7 | 17.9 | 7.7E-02 | 18.1 |
| 6.5 | 24 | 8.4E-02 | 17.5 |
| 6 | | | 16 |

*1 useful signal plus 1 interference outside GI
** MER "at failure" (1 useful @ level -50 dBm + noise)

useful "C" = 0 @ 0 microseconds
interf. "I" = @ 300 microseconds

Path#1 (SFNuseful)
-0 dB

Path#2 (SFNinterf)
(this level varying in time)

0 20 180 224 300 delay (µs)

"derived" parameters

| C/I - MER | margin | MER-ref | delta |
|-----------|--------|---------|-------|
| (dB) | (dB) | (dB) | (dB) |
| -8.4 | 23 | 20.3 | -2.9 |
| -8.5 | 22 | 19.3 | -2.8 |
| -9.4 | 21 | 19.3 | -1.9 |
| -9.8 | 20 | 18.5 | -1.5 |
| -10.2 | 19 | 17.9 | -1.1 |
| -10.5 | 18 | 17.2 | -0.8 |
| -10.8 | 17 | 16.5 | -0.5 |
| -11.0 | 16 | 15.7 | -0.3 |
| -11.2 | 15 | 14.9 | -0.1 |
| -11.3 | 14 | 14 | 0 |
| -11.4 | 13 | 13.1 | 0.1 |
| -11.5 | 12 | 12.2 | 0.2 |
| -11.6 | 11 | 11.3 | 0.3 |
| -11.9 | 10 | 10.6 | 0.6 |
| -12.0 | 9 | 9.7 | 0.7 |
| -12.1 | 8 | 8.8 | 0.8 |
| -12.2 | 7 | 7.9 | 0.9 |
| -12.4 | 6 | 7.1 | 1.1 |
| -12.5 | 5 | 6.2 | 1.2 |
| -12.6 | 4 | 5.3 | 1.3 |
| -12.6 | 3 | 4.3 | 1.3 |
| -12.3 | 2 | 3 | 1 |
| -11.6 | 1 | 1.3 | 0.3 |
| -11.1 | 0 | -0.2 | -0.2 |

C/I = 17 is used in example #6

FIGURE A2.2
SFN: 1 Useful signal + 1 interference @300 µs
(data from Table A2.3)



TABLE A2.4

SFN: 2 Useful signal + 1 interference @600 μs

| | date | 06.02.2018 (Tuesday) | | | | |
|-------------------------|-------------|----------------------|-----------------|--------------|-------------|------|
| | time | PM | | | | |
| generator | SFU | | | | | |
| receiver | A1 | | | | | |
| MFN/SFN | SFN | | | | | |
| Measurem. type | Pr. Ratio * | | | | | |
| CH | 38 | | | | | |
| Level | -50 | dBm | | | | |
| FFT, PP | 32kn, PP2 | | | | | |
| GI | 1/16 | | | | | |
| GI duration | 224 | μs | (nominal value) | | | |
| PLP Mod | 256QAM | | | | | |
| PLP Code | 2/3 | | | | | |
| L1 mod | 16 QAM | | | | | |
| reference MER ** | 18.3 dB | | | | | |
| results of measurements | | | | | | |
| C/I (dB) | Iter numb. | BER Before LDPC | BER Before BCH | MER PLP (dB) | MER L1 (dB) | |
| I=0 | 3.2 | 5.6E-05 | | 40.2 | 38.6 | |
| 40 | 3.3 | 5.9E-05 | | 34.9 | 34.1 | |
| 39 | 3.3 | 6.0E-05 | | 34.4 | 33.4 | |
| 38 | 3.3 | 6.4E-05 | | 33.4 | 32.7 | |
| 37 | 3.4 | 7.6E-05 | | 32.6 | 32 | |
| 36 | 3.5 | 1.1E-04 | | 31.8 | 31.1 | |
| 35 | 3.5 | 2.3E-04 | | 30.9 | 30.3 | |
| 34 | 3.6 | 5.1E-04 | | 30.1 | 29.4 | |
| 33 | 3.7 | 1.1E-03 | | 29.2 | 28.5 | |
| 32 | 3.9 | 2.3E-03 | | 28.4 | 27.6 | |
| 31 | 4.1 | 4.2E-03 | | 27.5 | 26.7 | |
| 30 | 4.5 | 7.1E-03 | | 26.6 | 25.7 | |
| 29 | 4.8 | 1.1E-02 | | 25.7 | 24.8 | |
| 28 | 5.4 | 1.7E-02 | | 24.7 | 23.8 | |
| 27 | 6 | 2.4E-02 | | 23.7 | 22.9 | |
| 26 | 6.7 | 3.3E-02 | | 22.6 | 21.9 | |
| 25 | 7.6 | 4.2E-02 | | 21.2 | 20.9 | |
| 24.5 | | | | | | |
| 24 | 9 | 5.3E-02 | | 19.6 | 19.9 | |
| 23.5 | | | | | | |
| 23 | 11.1 | 6.5E-02 | | 18.3 | 18.9 | |
| 22.5 | | | | | | |
| ok | 22 | 15.5 | 7.8E-02 | | 17.3 | 17.9 |
| ok | 21.6 | 19.9 | 8.3E-02 | | 16.9 | 17.6 |
| KO | 21.5 | 21.5 | 8.5E-02 | 4.2E-06 | 16.8 | 17.4 |
| KO | 21.4 | 24.5 | 8.6E-02 | 2.4E-06 | 16.7 | 17.3 |
| KO | 21 | - | - | - | - | 17.4 |

FIGURE A2.3
SFN: 2 Useful signal + 1 interference @600 μ s
(data from Table A2.4)

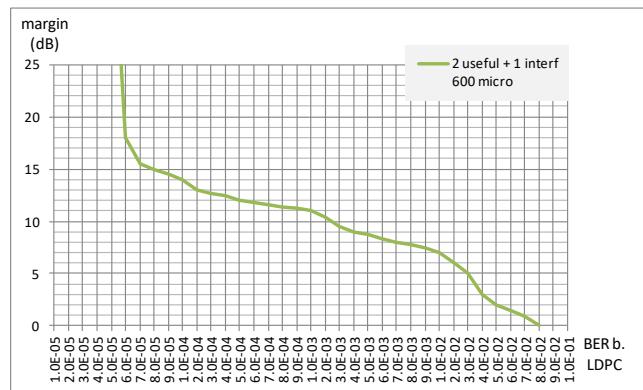


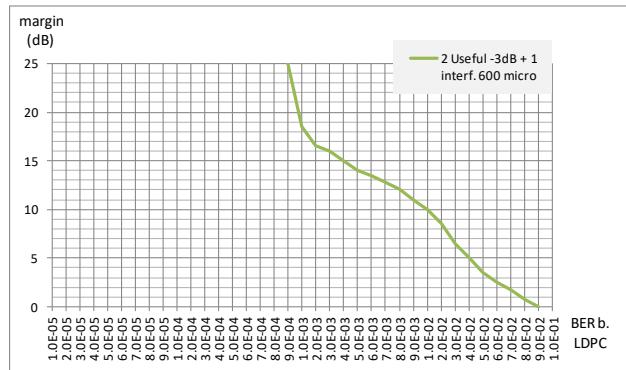
TABLE A2.5
SFN: 2 Useful signal (0, -3 dB) + 1 interference @600 μ s

| | | date 08.02.2018 | | | | | | | |
|-------------------------|-------------|-----------------|-----------------|---------|-------------|---------------------|--------|---------|-------|
| | | time AM | | | | | | | |
| | | generator SFU | | | | | | | |
| receiver | | | | | | | | | |
| MFN/SFN | SFN | | | | | | | | |
| Measurem. type | Pr. Ratio * | | | | | | | | |
| CH | 38 | | | | | | | | |
| Level | -50 | dBm | | | | | | | |
| FFT, PP | 32Kn, PP2 | | | | | | | | |
| GI | 1/16 | | | | | | | | |
| GI duration | 224 | μs | (nominal value) | | | | | | |
| PLP Mod | 256QAM | | | | | | | | |
| PLP Code | 2/3 | | | | | | | | |
| L1 mod | 16 QAM | | | | | | | | |
| reference MER ** | 18.3 dB | | | | | | | | |
| results of measurements | | | | | | | | | |
| C/I (dB) | Iter. numb. | BER Before LDPC | BER Before BCH | MER PLP | MER L1 (dB) | derived* parameters | | | |
| I=0 | 4.8 | 7.1E-05 | | 36.6 | 35.9 | C/I-MER | margin | MER-ref | delta |
| | 40 | 5.1 | 1.2E-03 | | 32.3 | 18.5 | 14 | -4.5 | |
| | 39 | 5.2 | 1.7E-03 | | 31.8 | 31 | 17.5 | 13.5 | -4 |
| | 38 | 5.2 | 2.4E-03 | | 31.2 | 30.4 | 16.5 | 12.9 | -3.6 |
| | 37 | 5.3 | 3.3E-03 | | 30.6 | 29.4 | 15.5 | 12.3 | -3.2 |
| | 36 | 5.5 | 4.4E-03 | | 30 | 28.7 | 14.5 | 11.7 | -2.8 |
| | 35 | 5.6 | 5.9E-03 | | 29.4 | 28 | 13.5 | 11.1 | -2.4 |
| | 34 | 5.7 | 7.7E-03 | | 28.9 | 27.1 | 12.5 | 10.6 | -1.9 |
| | 33 | 5.8 | 9.8E-03 | | 28.3 | 26.3 | 11.5 | 10 | -1.5 |
| | 32 | 6 | 1.2E-02 | | 27.7 | 25.3 | 10.5 | 9.4 | -1.1 |
| | 31 | 6.1 | 1.5E-02 | | 27 | 24.4 | 9.5 | 8.7 | -0.8 |
| | 30 | 6.3 | 1.9E-02 | | 26.2 | 23.5 | 8.5 | 7.9 | -0.6 |
| | 29 | 6.6 | 2.4E-02 | | 25.4 | 22.5 | 7.5 | 7.1 | -0.4 |
| | 28 | 7 | 2.9E-02 | | 24.4 | 21.5 | 6.5 | 6.1 | -0.4 |
| | 27 | 7.4 | 3.5E-02 | | 23.2 | 20.6 | 5.5 | 4.9 | -0.6 |
| | 26 | 8 | 4.2E-02 | | 21.5 | 19.6 | 4.5 | 3.7 | -1.3 |
| | 25 | 8.9 | 5.1E-02 | | 19 | 18.6 | 3.5 | 0.7 | 2.8 |
| | 24 | 10 | 6.1E-02 | | 17.4 | 17.6 | 2.5 | -0.9 | -3.4 |
| | 23 | 12 | 7.3E-02 | | 16 | 16.6 | 1.5 | -2.3 | 3.8 |
| | 22 | 15.9 | 8.5E-02 | | 14.7 | 15.6 | 0.5 | -3.6 | -4.1 |
| ok | 21.5 | 20.2 | 9.1E-02 | | 14 | 15.1 | 7.5 | 0 | -4.3 |
| ok | 21.4 | 21.7 | 9.3E-02 | | 13.9 | 15 | | | |
| ok | 21.3 | 23.4 | 9.4E-02 | | 13.7 | 14.9 | | | |
| ok | 21.2 | 26 | 9.5E-02 | | 13.6 | 14.8 | | | |
| KO | 21.1 | 30 | 9.7E-02 | 5.1E-05 | 13.5 | 14.7 | | | |
| KO | 21 | 35 | 9.8E-02 | 1.8E-03 | 13.3 | 14.7 | | | |

* 2 useful signal (near echo 0 dB) plus 1 interference outside GI
** MER "at failure" (1 useful @ level -50 dBm + noise)

FIGURE A2.4

**SFN: 2 Useful signal (0, -3 dB) + 1 interference @600 μs
(data from Table A2.5)**



The profile used to obtain Table A2.5 is similar to the case of “0 dB echo”.

TABLE A2.6

SFN: 3 Useful signal + 1 interference @600 μs

FIGURE A2.5
SFN: 3 Useful signal + 1 interference @600 μ s
(data from Table A2.6)

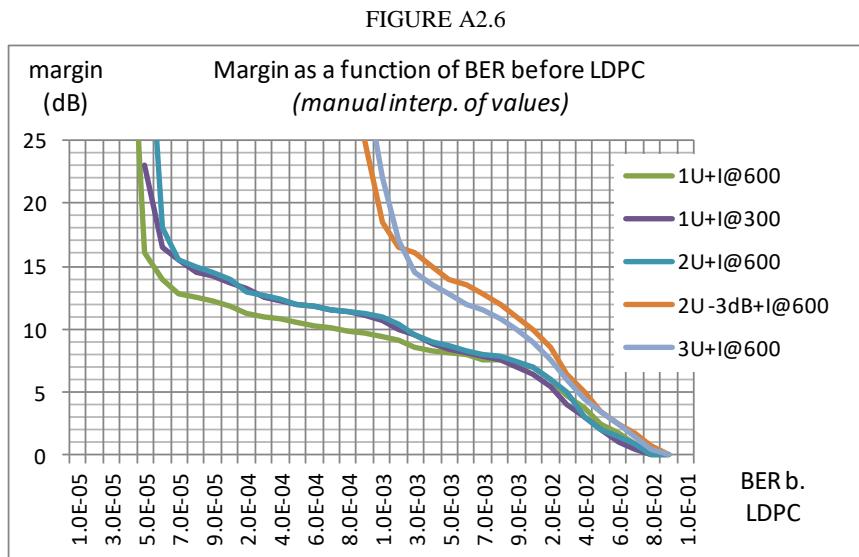
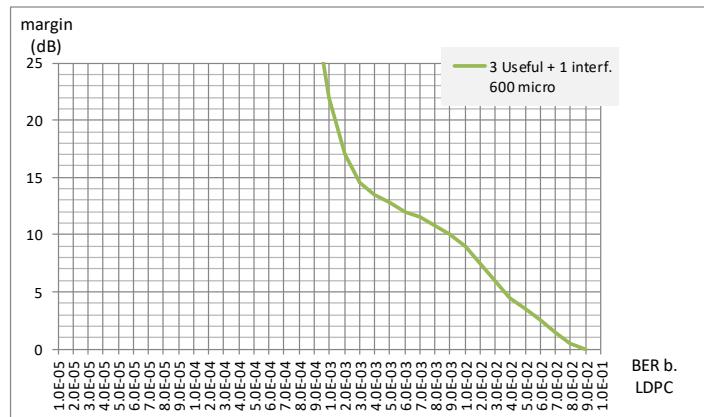


Figure A2.6 shows the margin as a function of BER before LDPC (with manual interpolation of values) derived from the examples of Tables A2.1, A2.3, A2.4, A2.5, A2.6 for the mode 32 k not extended, PP2, GI 1/16, 256QAM, code rate 2/3.

In the following pages, Tables A2.7 and A2.8 are illustrated. They are related to mode 32 k not extended, PP2, GI 1/16, 256QAM, code rate 3/5 and show the behavior of SFN with one useful path and one interference outside the Guard Interval at 600 μ s and 350 μ s, respectively.

TABLE A2.7

SFN: 1 Useful signal + 1 interference @600 µs
Mode 256QAM, code 3/5

| | | | | | | | | |
|--|-------------------------|-----------------|-----------------|--------------|-------------|------|--|--|
| | date | 09/08/18 | | | | | | |
| | time | | | | | | | |
| | generator SFU | | | | | | | |
| | receiver A2 | | | | | | | |
| MFN/SFN | SFN | | | | | | | |
| Measurem. type | Pr. Ratio * | | | | | | | |
| CH | 38 | 610 MHz | | | | | | |
| Level | -50 | dBm | | | | | | |
| FFT, PP | 32kn, PP2 | | | | | | | |
| GI | 1/16 | | | | | | | |
| GI duration | 224 | µs | (nominal value) | | | | | |
| PLP Mod | 256QAM | | | | | | | |
| PLP Code | 3/5 | | | | | | | |
| * 1 useful signal plus 1 interference outside GI | | | | | | | | |
| reference MER (MFN) | 17.1 | dB | Bei * | | | | | |
| reference C/I | 20 | dB | Bei * | | | | | |
| | | | | | | | | |
| | results of measurements | | | | | | | |
| C/I (dB) | Iter num. | BER Before LDPC | BER Before BCH | MER PLP (dB) | MER L1 (dB) | | | |
| Echo off | 3.5 | 5.9E-05 | | 40.3 | 38.5 | | | |
| 40.0 | 3.5 | 6.0E-05 | | 35.3 | 34.3 | | | |
| 39.0 | 3.5 | 6.0E-05 | | 34.6 | 33.7 | | | |
| 38.0 | 3.5 | 6.0E-05 | | 33.8 | 33.0 | | | |
| 37.0 | 3.6 | 6.1E-05 | | 33.1 | 32.3 | | | |
| 36.0 | 3.6 | 6.2E-05 | | 32.2 | 31.5 | | | |
| 35.0 | 3.6 | 6.7E-05 | | 31.4 | 30.6 | | | |
| 34.0 | 3.7 | 9.1E-05 | | 30.5 | 29.8 | | | |
| 33.0 | 3.8 | 2.0E-04 | | 29.6 | 28.9 | | | |
| 32.0 | 4.1 | 5.7E-04 | | 28.7 | 28.0 | | | |
| 31.0 | 4.4 | 1.6E-03 | | 27.8 | 27.1 | | | |
| 30.0 | 4.9 | 3.7E-03 | | 26.8 | 26.2 | | | |
| 29.0 | 5.5 | 7.5E-03 | | 25.7 | 25.2 | | | |
| 28.0 | 6.4 | 1.3E-02 | | 24.7 | 24.3 | | | |
| 27.0 | 7.6 | 2.1E-02 | | 23.7 | 23.3 | | | |
| 26.0 | 9.2 | 3.0E-02 | | 22.5 | 22.3 | | | |
| 25.0 | 11.2 | 4.0E-02 | | 21.3 | 21.4 | | | |
| 24.5 | 12.2 | 4.6E-02 | | 20.5 | 20.9 | | | |
| 24.0 | 13.7 | 5.1E-02 | | 19.8 | 20.4 | | | |
| 23.5 | 15.2 | 5.7E-02 | | 19.2 | 19.9 | | | |
| 23.0 | 17.0 | 6.3E-02 | | 18.6 | 19.4 | | | |
| 22.5 | 19.1 | 6.9E-02 | | 18.1 | 18.9 | | | |
| 22.0 | 22.0 | 7.6E-02 | | 17.8 | 18.4 | | | |
| 21.5 | 25.0 | 8.2E-02 | | 17.3 | 17.9 | | | |
| 21.0 | 28.9 | 8.9E-02 | | 16.9 | 17.4 | | | |
| 20.5 | 33.3 | 9.6E-02 | | 16.4 | 16.9 | | | |
| 20.0 | 36.0 | 1.0E-01 | 7.9E-08 | 15.8 | 16.4 | | | |
| *** | 19.9 | 36.1 | 1.0E-01 | 3.4E-07 | 15.8 | 16.3 | | |
| * | 19.7 | 36.3 | 1.1E-01 | 6.6E-06 | 15.5 | 16.1 | | |
| | | | | | | | | |
| C/I (dB) | Iter num. | BER Before LDPC | BER Before BCH | MER PLP (dB) | MER L1 (dB) | | | |

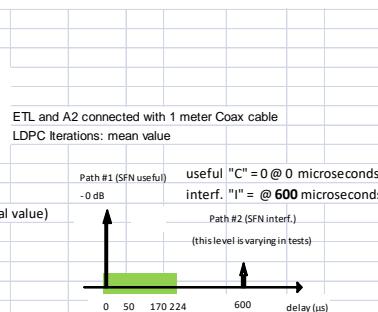
* visual failure point: where the picture is only just good (due to ESR5) in 0.1 dB steps

** receiver failure point: where measured values are still there (even only for a short time)

*** BER before BCH first time (0.1 dB steps) worst than 1E-07

TABLE A2.7

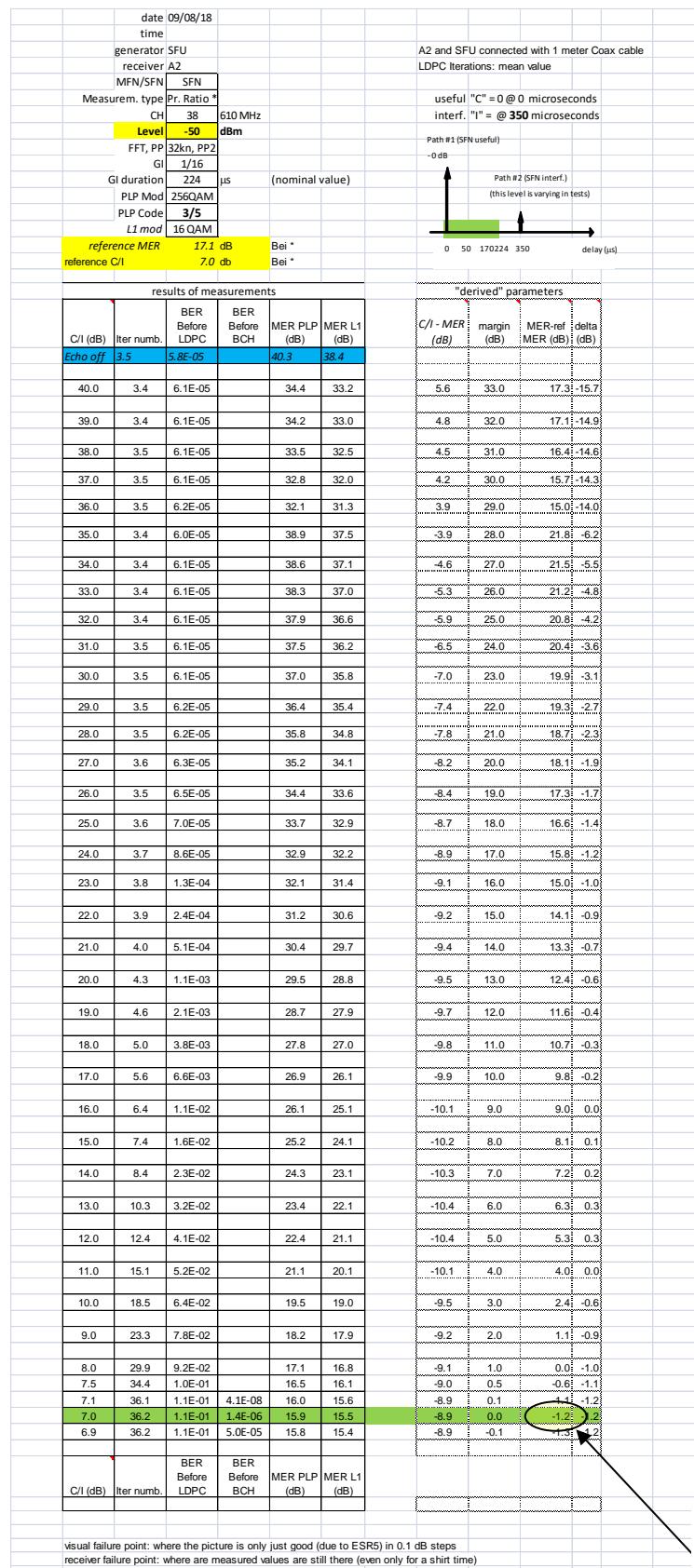
SFN: 1 Useful signal + 1 interference @600 µs
Mode 256QAM, code 3/5



| C/I - MER (dB) | margin (dB) | MER-ref (dB) | delta (dB) |
|----------------|-------------|--------------|------------|
| 4.7 | 20.0 | 18.2 | -1.8 |
| 4.4 | 19.0 | 17.5 | -1.5 |
| 4.2 | 18.0 | 16.7 | -1.3 |
| 3.9 | 17.0 | 16.0 | -1.0 |
| 3.8 | 16.0 | 15.1 | -0.9 |
| 3.6 | 15.0 | 14.3 | -0.7 |
| 3.5 | 14.0 | 13.4 | -0.6 |
| 3.4 | 13.0 | 12.5 | -0.5 |
| 3.3 | 12.0 | 11.6 | -0.4 |
| 3.2 | 11.0 | 10.7 | -0.3 |
| 3.2 | 10.0 | 9.7 | -0.3 |
| 3.3 | 9.0 | 8.6 | -0.4 |
| 3.3 | 8.0 | 7.6 | -0.4 |
| 3.3 | 7.0 | 6.6 | -0.4 |
| 3.5 | 6.0 | 5.4 | -0.6 |
| 3.7 | 5.0 | 4.2 | -0.8 |
| 4.0 | 4.5 | 3.4 | -1.1 |
| 4.2 | 4.0 | 2.7 | -1.3 |
| 4.3 | 3.5 | 2.1 | -1.4 |
| 4.4 | 3.0 | 1.5 | -1.5 |
| 4.4 | 2.5 | 1.0 | -1.5 |
| 4.2 | 2.0 | 0.7 | -1.3 |
| 4.2 | 1.5 | 0.2 | -1.3 |
| 4.1 | 1.0 | -0.2 | -1.2 |
| 4.2 | 0.0 | -1.3 | -1.3 |
| 4.1 | -0.1 | -1.3 | -1.2 |
| 4.2 | -0.3 | -1.6 | -1.3 |

TABLE A2.8

SFN: 1 Useful signal + 1 interference @350 µs
Mode 256QAM, code 3/5



"Reference MER" value for this mode is 17.1 dB and 15.9 - 17.1 = -1.2 dB

Annex 3 to Part 1

Summary of the values needed to obtain the margin to the failure point

This Annex 3 to Part 1 summarizes for a number of DVB-T2 system variants the values of “reference MER”, Lc and $f(BER)$ that can be used in the two formulas, one for MFN and the other for SFN, to obtain the margin to the failure point following the procedure indicated in §§ 5.1 and 5.2.

The two formulas are shown below.

- MFN margin = MER – reference MER + $Lc_{mfn} + f(BER)_{mfn}$
- SFN margin = MER – reference MER + $Lc_{sfn} + f(BER)_{sfn}$

In particular, Lc is used to correct the results as a function of the received level, while $f(BER)$ is used to correct the non-linearity of MER as a function of the C/I .

Note that the reference MER has the same value for both the MFN case and the SFN case.

Furthermore, for the same modes, this Annex also summarizes the values of the additional factors, function of the BER Before LDPC and of the number of LDPC iterations, that can also be used to obtain the margin.

TABLE A3.1
32k not extended, PP2, 1/16, 256 QAM, 2/3

| | Ref MER | LDPC iter. and BER Tables | Lc | $f(BER)$ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|-----------------|---------|--|---|----------|---------|------|---------|------|---------|------|---------|------|---------|------|---------|-------|-----------------|--------|-------|-------|-------|------|-------|------|------|------|------|------|------|-------|--|-----|------|------|------|-----|-----|-----|-----|-----|---|---|-----|-----|-----|-----|-----|-----|-----|-----|-----|----------------------|-----|-----|-----|-----|---|-----|-----|-----|-----|-----|-----|-----|---|-----|-----|-----|-----|-----|-----|-----|---|-----|-----|-----|---|-----|-----|-----|---|---|-----|-----|---|---|-----|-----|---|---|---|--------------------------------|
| MFN | 18.3 dB | | <p>Lc</p> <table border="1"> <thead> <tr> <th>BER</th> <th>1e-2</th> <th>2e-2</th> <th>4e-2</th> </tr> </thead> <tbody> <tr><td>-63</td><td>0</td><td>0</td><td>0</td></tr> <tr><td>-64</td><td>0.5</td><td>0.18</td><td>0</td></tr> <tr><td>-65</td><td>0.85</td><td>0.28</td><td>0</td></tr> <tr><td>-66</td><td>1.35</td><td>0.65</td><td>0.25</td></tr> <tr><td>-67</td><td>2.1</td><td>0.9</td><td>0.28</td></tr> <tr><td>-68</td><td>3</td><td>1.4</td><td>0.4</td></tr> <tr><td>-69</td><td>6</td><td>2.2</td><td>0.7</td></tr> <tr><td>-70</td><td>6</td><td>3.5</td><td>1.2</td></tr> <tr><td>-71</td><td>6</td><td>6</td><td>1.9</td></tr> <tr><td>-72</td><td>6</td><td>6</td><td>3.1</td></tr> <tr><td>-73</td><td>6</td><td>6</td><td>6</td></tr> </tbody> </table> | BER | 1e-2 | 2e-2 | 4e-2 | -63 | 0 | 0 | 0 | -64 | 0.5 | 0.18 | 0 | -65 | 0.85 | 0.28 | 0 | -66 | 1.35 | 0.65 | 0.25 | -67 | 2.1 | 0.9 | 0.28 | -68 | 3 | 1.4 | 0.4 | -69 | 6 | 2.2 | 0.7 | -70 | 6 | 3.5 | 1.2 | -71 | 6 | 6 | 1.9 | -72 | 6 | 6 | 3.1 | -73 | 6 | 6 | 6 | Not relevant for MFN | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| BER | 1e-2 | 2e-2 | 4e-2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -63 | 0 | 0 | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -64 | 0.5 | 0.18 | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -65 | 0.85 | 0.28 | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -66 | 1.35 | 0.65 | 0.25 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -67 | 2.1 | 0.9 | 0.28 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -68 | 3 | 1.4 | 0.4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -69 | 6 | 2.2 | 0.7 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -70 | 6 | 3.5 | 1.2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -71 | 6 | 6 | 1.9 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -72 | 6 | 6 | 3.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -73 | 6 | 6 | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SFN | 18.3 dB | <table border="1"> <thead> <tr> <th>BER before LDPC</th> <th>margin</th> </tr> </thead> <tbody> <tr><td><= 8E-2</td><td>>= 0</td></tr> <tr><td><= 6E-2</td><td>>= 2</td></tr> <tr><td><= 4E-2</td><td>>= 3</td></tr> <tr><td><= 1E-2</td><td>>= 6</td></tr> <tr><td><= 1E-3</td><td>>= 9</td></tr> <tr><td><= 1E-4</td><td>>= 11</td></tr> </tbody> </table> <table border="1"> <thead> <tr> <th>LDPC iterations</th> <th>margin</th> </tr> </thead> <tbody> <tr><td><= 20</td><td>>= -1</td></tr> <tr><td><= 15</td><td>>= 0</td></tr> <tr><td><= 10</td><td>>= 2</td></tr> <tr><td><= 6</td><td>>= 4</td></tr> <tr><td><= 5</td><td>>= 6</td></tr> <tr><td><= 3</td><td>>= 10</td></tr> </tbody> </table> | BER before LDPC | margin | <= 8E-2 | >= 0 | <= 6E-2 | >= 2 | <= 4E-2 | >= 3 | <= 1E-2 | >= 6 | <= 1E-3 | >= 9 | <= 1E-4 | >= 11 | LDPC iterations | margin | <= 20 | >= -1 | <= 15 | >= 0 | <= 10 | >= 2 | <= 6 | >= 4 | <= 5 | >= 6 | <= 3 | >= 10 | <p>Lc_{sfn}</p> <table border="1"> <thead> <tr> <th>BER</th> <th>1e-2</th> <th>2e-2</th> <th>4e-2</th> </tr> </thead> <tbody> <tr><td>-60</td><td>0.1</td><td>0</td><td>0</td></tr> <tr><td>-61</td><td>0</td><td>0</td><td>0.1</td></tr> <tr><td>-62</td><td>0.1</td><td>0.1</td><td>0.2</td></tr> <tr><td>-63</td><td>0.4</td><td>0.2</td><td>0.3</td></tr> <tr><td>-64</td><td>0.7</td><td>0.4</td><td>0.4</td></tr> <tr><td>-65</td><td>1</td><td>0.6</td><td>0.5</td></tr> <tr><td>-66</td><td>1.4</td><td>0.8</td><td>0.6</td></tr> <tr><td>-67</td><td>2</td><td>1.1</td><td>0.7</td></tr> <tr><td>-68</td><td>3.3</td><td>1.6</td><td>0.8</td></tr> <tr><td>-69</td><td>6</td><td>2.4</td><td>1.1</td></tr> <tr><td>-70</td><td>6</td><td>3.8</td><td>1.5</td></tr> <tr><td>-71</td><td>6</td><td>6</td><td>2.3</td></tr> <tr><td>-72</td><td>6</td><td>6</td><td>3.6</td></tr> <tr><td>-73</td><td>6</td><td>6</td><td>6</td></tr> </tbody> </table> | BER | 1e-2 | 2e-2 | 4e-2 | -60 | 0.1 | 0 | 0 | -61 | 0 | 0 | 0.1 | -62 | 0.1 | 0.1 | 0.2 | -63 | 0.4 | 0.2 | 0.3 | -64 | 0.7 | 0.4 | 0.4 | -65 | 1 | 0.6 | 0.5 | -66 | 1.4 | 0.8 | 0.6 | -67 | 2 | 1.1 | 0.7 | -68 | 3.3 | 1.6 | 0.8 | -69 | 6 | 2.4 | 1.1 | -70 | 6 | 3.8 | 1.5 | -71 | 6 | 6 | 2.3 | -72 | 6 | 6 | 3.6 | -73 | 6 | 6 | 6 | $f(BER)$ for level > -60 dBm |
| BER before LDPC | margin | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 8E-2 | >= 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 6E-2 | >= 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 4E-2 | >= 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 1E-2 | >= 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 1E-3 | >= 9 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 1E-4 | >= 11 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| LDPC iterations | margin | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 20 | >= -1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 15 | >= 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 10 | >= 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 6 | >= 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 5 | >= 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 3 | >= 10 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| BER | 1e-2 | 2e-2 | 4e-2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -60 | 0.1 | 0 | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -61 | 0 | 0 | 0.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -62 | 0.1 | 0.1 | 0.2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -63 | 0.4 | 0.2 | 0.3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -64 | 0.7 | 0.4 | 0.4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -65 | 1 | 0.6 | 0.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -66 | 1.4 | 0.8 | 0.6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -67 | 2 | 1.1 | 0.7 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -68 | 3.3 | 1.6 | 0.8 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -69 | 6 | 2.4 | 1.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -70 | 6 | 3.8 | 1.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -71 | 6 | 6 | 2.3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -72 | 6 | 6 | 3.6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -73 | 6 | 6 | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

TABLE A3.2

Results* (AWGN interference limited) with different input levels (MFN)
(32k not extended, PP2, 1/16, 256 QAM, 2/3)

| MFN | | reference MER (dB) 18.3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|------------|----------------|--------------------------------|--------------|-------------|------------------------|-----------------|--------------|-------------|------------------------|-----------------|--------------|-------------|------------------------|-----------------|--------------|-------------|------------------------|-----------------|--------------|-------------|------------------------|-----------------|--------------|-------------|------------------------|-----------------|--------------|-------------|------------------------|-----|-------|---------|------|-----|-----|------|
| | | -50 | | | | | -60 | | | | | -65 | | | | | -68 | | | | | -69 | | | | | -70 | | | | | | | | | |
| C/I (dB) | margin ** (dB) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER - ref MER (dB) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER - ref MER (dB) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER - ref MER (dB) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER - ref MER (dB) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER - ref MER (dB) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER - ref MER (dB) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER - ref MER (dB) | | | | | | | |
| <i>j=0</i> | | 5.7E-05 | 41.4 | | | 6.2E-05 | 34.9 | | | 1.8E-04 | 30.3 | | | 2.9E-03 | 27.3 | | | 5.9E-03 | 26.3 | | | 9.7E-03 | 25.4 | | | 2.5E-02 | 23.4 | | | | | | | | | |
| 40 | 20 | 6.0E-05 | 36.9 | 20 | 18.6 | -1.4 | 6.5E-05 | 33.4 | 20 | 15.1 | -4.9 | 3.5E-04 | 29.6 | 19.5 | 11.3 | -8.2 | 3.6E-03 | 27 | 19 | 8.7 | -10.3 | 6.9E-03 | 26 | 19 | 7.6 | -11.4 | 1.1E-02 | 25.2 | 19 | 6.9 | -12.1 | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 39 | 19 | 6.1E-05 | 36.2 | 19 | 17.9 | -1.1 | 6.4E-05 | 33.1 | 19 | 14.8 | -4.2 | 3.9E-04 | 29.5 | 18.5 | 11.2 | -7.3 | 3.9E-03 | 26.9 | 18 | 8.6 | -9.4 | 7.0E-03 | 26 | 18 | 7.6 | -10.4 | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 38 | 18 | 6.1E-05 | 35.4 | 18 | 17.1 | -0.9 | 6.6E-05 | 32.7 | 18 | 14.4 | -3.6 | 4.8E-04 | 29.3 | 17.5 | 11 | -6.5 | 4.1E-03 | 26.8 | 17 | 8.5 | -8.5 | 7.5E-03 | 25.9 | 17 | 7.5 | -9.5 | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 37 | 17 | 6.1E-05 | 34.7 | 17 | 16.4 | -0.6 | 6.9E-05 | 32.3 | 17 | 14 | -3 | 5.6E-04 | 29.1 | 16.5 | 10.8 | -5.7 | 4.5E-03 | 26.7 | 16 | 8.4 | -7.6 | 8.0E-03 | 25.8 | 16 | 7.4 | -8.6 | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 36 | 16 | 6.1E-05 | 33.9 | 16 | 15.6 | -0.4 | 7.6E-05 | 31.8 | 16 | 13.5 | -2.5 | 7.4E-04 | 28.9 | 15.5 | 10.6 | -4.9 | 4.9E-03 | 26.6 | 15 | 8.3 | -6.7 | 8.5E-03 | 25.7 | 15 | 7.3 | -7.7 | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 35 | 15 | 6.5E-05 | 33 | 15 | 14.7 | -0.3 | 9.3E-05 | 31.3 | 15 | 13 | -2 | 9.6E-04 | 28.6 | 14.5 | 10.3 | -4.2 | 5.5E-03 | 26.4 | 14 | 8.1 | -5.9 | 9.2E-03 | 25.5 | 14 | 7.1 | -6.9 | 1.3E-02 | 24.8 | 14 | 6.5 | -7.5 | 2.8E-02 | 22.9 | 13 | 4.6 | -8.4 |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 34 | 14 | 6.8E-05 | 32.2 | 14 | 13.9 | -0.1 | 1.3E-04 | 30.7 | 14 | 12.4 | -1.6 | 1.3E-03 | 28.3 | 13.5 | 10 | -3.5 | 6.3E-03 | 26.2 | 13 | 7.9 | -5.1 | 1.0E-02 | 25.4 | 13 | 7 | -6 | 1.4E-02 | 24.7 | 13 | 6.4 | -6.6 | 3.0E-02 | 22.8 | 12 | 4.5 | -7.5 |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 33 | 13 | 8.9E-05 | 31.3 | 13 | 13 | 0 | 2.2E-04 | 30.1 | 13 | 11.8 | -1.2 | 1.8E-03 | 27.9 | 12.5 | 9.6 | -2.9 | 7.3E-03 | 25.9 | 12 | 7.6 | -4.4 | 1.1E-02 | 25.2 | 12 | 6.8 | -5.2 | 1.5E-02 | 24.5 | 12 | 6.2 | -5.8 | 3.0E-02 | 22.7 | 11 | 4.4 | -6.6 |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 32 | 12 | 1.7E-04 | 30.4 | 12 | 12.1 | 0.1 | 4.5E-04 | 29.4 | 12 | 11.1 | -0.9 | 2.6E-03 | 27.4 | 11.5 | 9.1 | -2.4 | 8.7E-03 | 25.7 | 11 | 7.4 | -3.6 | 1.3E-02 | 24.9 | 11 | 6.5 | -4.5 | 1.7E-02 | 24.3 | 11 | 6 | -5 | 3.2E-02 | 22.5 | 10 | 4.2 | -5.8 |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 31 | 11 | 4.0E-04 | 29.5 | 11 | 11.2 | 0.2 | 9.3E-04 | 28.6 | 11 | 10.3 | -0.7 | 3.8E-03 | 27 | 10.5 | 8.7 | -1.8 | 1.0E-02 | 25.3 | 10 | 7 | -3 | 1.4E-02 | 24.6 | 10 | 6.2 | -3.8 | 2.0E-02 | 23.9 | 10 | 5.6 | -4.4 | 3.4E-02 | 22.3 | 9 | 4 | -5 |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 30 | 10 | 1.0E-03 | 28.5 | 10 | 10.2 | 0.2 | 2.0E-03 | 27.8 | 10 | 9.5 | -0.5 | 5.6E-03 | 26.4 | 9.5 | 8.1 | -1.4 | 1.3E-02 | 24.9 | 9 | 6.6 | -2.4 | 1.7E-02 | 24.3 | 9 | 5.9 | -3.1 | 2.2E-02 | 23.6 | 9 | 5.3 | -3.7 | 3.6E-02 | 22.2 | 8 | 3.9 | -4.1 |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 29.5 | 9.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 29 | 9 | 2.4E-03 | 27.6 | 9 | 9.3 | 0.3 | 3.7E-03 | 27 | 9 | 8.7 | -0.3 | 8.1E-03 | 25.8 | 8.5 | 7.5 | -1 | 1.6E-02 | 24.4 | 8 | 6.1 | -1.9 | 2.0E-02 | 23.9 | 8 | 5.5 | -2.5 | 2.6E-02 | 23.2 | 8 | 4.9 | -3.1 | 3.9E-02 | 21.8 | 7 | 3.5 | -3.5 |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 28.5 | 8.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 28 | 8 | 4.8E-03 | 26.6 | 8 | 8.3 | 0.3 | 6.5E-03 | 26.1 | 8 | 7.8 | -0.2 | 1.2E-02 | 25.1 | 7.5 | 6.8 | -0.7 | 2.0E-02 | 23.9 | 7 | 5.6 | -1.4 | 2.4E-02 | 23.4 | 7 | 5 | -2 | 2.9E-02 | 22.8 | 7 | 4.5 | -2.5 | 4.2E-02 | 21.5 | 6 | 3.2 | -2.8 |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 27.5 | 7.5 | 6.6E-03 | 26.1 | 7.5 | 7.8 | 0.3 | 8.6E-03 | 25.6 | 7.5 | 7.3 | -0.2 | 1.4E-02 | 24.7 | 7 | 6.4 | -0.6 | 2.2E-02 | 23.7 | 6.5 | 5.4 | -1.1 | 2.6E-02 | 23.1 | 6.5 | 4.7 | -1.8 | 3.2E-02 | 22.6 | 6.5 | 4.3 | -2.2 | 4.4E-02 | 21.3 | 5.5 | 3 | -2.5 |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 27 | 7 | 8.9E-03 | 25.6 | 7 | 7.3 | 0.3 | 1.1E-02 | 25.2 | 7 | 6.9 | -0.1 | 1.7E-02 | 24.3 | 6.5 | 6 | -0.5 | 2.5E-02 | 23.3 | 6 | 5 | -1 | 2.9E-02 | 22.9 | 6 | 4.5 | -1.5 | 3.4E-02 | 22.3 | 6 | 4 | -2 | 4.6E-02 | 21.1 | 5 | 2.8 | -2.2 |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 26.5 | 6.5 | 1.2E-02 | 25.1 | 6.5 | 6.8 | 0.3 | 1.4E-02 | 24.7 | 6.5 | 6.4 | -0.1 | 1.9E-02 | 24 | 6 | 5.7 | -0.3 | 2.8E-02 | 23 | 5.5 | 4.7 | -0.8 | 3.2E-02 | 22.6 | 5.5 | 4.2 | -1.3 | 3.7E-02 | 22.1 | 5.5 | 3.8 | -1.7 | 4.9E-02 | 20.8 | 4.5 | 2.5 | -2 |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 26 | 6 | 1.5E-02 | 24.6 | 6 | 6.3 | 0.3 | 1.7E-02 | 24.3 | 6 | 6 | 0 | 2.3E-02 | 23.6 | 5.5 | 5.3 | -0.2 | 3.1E-02 | 22.7 | 5 | 4.4 | -0.6 | 3.5E-02 | 22.3 | 5 | 3.9 | -1.1 | 3.9E-02 | 21.8 | 5 | 3.5 | -1.5 | 5.1E-02 | 20.6 | 4 | 2.3 | -1.7 |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 25.5 | 5.5 | 1.8E-02 | 24.1 | 5.5 | 5.8 | 0.3 | 2.1E-02 | 23.8 | 5.5 | 5.5 | 0 | 2.6E-02 | 23.1 | 5 | 4.8 | -0.2 | 3.4E-02 | 22.3 | 4.5 | 4 | -0.5 | 3.8E-02 | 21.9 | 4.5 | 3.5 | -1 | 4.3E-02 | 21.4 | 4.5 | 3.1 | -1.4 | 5.4E-02 | 20.3 | 3.5 | 2 | -1.5 |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 25 | 5 | 2.3E-02 | 23.6 | 5 | 5.3 | 0.3 | 2.5E-02 | 23.3 | 5 | 5 | 0 | 3.0E-02 | 22.7 | 4.5 | 4.4 | -0.1 | 3.8E-02 | 21.9 | 4 | 3.6 | -0.4 | 4.2E-02 | 21.6 | 4 | 3.2 | -0.8 | 4.6E-02 | 21.1 | 4 | 2.8 | -1.2 | 5.7E-02 | 20.1 | 3 | 1.8 | -1.2 |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 24.5 | 4.5 | 2.7E-02 | 23.1 | 4.5 | 4.8 | 0.3 | 2.9E-02 | 22.8 | 4.5 | 4.5 | 0 | 3.5E-02 | 22.2 | 4 | 3.9 | -0.1 | 4.2E-02 | 21.5 | 3.5 | 3.2 | -0.3 | 4.6E-02 | 21.1 | 3.5 | 2.7 | -0.8 | 5.0E-02 | 20.7 | 3.5 | 2.4 | -1.1 | 6.0E-02 | 19.8 | 2.5 | 1.5 | -1 |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 24 | 4 | 3.2E-02 | 22.5 | 4 | 4.2 | 0.2 | 3.4E-02 | 22.3 | 4 | 4 | 0 | 3.9E-02 | 21.8 | 3.5 | 3.5 | 0</ | | | | | | | | | | | | | | | | | | | | |

TABLE A3.3

Results with different input levels (SFN) * **(32k not extended, PP2, 1/16, 256 QAM, 2/3)**

(*) 1 Useful signal + 1 SFN auto-interference @600 µs.

TABLE A3.4
32k, PP2, 1/16, 256 QAM, 3/5

| | Ref MER | LDPC iter. and BER Tables | Lc | $f(BER)$ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|-----------------|---------|--|--|----------|---------|------|---------|------|---------|------|---------|------|---------|-------|---------|-------|-----------------|--------|-------|------|-------|------|-------|------|------|------|------|------|------|-------|--|------|------|------|------|-----|-----|-----|-----|------|------|------|------|-----|------|------|------|-----|-----|-----|------|-----|------|-----|------|-----|-----|-----|-----|-----|-----|---|-----|-----|------|-----|------|----------------------|-----|-----|-----|-----|---|-----|------|---|-----|-----|---|---|---|-----|-----|---|---|-----|-----|---|---|---|---|---|---|---|---|---|---|---|---|---------------------|
| MFN | 17.1 dB | | <p>Lc_{mfn} BER</p> <table border="1"> <tr><td>1e-2</td><td>2e-2</td><td>4e-2</td><td>6e-2</td></tr> <tr><td>0.3</td><td>0.1</td><td>0.2</td><td>0.5</td></tr> <tr><td>0.35</td><td>0.2</td><td>0.2</td><td>0.5</td></tr> <tr><td>0.4</td><td>0.2</td><td>0.2</td><td>0.52</td></tr> <tr><td>0.6</td><td>0.3</td><td>0.35</td><td>0.55</td></tr> <tr><td>1.2</td><td>0.7</td><td>0.5</td><td>0.6</td></tr> <tr><td>1.9</td><td>1</td><td>0.7</td><td>0.7</td></tr> <tr><td>2.6</td><td>1.4</td><td>0.85</td><td>0.8</td></tr> <tr><td>3.5</td><td>1.9</td><td>1.1</td><td>0.9</td></tr> <tr><td>4.3</td><td>2.5</td><td>1.4</td><td>1.1</td></tr> <tr><td>5.3</td><td>3.4</td><td>1.75</td><td>1.25</td></tr> <tr><td>6</td><td>4.6</td><td>2.2</td><td>1.45</td></tr> <tr><td>6</td><td>6</td><td>3</td><td>1.8</td></tr> <tr><td>6</td><td>6</td><td>4.3</td><td>2.2</td></tr> <tr><td>6</td><td>6</td><td>6</td><td>3</td></tr> <tr><td>6</td><td>6</td><td>6</td><td>5.5</td></tr> </table> | 1e-2 | 2e-2 | 4e-2 | 6e-2 | 0.3 | 0.1 | 0.2 | 0.5 | 0.35 | 0.2 | 0.2 | 0.5 | 0.4 | 0.2 | 0.2 | 0.52 | 0.6 | 0.3 | 0.35 | 0.55 | 1.2 | 0.7 | 0.5 | 0.6 | 1.9 | 1 | 0.7 | 0.7 | 2.6 | 1.4 | 0.85 | 0.8 | 3.5 | 1.9 | 1.1 | 0.9 | 4.3 | 2.5 | 1.4 | 1.1 | 5.3 | 3.4 | 1.75 | 1.25 | 6 | 4.6 | 2.2 | 1.45 | 6 | 6 | 3 | 1.8 | 6 | 6 | 4.3 | 2.2 | 6 | 6 | 6 | 3 | 6 | 6 | 6 | 5.5 | Not relevant for MFN | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1e-2 | 2e-2 | 4e-2 | 6e-2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.3 | 0.1 | 0.2 | 0.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.35 | 0.2 | 0.2 | 0.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.4 | 0.2 | 0.2 | 0.52 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.6 | 0.3 | 0.35 | 0.55 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.2 | 0.7 | 0.5 | 0.6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.9 | 1 | 0.7 | 0.7 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2.6 | 1.4 | 0.85 | 0.8 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3.5 | 1.9 | 1.1 | 0.9 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 4.3 | 2.5 | 1.4 | 1.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 5.3 | 3.4 | 1.75 | 1.25 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 6 | 4.6 | 2.2 | 1.45 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 6 | 6 | 3 | 1.8 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 6 | 6 | 4.3 | 2.2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 6 | 6 | 6 | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 6 | 6 | 6 | 5.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SFN | 17.1 dB | <table border="1"> <tr><td>BER before LDPC</td><td>margin</td></tr> <tr><td><= 8E-2</td><td>>= 1</td></tr> <tr><td><= 6E-2</td><td>>= 3</td></tr> <tr><td><= 4E-2</td><td>>= 4</td></tr> <tr><td><= 1E-2</td><td>>= 8</td></tr> <tr><td><= 1E-3</td><td>>= 12</td></tr> <tr><td><= 1E-4</td><td>>= 15</td></tr> </table> <table border="1"> <tr><td>LDPC iterations</td><td>margin</td></tr> <tr><td><= 20</td><td>>= 1</td></tr> <tr><td><= 15</td><td>>= 3</td></tr> <tr><td><= 10</td><td>>= 5</td></tr> <tr><td><= 6</td><td>>= 7</td></tr> <tr><td><= 5</td><td>>= 9</td></tr> <tr><td><= 4</td><td>>= 15</td></tr> </table> | BER before LDPC | margin | <= 8E-2 | >= 1 | <= 6E-2 | >= 3 | <= 4E-2 | >= 4 | <= 1E-2 | >= 8 | <= 1E-3 | >= 12 | <= 1E-4 | >= 15 | LDPC iterations | margin | <= 20 | >= 1 | <= 15 | >= 3 | <= 10 | >= 5 | <= 6 | >= 7 | <= 5 | >= 9 | <= 4 | >= 15 | <p>Lc_{sfn} BER</p> <table border="1"> <tr><td>1e-2</td><td>2e-2</td><td>4e-2</td><td>6e-2</td></tr> <tr><td>0.2</td><td>0.2</td><td>0.4</td><td>1.1</td></tr> <tr><td>0.25</td><td>0.25</td><td>0.42</td><td>1.12</td></tr> <tr><td>0.4</td><td>0.35</td><td>0.45</td><td>1.15</td></tr> <tr><td>0.6</td><td>0.5</td><td>0.5</td><td>1.2</td></tr> <tr><td>0.9</td><td>0.65</td><td>0.6</td><td>1.25</td></tr> <tr><td>1.2</td><td>0.8</td><td>0.8</td><td>1.3</td></tr> <tr><td>1.6</td><td>1.2</td><td>1</td><td>1.4</td></tr> <tr><td>2.2</td><td>1.65</td><td>1.2</td><td>1.55</td></tr> <tr><td>3</td><td>2.2</td><td>1.5</td><td>1.7</td></tr> <tr><td>4.5</td><td>3</td><td>1.8</td><td>1.85</td></tr> <tr><td>6</td><td>4.6</td><td>2.2</td><td>2</td></tr> <tr><td>6</td><td>6</td><td>2.9</td><td>2.2</td></tr> <tr><td>6</td><td>6</td><td>4.1</td><td>2.5</td></tr> <tr><td>6</td><td>6</td><td>6</td><td>3</td></tr> <tr><td>6</td><td>6</td><td>6</td><td>4</td></tr> <tr><td>6</td><td>6</td><td>6</td><td>6</td></tr> </table> | 1e-2 | 2e-2 | 4e-2 | 6e-2 | 0.2 | 0.2 | 0.4 | 1.1 | 0.25 | 0.25 | 0.42 | 1.12 | 0.4 | 0.35 | 0.45 | 1.15 | 0.6 | 0.5 | 0.5 | 1.2 | 0.9 | 0.65 | 0.6 | 1.25 | 1.2 | 0.8 | 0.8 | 1.3 | 1.6 | 1.2 | 1 | 1.4 | 2.2 | 1.65 | 1.2 | 1.55 | 3 | 2.2 | 1.5 | 1.7 | 4.5 | 3 | 1.8 | 1.85 | 6 | 4.6 | 2.2 | 2 | 6 | 6 | 2.9 | 2.2 | 6 | 6 | 4.1 | 2.5 | 6 | 6 | 6 | 3 | 6 | 6 | 6 | 4 | 6 | 6 | 6 | 6 | For level > -60 dBm |
| BER before LDPC | margin | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 8E-2 | >= 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 6E-2 | >= 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 4E-2 | >= 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 1E-2 | >= 8 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 1E-3 | >= 12 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 1E-4 | >= 15 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| LDPC iterations | margin | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 20 | >= 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 15 | >= 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 10 | >= 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 6 | >= 7 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 5 | >= 9 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 4 | >= 15 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1e-2 | 2e-2 | 4e-2 | 6e-2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.2 | 0.2 | 0.4 | 1.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.25 | 0.25 | 0.42 | 1.12 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.4 | 0.35 | 0.45 | 1.15 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.6 | 0.5 | 0.5 | 1.2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.9 | 0.65 | 0.6 | 1.25 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.2 | 0.8 | 0.8 | 1.3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.6 | 1.2 | 1 | 1.4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2.2 | 1.65 | 1.2 | 1.55 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3 | 2.2 | 1.5 | 1.7 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 4.5 | 3 | 1.8 | 1.85 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 6 | 4.6 | 2.2 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 6 | 6 | 2.9 | 2.2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 6 | 6 | 4.1 | 2.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 6 | 6 | 6 | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 6 | 6 | 6 | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 6 | 6 | 6 | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

TABLE A3.5

Results* (AWGN interference limited) with different input levels (MFN)
(32k not extended, PP2, 1/16 256 QAM, 3/5)

| MFN | | ref. MER (dB) | | | | | | | | | | | | 17.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|------------------|----------------|---------------|-----------------|--------------|-------------|------------------------|------------------|-----------------|--------------|-------------|------------------------|------------------|-----------------|--------------|-------------|------------------------|------------------|-----------------|--------------|-------------|------------------------|------------------|-----------------|--------------|----------------|------------------------|------------------|-----------------|----------------|-------------|------------------------|------------------|-----------------|--------------|-------------|------------------------|------------------|-----------------|--------------|-------------|------------------------|------------------|----------|-----|----|----|--|----|--|--|----|
| | | -50 dBm | | | | | | -60 | | | | | | -63 | | | | | | -65 | | | | | | -68 | | | | | | -70 | | | | | | -72 | | | | | | -74 | | | | | | | |
| level (dBm) | C/N (dB) | margin (dB) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER - ref MER (dB) | delta (x-margin) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER - ref MER (dB) | delta (x-margin) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER - ref MER (dB) | delta (x-margin) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER - ref MER (dB) | delta (x-margin) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER - ref MER (dB) | delta (x-margin) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER - ref MER (dB) | delta (x-margin) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER - ref MER (dB) | delta (x-margin) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER - ref MER (dB) | delta (x-margin) | C/N (dB) | | | | | | | | |
| Noise off | 5.1E-05 | 41.3 | | | | | | 5.4E-05 | 34.8 | | | | 6.7E-05 | 32.1 | | | 9.8E-04 | 28.7 | | | 2.9E-03 | 27.4 | | | 1.0E-02 | 25.4 | | | 2.5E-02 | 23.3 | | | 4.7E-02 | 21.0 | | | Noise off | | | | | | | | | | | | | | |
| 40 | 21.0 | 5.3E-05 | 36.5 | 21.0 | 19.4 | -1.6 | | 5.7E-05 | 33.2 | 20.7 | 16.1 | -4.6 | 9.8E-05 | 31.2 | 20.5 | 14.1 | -6.4 | 1.5E-03 | 28.2 | 20.5 | 11.1 | -9.4 | 3.8E-03 | 27.1 | 20.5 | 10.0 | -10.5 | 1.2E-02 | 25.2 | 20.0 | 8.1 | -11.9 | 2.5E-02 | 23.2 | 19.5 | 6.1 | -13.4 | 4.8E-02 | 20.8 | 18.5 | 3.7 | -14.8 | 40 | | | | | | | | |
| | 20.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 39.5 | | | | | | | | | |
| 39 | 20.0 | 5.3E-05 | 35.8 | 20.0 | 18.7 | -1.3 | | | | | | | | 1.1E-04 | 30.9 | 19.5 | 13.8 | -5.7 | 1.7E-03 | 28.1 | 19.5 | 11.0 | -8.5 | 3.9E-03 | 27.0 | 19.5 | 9.9 | -9.6 | | | | | | | | | | | | | | | | | | | | 39 | | | |
| | 19.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 38.5 | | | | | | | | | |
| 38 | 19.0 | 5.3E-05 | 35.0 | 19.0 | 17.9 | -1.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 38 | | | | | | | | | | | |
| | 18.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 37.5 | | | | | | | | | |
| 37 | 18.0 | 5.5E-05 | 34.2 | 18.0 | 17.1 | -0.9 | | | | | | | | 1.8E-04 | 30.4 | 17.5 | 13.3 | -4.2 | 2.3E-03 | 27.8 | 17.5 | 10.7 | -6.8 | | | | | | | | | | | | | | | | | | | | | 37 | | | | | | | |
| | 17.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 36.5 | | | | | | | | | |
| 36 | 17.0 | 5.6E-05 | 33.4 | 17.0 | 16.3 | -0.7 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 36 | | | | | | | | | | | | |
| | 16.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 35.5 | | | | | | | | | | |
| 35 | 16.0 | 5.9E-05 | 32.6 | 16.0 | 15.5 | -0.5 | 1.1E-04 | 31.0 | 15.7 | 13.9 | -1.8 | 3.7E-04 | 29.6 | 15.5 | 12.5 | -3.0 | 3.0E-03 | 27.3 | 15.5 | 10.2 | -5.3 | 5.8E-03 | 26.4 | 15.5 | 9.3 | -6.2 | 1.5E-02 | 24.6 | 15.0 | 7.5 | -7.5 | | | | | | | | | | | | 35 | | | | | | | | |
| | 15.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 34.5 | | | | | | | | | | |
| 34 | 15.0 | 7.2E-05 | 31.7 | 15.0 | 14.6 | -0.4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 34 | | | | | | | | | | | | | |
| | 14.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 33.5 | | | | | | | | | | |
| 33 | 14.0 | 1.2E-04 | 30.8 | 14.0 | 13.7 | -0.3 | | | | | | | | 9.5E-04 | 28.7 | 13.5 | 11.6 | -1.9 | 4.6E-03 | 26.8 | 13.5 | 9.7 | -3.8 | 7.8E-03 | 25.9 | 13.5 | 8.8 | -4.7 | | | | | | | | | | | | | | | | | 33 | | | | | | |
| | 13.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 32.5 | | | | | | | | | | |
| 32 | 13.0 | 2.7E-04 | 29.9 | 13.0 | 12.8 | -0.2 | | | | | | | | 1.6E-03 | 28.2 | 12.5 | 11.1 | -1.4 | 5.8E-03 | 26.4 | 12.5 | 9.3 | -3.2 | 9.3E-03 | 25.6 | 12.5 | 8.5 | -4.0 | 1.9E-02 | 24.0 | 12.0 | 6.9 | -5.1 | | | | | | | | | | | | 32 | | | | | | |
| | 12.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 31.5 | | | | | | | | | | |
| 31 | 12.0 | 6.9E-04 | 29.0 | 12.0 | 11.9 | -0.1 | | | | | | | | 2.7E-03 | 27.5 | 11.5 | 10.4 | -1.1 | 7.7E-03 | 26.0 | 11.5 | 8.9 | -2.6 | 1.1E-02 | 25.2 | 11.5 | 8.1 | -3.4 | 2.1E-02 | 23.8 | 11.0 | 6.7 | -4.3 | | | | | | | | | | | 31 | | | | | | | |
| | 11.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 30.5 | | | | | | | | | | |
| 30 | 11.0 | 1.6E-03 | 28.1 | 11.0 | 11.0 | 0.0 | 2.8E-03 | 27.5 | 10.7 | 10.4 | -0.3 | 4.4E-03 | 26.8 | 10.5 | 9.7 | -0.8 | 1.0E-02 | 25.5 | 10.5 | 8.4 | -2.1 | 1.4E-02 | 24.8 | 10.5 | 7.7 | -2.8 | 2.4E-02 | 23.5 | 10.0 | 6.4 | -3.6 | 3.7E-02 | 22.0 | 9.5 | 4.9 | -4.6 | 5.7E-02 | 19.9 | 8.5 | 2.8 | -5.7 | 30 | | | | | | | | | |
| | 29.5 | 10.5 | 2.4E-03 | 27.6 | 10.5 | 10.5 | 0.0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 29.5 | | | | | | | | | | | | |
| 29 | 10.0 | 3.0E-03 | 27.2 | 10.0 | 10.1 | 0.1 | 5.1E-03 | 26.6 | 9.7 | 9.5 | -0.2 | 7.1E-03 | 26.1 | 9.5 | 9.0 | -0.5 | 1.3E-02 | 24.9 | 9.5 | 7.8 | -1.7 | 1.7E-02 | 24.3 | 9.5 | 7.2 | -2.3 | 2.8E-02 | 23.1 | 9.0 | 6.0 | -3.0 | 4.1E-02 | 21.6 | 8.5 | 4.5 | -4.0 | | | | | | | | | | 29 | | | | | |
| | 28.5 | 9.5 | 4.9E-03 | 26.7 | 9.5 | 9.6 | 0.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 28.5 | | | | | | | | | | | | |
| 28 | 9.0 | 6.7E-03 | 26.2 | 9.0 | 9.1 | 0.1 | 8.7E-03 | 25.7 | 8.7 | 8.6 | -0.1 | 1.1E-02 | 25.3 | 8.5 | 8.2 | -0.3 | 1.8E-02 | 24.3 | 8.5 | 7.2 | -1.3 | 2.2E-02 | 23.8 | 8.5 | 6.7 | -1.8 | 3.1E-02 | 22.6 | 8.0 | 5.5 | -2.5 | 4.4E-02 | 21.2 | 7.5 | 4.1 | -3.4 | | | | | | | | | | 28 | | | | | |
| | 27.5 | 8.5 | 8.9E-03 | 25.7 | 8.5 | 8.6 | 0.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 27.5 | | | | | | | | | | | | | |
| 27 | 8.0 | 1.2E-02 | 25.2 | 8.0 | 8.1 | 0.1 | 1.4E-02 | 24.8 | 7.7 | 7.7 | 0.0 | 1.6E-02 | 24.5 | 7.5 | 7.4 | -0.1 | 2.3E-02 | 23.6 | 7.5 | 6.5 | -1.0 | 2.7E-02 | 23.1 | 7.5 | 6.0 | -1.5 | 3.7E-02 | 22.0 | 7.0 | 4.9 | -2.1 | 4.9E-02 | 20.8 | 6.5 | 3.7 | -2.8 | | | | | | | | | | 27 | | | | | |
| | 26.5 | 7.5 | 1.5E-02 | 24.7 | 7.5 | 7.6 | 0.1 | 1.7E-02 | 24.4 | 7.2 | 7.3 | 0.1 | | | | | | | | | | | | | | | | | | | | | | | | | | 26.5 | | | | | | | | | | | | | |
| 26 | 7.0 | 1.8E-02 | 24.7 | 7.0 | 7.1 | 0.1 | 2.1E-02 | 23.9 | 6.7 | 6.8 | 0.1 | 2.3E-02 | 23.6 | 6.5 | 6.5 | 0.0 | 3.0E-02 | 22.8 | 6.5 | 5.7 | -0.8 | 3.4E-02 | 22.4 | 6.5 | 5.3 | -1.2 | 4.3E-02 | 21.4 | 6.0 | 4.3 | -1.7 | 5.4E-02 | 20.2 | 5.5 | 3.1 | -2.4 | | | | | | | | | | 26 | | | | | |
| | 25.5 | 6.5 | 2.2E-02 | 23.7 | 6.5 | 6.6 | 0.1 | 2.5E-02 | 23.4 | 6.2 | 6.3 | 0.1 | | | | | | | | | | | | | | | | | | | | | | | | | | 25.5 | | | | | | | | | | | | | |
| 25 | 6.0 | 2.7E-02 | 23.1 | 6.0 | 6.0 | 0.0 | 2.9E-02 | 22.9 | 5.7 | 5.8 | 0.1 | 3.2E-02 | 22.6 | 5.5 | 5.5 | 0.0 | 3.8E-02 | 21.9 | 5.5 | 4.8 | -0.7 | 4.1E-02 | 21.6 | 5.5 | 4.5 | -1.0 | 5.0E-02 | 20.7 | 5.0 | 3.6 | -1.4 | 6.0E-02 | 19.6 | 4.5 | 2.5 | -2.0 | 7.5E-02 | 18.5 | 3.5 | 1.4 | -2.1 | | | | | | | | | | 25 |
| | 24.5 | 5.5 | 3.2E-02 | 22.6 | 5.5 | 5.5 | 0.0 | 3.4E-02 | 22.3 | 5.2 | 5.2 | 0.0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 24.5 | | | | | | | | | | |
| 24 | 5.0 | 3.7E-02 | 22.0 | 5.0 | 4.3 | -0.1 | 3.9E-02 | 21.8 | 4.7 | 4.7 | 0.0 | 4.1E-02 | 21.5 | 4.5 | 4.4 | -0.1 | 4.7E-02 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

TABLE A3.6

**Results with different input levels (SFN)*
(32k not extended, PP2, 1/16 256 QAM, 3/5)**

| SFN | ref. MER (dB) | 17.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|----------------|-------------------|-----------------|--------------|-------------|------------------------|-----------------|--------------|-------------|------------------------|-----------------|--------------|-------------|------------------------|-----------------|--------------|-------------|------------------------|-----------------|--------------|-------------|------------------------|-----------------|--------------|-------------|------------------------|-----------------|--------------|-------------|------------------------|-----------------|--------------|-------------|------------------------|----------------|---------|-------|---------|------|------|-------|------|------|--|--|----|--|--|----|--|--|--|----|--|----|--|--|----|
| level (dBm) | -50 | | | | -60 | | | | -63 | | | | -65 | | | | -68 | | | | -70 | | | | -72 | | | | -75 | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| C/I (dB) | margin (MFn) (dB) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER - ref MER (dB) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER - ref MER (dB) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER - ref MER (dB) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER - ref MER (dB) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER - ref MER (dB) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER - ref MER (dB) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER - ref MER (dB) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER - ref MER (dB) | | | | | | | | | | | | | | | | | | | | | | | | |
| <i>Int.off</i> | 5.0E-05 | 41.2 | | 5.4E-05 | 34.8 | | 6.7E-05 | 32.1 | | 2.0E-04 | 20.3 | | 2.8E-03 | 27.4 | | 1.0E-02 | 25.4 | | 2.4E-02 | 23.4 | | 2.4E-02 | 23.4 | | 2.4E-02 | 19.9 | | 2.4E-02 | 19.9 | | 2.4E-02 | 19.9 | | <i>Int.off</i> | | | | | | | | | | | | | | | | | | | | | | | |
| 40 | 21.0 | 5.2E-05 | 35.6 | 19.7 | 18.5 | -1.2 | 5.8E-05 | 32.7 | 19.7 | 15.6 | -4.1 | 1.3E-04 | 30.9 | 19.7 | 13.8 | -5.9 | 4.9E-04 | 29.4 | 19.5 | 12.3 | -7.2 | 4.0E-03 | 27.0 | 19.5 | 9.9 | -9.6 | 1.2E-02 | 25.2 | 19.0 | 8.1 | -10.9 | 2.6E-02 | 23.3 | 18.5 | 6.2 | -12.3 | 6.0E-02 | 19.6 | 16.5 | -14.0 | 40 | | | | | | | | | | | | | | | | |
| 39 | 20.0 | | | | | | 6.0E-05 | 32.3 | 18.7 | 15.2 | -3.5 | 1.5E-04 | 30.6 | 18.7 | 13.5 | -5.2 | 5.8E-04 | 29.3 | 18.5 | 12.2 | -6.3 | 4.4E-03 | 26.9 | 18.5 | 9.8 | -8.7 | | | | | | | | | | | | | | | | | | | 39 | | | | | | | | | | | | |
| 38 | 19.0 | | | | | | 6.4E-05 | 31.8 | 17.7 | 14.7 | -3.0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 38 | | | | | | | | | |
| 37 | 18.0 | | | | | | 7.9E-05 | 31.3 | 16.7 | 14.2 | -2.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 37 | | | | | | | | | |
| 36 | 17.0 | | | | | | 1.1E-04 | 30.8 | 15.7 | 13.7 | -2.0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 36 | | | | | | | | | |
| 35 | 16.0 | 5.7E-05 | 31.5 | 14.7 | 14.4 | -0.3 | 1.8E-04 | 30.1 | 14.7 | 13.0 | -1.7 | 6.6E-04 | 29.1 | 14.7 | 12.0 | -2.7 | 1.8E-03 | 28.1 | 14.5 | 11.0 | -3.5 | 6.9E-03 | 26.2 | 14.5 | 9.1 | -5.4 | 1.6E-02 | 24.6 | 14.0 | 7.5 | -6.5 | 2.9E-02 | 22.8 | 13.5 | 5.7 | -7.8 | 6.2E-02 | 19.4 | 11.5 | 2.3 | -9.2 | 35 | | | | | | | | | | | | | | | |
| 34 | 15.0 | | | | | | 8.1E-04 | 29.5 | 13.7 | 12.4 | -1.3 | 1.1E-03 | 28.6 | 13.7 | 11.5 | -2.2 | 2.4E-03 | 27.7 | 13.5 | 10.6 | -2.9 | 8.2E-03 | 25.9 | 13.5 | 8.8 | -4.7 | | | | | | | | | | | | | | | | | | | | | | | | | | | | 34 | | | |
| 33 | 14.0 | | | | | | 7.2E-04 | 28.8 | 12.7 | 11.7 | -1.0 | 1.8E-03 | 28.0 | 12.7 | 10.9 | -1.8 | | | | | 9.7E-03 | 25.5 | 12.5 | 8.4 | -4.1 | 1.9E-02 | 24.1 | 12.0 | 7.0 | -5.0 | 3.2E-02 | 22.5 | 11.5 | 5.4 | -6.1 | | | | | | | | | | | | | | | | | | | | | | 33 |
| 32 | 13.0 | | | | | | 1.1E-03 | 28.4 | 12.2 | 11.3 | -0.9 | | | | | 1.5E-03 | 28.0 | 11.7 | 10.9 | -0.8 | 3.0E-03 | 27.3 | 11.7 | 10.2 | -1.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | 32 | | | | | |
| 31 | 12.0 | | | | | | 3.0E-03 | 27.2 | 10.7 | 10.1 | -0.6 | 4.9E-03 | 26.6 | 10.7 | 9.5 | -1.2 | | | | | 1.5E-02 | 24.7 | 10.5 | 7.6 | -2.9 | 2.4E-02 | 23.4 | 10.0 | 6.3 | -3.7 | 3.7E-02 | 21.9 | 9.5 | 4.8 | -4.7 | | | | | | | | | | | | | | | | | | | | | | 31 |
| 30 | 11.0 | 3.6E-03 | 26.8 | 9.7 | 9.7 | 0.0 | 5.6E-03 | 26.3 | 9.7 | 9.2 | -0.5 | 7.8E-03 | 25.8 | 9.7 | 8.7 | -1 | 1.0E-02 | 25.3 | 9.5 | 8.2 | -1.3 | 1.8E-02 | 24.2 | 9.5 | 7.1 | -2.4 | 2.7E-02 | 23.0 | 9.0 | 5.9 | -3.1 | 4.0E-02 | 21.5 | 8.5 | 4.4 | -4.1 | 7.0E-02 | 18.6 | 6.5 | 1.5 | -5.0 | 30 | | | | | | | | | | | | | | | |
| 29.5 | 10.0 | 5.3E-03 | 26.3 | 9.2 | 9.2 | 0.0 | 7.4E-03 | 25.8 | 9.2 | 8.7 | -0.5 | | | | | 2.0E-02 | 23.9 | 9.0 | 6.8 | -2.2 | 3.0E-02 | 22.7 | 8.5 | 5.6 | -2.9 | 4.2E-02 | 21.3 | 8 | 4.2 | -3.8 | 7.2E-02 | 18.5 | 6.0 | 1.4 | -4.6 | 29.5 | | | | | | | | | | | | | | | | | | | | | |
| 29 | 9.5 | 7.4E-03 | 25.8 | 8.7 | 8.7 | 0.0 | 9.6E-03 | 25.4 | 8.7 | 8.3 | -0.4 | 1.2E-02 | 25.0 | 8.7 | 7.9 | -0.8 | | | | 2.3E-02 | 23.6 | 8.5 | 6.5 | -2 | 3.2E-02 | 22.4 | 8.0 | 5.3 | -2.7 | 4.4E-02 | 21.1 | 7.5 | 4.0 | -3.5 | 7.3E-02 | 18.4 | 5.5 | 1.3 | -4.2 | 29 | | | | | | | | | | | | | | | | | |
| 28.5 | 9.0 | 1.0E-02 | 25.3 | 8.2 | 8.2 | 0.0 | 1.2E-02 | 24.9 | 8.2 | 7.8 | -0.4 | | | | | | | | | 3.4E-02 | 22.1 | 7.5 | 5 | -2.5 | 4.6E-02 | 20.8 | 7.0 | 3.7 | -3.3 | 7.4E-02 | 18.3 | 5.0 | 1.2 | -3.8 | 28.5 | | | | | | | | | | | | | | | | | | | | | | |
| 28 | 8.5 | 1.3E-02 | 24.7 | 7.7 | 7.6 | -0.1 | 1.5E-02 | 24.4 | 7.7 | 7.3 | -0.4 | 1.8E-02 | 24.1 | 7.7 | 7 | -0.7 | 2.1E-02 | 23.8 | 7.5 | 6.7 | -0.8 | 2.8E-02 | 22.8 | 7.5 | 5.7 | -1.8 | 3.7E-02 | 21.8 | 7.0 | 4.7 | -2.3 | 4.8E-02 | 20.4 | 6.5 | 3.3 | -3.2 | 7.6E-02 | 18.2 | 4.5 | 1.1 | -3.4 | 28 | | | | | | | | | | | | | | | |
| 27.5 | 8.0 | 1.7E-02 | 24.2 | 7.2 | 7.1 | -0.1 | 1.9E-02 | 23.9 | 7.2 | 6.8 | -0.4 | | | | | 3.1E-02 | 22.4 | 7.0 | 5.3 | -1.7 | 4.0E-02 | 21.4 | 6.5 | 4.3 | -2.2 | 5.1E-02 | 20.1 | 6 | 3.0 | -3.0 | 7.8E-02 | 18.0 | 4.0 | 0.9 | -3.1 | 27.5 | | | | | | | | | | | | | | | | | | | | | |
| 27 | 7.5 | 2.1E-02 | 23.7 | 6.7 | 6.6 | -0.1 | 2.3E-02 | 23.4 | 6.7 | 6.3 | -0.4 | 2.5E-02 | 23.1 | 6.7 | 6 | -0.7 | 2.8E-02 | 22.8 | 6.5 | 5.7 | -0.8 | 3.5E-02 | 22.0 | 6.5 | 4.9 | -1.6 | 4.3E-02 | 21.0 | 6.0 | 3.9 | -2.1 | 5.3E-02 | 19.8 | 5.5 | 2.7 | -2.8 | 8.0E-02 | 17.9 | 3.5 | 0.8 | -2.7 | 27 | | | | | | | | | | | | | | | |
| 26.5 | 7.0 | 2.5E-02 | 23.1 | 6.2 | 6.0 | -0.2 | 2.7E-02 | 22.9 | 6.2 | 5.8 | -0.4 | | | | | 3.8E-02 | 21.5 | 6.0 | 4.4 | -1.6 | 4.7E-02 | 20.5 | 5.5 | 3.4 | -2.1 | 5.6E-02 | 19.4 | 5.0 | 2.3 | -2.7 | 8.2E-02 | 17.8 | 3.0 | 0.7 | -2.3 | 26.5 | | | | | | | | | | | | | | | | | | | | | |
| 26 | 6.5 | 3.0E-02 | 22.6 | 5.7 | 5.5 | -0.2 | 3.2E-02 | 22.3 | 5.7 | 5.2 | -0.5 | 3.4E-02 | 22.1 | 5.7 | 5 | -0.7 | 3.6E-02 | 21.8 | 5.5 | 4.7 | -0.8 | 4.3E-02 | 21.0 | 5.5 | 3.9 | -1.6 | 5.0E-02 | 20.1 | 5.0 | 3.0 | -2.0 | 5.9E-02 | 19.1 | 4.5 | 2.0 | -2.5 | 8.4E-02 | 17.6 | 2.5 | 0.5 | -2.0 | 26 | | | | | | | | | | | | | | | |
| 25.5 | 6.0 | 3.5E-02 | 21.9 | 5.2 | 4.8 | -0.4 | 3.7E-02 | 21.7 | 5.2 | 4.6 | -0.6 | 4.2E-02 | 21.0 | 4.7 | 3.9 | -0.8 | 4.4E-02 | 20.8 | 4.7 | 3.7 | -1 | 4.6E-02 | 20.5 | 4.5 | 3.4 | -1.1 | 5.1E-02 | 19.5 | 4.5 | 2.4 | -2.1 | 6.3E-02 | 18.7 | 4.0 | 1.6 | -2.4 | 8.6E-02 | 17.5 | 2.0 | 0.4 | -1.6 | 25.5 | | | | | | | | | | | | | | | |
| 25 | 5.5 | 4.0E-02 | 21.2 | 4.7 | 4.1 | -0.6 | 4.2E-02 | 21.0 | 4.7 | 3.9 | -0.8 | 4.4E-02 | 20.8 | 4.7 | 3.7 | -1 | 4.6E-02 | 20.5 | 4.5 | 3.4 | -1.1 | 5.1E-02 | 19.1 | 4.0 | 2.0 | -2.0 | 6.7E-02 | 18.5 | 3.5 | 1.4 | -2.1 | 8.9E-02 | 17.3 | 1.5 | 0.2 | -1.3 | 25 | | | | | | | | | | | | | | | | | | | | |
| 24.5 | 5.0 | 4.6E-02 | 20.5 | 4.2 | 3.4 | -0.8 | 4.7E-02 | 20.3 | 4.2 | 3.2 | -1.0 | | | | | 6.3E-02 | 22.4 | 18.7 | 3.5 | 1.6 | -1.9 | 7.1E-02 | 18.2 | 3.0 | 1.1 | -1.9 | 9.2E-02 | 17.1 | 1.0 | 0.0 | -1.0 | 24.5 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 24 | 4.5 | 5.1E-02 | 19.8 | 3.7 | 2.7 | -1.0 | 5.3E-02 | 19.6 | 3.7 | 2.5 | -1.2 | 5.4E-02 | 19.4 | 3.7 | 2.3 | -1.4 | 5.6E-02 | 19.3 | 3.5 | 2.2 | -1.3 | 6.1E-02 | 18.8 | 3.0 | 1.2 | -1.8 | 7.5E-02 | 17.9 | 2.5 | 0.8 | -1.7 | 9.5E-02 | 16.9 | 0.5 | -0.2 | -0.7 | 24 | | | | | | | | | | | | | | | | | | | | |
| 23.5 | 4.0 | 5.7E-02 | 19.1 | 3.2 | 2.0 | -1.2 | 5.9E-02 | 19.0 | 3.2 | 1.9 | -1.3 | | | | | 7.2E-02 | 21.0 | 2.5 | 0.9 | -1.6 | 7.9E-02 | 17.6 | 2.0 | 0.5 | -1.6 | 9.8E-02 | 16.7 | 0.0 | -0.4 | -0.4 | 23.5 | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 23 | 3.5 | 6.3E-02 | 18.6 | 2.7 | 1.5 | -1.2 | 6.5E-02 | 18.5 | 2.7 | 1.4 | -1.3 | 6.6E-02 | 18.4 | 2.7 | 1.3 | -1.4 | 6.8E-02 | 18.3 | 2.5 | 1.2 | -1.3 | 7.2E-02 | 18.0 | 2.5 | 0.9 | -1.6 | 7.7E-02 | 17.7 | 2.0 | 0.6 | -1.4 | 8.4E-02 | 17.4 | 1.5 | 0.3 | -1.2 | 1.0E-01 | 16.4 | 0.5 | -0.7 | -0.2 | 23 | | | | | | | | | | | | | | | |
| 22.5 | 3.0 | 6.9E-02 | 18.1 | 2.2 | 1.0 | -1.2 | 7.1E-02 | 18.1 | 2.2 | 1.0 | -1.2 | | | | | 7.7E-02 | 17.7 | 2.0 | 0.6 | -1.4 | 8.2E-02 | 17.4 | 1.5 | 0.3 | -1.2 | 8.9E-02 | 17.1 | 1.0 | 0.0 | -1.0 | 1.1E-01 | 16.1 | -1.0 | -1.0 | 0.0 | 22.5 | | | | | | | | | | | | | | | | | | | | | |
| 22 | 2.5 | 7.6E-02 | 17.7 | 1.7 | 0.6 | -1.1 | 7.7E-02 | 17.7 | 1.7 | 0.6 | -1.1 | 7.8E-02 | 17.6 | 1.7 | 0.5 | -1.2 | 7.9E-02 | 17.5 | 1.5 | 0.4 | -1.1 | 8.3E-02 | 17.3 | 1.5 | 0.2 | -1.3 | 8.8E-02 | 17.0 | 1.0 | -0.1 | -1.1 | 9.4E-02 | 16.7 | 0.5 | -0.4 | -0.9 | </td | | | | | | | | | | | | | | | | | | | | |

TABLE A3.7
16k extended, PP2, 19/128, 64 QAM, 1/2

| | Ref MER | LDPC iter. and BER Tables | Lc | $f(BER)$ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|------------|---------|--|--|----------|------------|------|------------|------|------------|-------|---------|-------|---------|-------|---------|-------|------|--------|-------|------|-------|------|-------|-------|-------|-------|-------|-------|------|-------|---|------|------|------|------|------|--------|-----|-----|-----|-----|-----|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|------|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|------|-----|-----|-----|-----|-----|---|-----|-----|-----|-----|-----|-----|---|-----|-----|-----|------|-----|-----|-----|-----|-----|-----|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|---|-----|-----|-----|-----|-----|-----|---|---|-----|-----|-----|-----|-----|---|---|-----|-----|-----|-----|-----|---|---|---|-----|---|-----|-----|---|---|---|-----|-----|-----|-----|---|---|---|---|---|---|-----|---|---|---|---|---|---|-----|---|---|---|---|---|---|---|
| MFN | 11.0 dB | | <p>Lc_{mfn}</p> <table border="1"> <caption>BER</caption> <thead> <tr> <th>1e-2</th><th>2e-2</th><th>4e-2</th><th>6e-2</th><th>8e-2</th><th>1.1e-1</th></tr> </thead> <tbody> <tr><td>-40</td><td>-0.2</td><td>-0.1</td><td>0.1</td><td>0.4</td><td>1.2</td></tr> <tr><td>-50</td><td>-0.2</td><td>-0.1</td><td>0.1</td><td>0.4</td><td>1.2</td></tr> <tr><td>-60</td><td>-0.2</td><td>-0.1</td><td>0.1</td><td>0.4</td><td>1.2</td></tr> <tr><td>-65</td><td>0</td><td>0.1</td><td>0.15</td><td>0.45</td><td>1.25</td></tr> <tr><td>-70</td><td>0.2</td><td>0.2</td><td>0.55</td><td>1.4</td><td>3.2</td></tr> <tr><td>-72</td><td>0.6</td><td>0.4</td><td>0.65</td><td>1.5</td><td>3.3</td></tr> <tr><td>-75</td><td>1.3</td><td>0.8</td><td>0.6</td><td>1.6</td><td>3.5</td></tr> <tr><td>-77</td><td>1.9</td><td>1.2</td><td>0.8</td><td>1</td><td>3.7</td></tr> <tr><td>-78</td><td>2.5</td><td>1.6</td><td>1.1</td><td>1.3</td><td>3.8</td></tr> <tr><td>-79</td><td>3.5</td><td>2.5</td><td>1.4</td><td>1.7</td><td>3.9</td></tr> <tr><td>-80</td><td>4.6</td><td>3.4</td><td>1.9</td><td>2.1</td><td>3.95</td></tr> <tr><td>-81</td><td>5.5</td><td>4.3</td><td>2.5</td><td>2.55</td><td>4</td></tr> <tr><td>-82</td><td>6</td><td>4.9</td><td>3.1</td><td>3</td><td>4</td></tr> <tr><td>-83</td><td>6</td><td>5.3</td><td>3.8</td><td>3.6</td><td>4</td></tr> <tr><td>-84</td><td>6</td><td>5.6</td><td>4.5</td><td>4.3</td><td>4</td></tr> <tr><td>-85</td><td>6</td><td>5.8</td><td>5.2</td><td>5</td><td>4.3</td></tr> <tr><td>-86</td><td>6</td><td>6</td><td>6</td><td>5.8</td><td>4.9</td></tr> <tr><td>-87</td><td>6</td><td>6</td><td>6</td><td>6</td><td>5.6</td></tr> <tr><td>-88</td><td>6</td><td>6</td><td>6</td><td>6</td><td>4</td></tr> </tbody> </table> <p>dB Additional margin (function of the level and BER) MFN</p> | 1e-2 | 2e-2 | 4e-2 | 6e-2 | 8e-2 | 1.1e-1 | -40 | -0.2 | -0.1 | 0.1 | 0.4 | 1.2 | -50 | -0.2 | -0.1 | 0.1 | 0.4 | 1.2 | -60 | -0.2 | -0.1 | 0.1 | 0.4 | 1.2 | -65 | 0 | 0.1 | 0.15 | 0.45 | 1.25 | -70 | 0.2 | 0.2 | 0.55 | 1.4 | 3.2 | -72 | 0.6 | 0.4 | 0.65 | 1.5 | 3.3 | -75 | 1.3 | 0.8 | 0.6 | 1.6 | 3.5 | -77 | 1.9 | 1.2 | 0.8 | 1 | 3.7 | -78 | 2.5 | 1.6 | 1.1 | 1.3 | 3.8 | -79 | 3.5 | 2.5 | 1.4 | 1.7 | 3.9 | -80 | 4.6 | 3.4 | 1.9 | 2.1 | 3.95 | -81 | 5.5 | 4.3 | 2.5 | 2.55 | 4 | -82 | 6 | 4.9 | 3.1 | 3 | 4 | -83 | 6 | 5.3 | 3.8 | 3.6 | 4 | -84 | 6 | 5.6 | 4.5 | 4.3 | 4 | -85 | 6 | 5.8 | 5.2 | 5 | 4.3 | -86 | 6 | 6 | 6 | 5.8 | 4.9 | -87 | 6 | 6 | 6 | 6 | 5.6 | -88 | 6 | 6 | 6 | 6 | 4 | <p>$f(BER)$ for level > -60 dBm</p> | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1e-2 | 2e-2 | 4e-2 | 6e-2 | 8e-2 | 1.1e-1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -40 | -0.2 | -0.1 | 0.1 | 0.4 | 1.2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -50 | -0.2 | -0.1 | 0.1 | 0.4 | 1.2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -60 | -0.2 | -0.1 | 0.1 | 0.4 | 1.2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -65 | 0 | 0.1 | 0.15 | 0.45 | 1.25 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -70 | 0.2 | 0.2 | 0.55 | 1.4 | 3.2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -72 | 0.6 | 0.4 | 0.65 | 1.5 | 3.3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -75 | 1.3 | 0.8 | 0.6 | 1.6 | 3.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -77 | 1.9 | 1.2 | 0.8 | 1 | 3.7 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -78 | 2.5 | 1.6 | 1.1 | 1.3 | 3.8 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -79 | 3.5 | 2.5 | 1.4 | 1.7 | 3.9 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -80 | 4.6 | 3.4 | 1.9 | 2.1 | 3.95 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -81 | 5.5 | 4.3 | 2.5 | 2.55 | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -82 | 6 | 4.9 | 3.1 | 3 | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -83 | 6 | 5.3 | 3.8 | 3.6 | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -84 | 6 | 5.6 | 4.5 | 4.3 | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -85 | 6 | 5.8 | 5.2 | 5 | 4.3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -86 | 6 | 6 | 6 | 5.8 | 4.9 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -87 | 6 | 6 | 6 | 6 | 5.6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -88 | 6 | 6 | 6 | 6 | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SFN | 11.0 dB | <table border="1"> <caption>BER before LDPC</caption> <thead> <tr> <th></th><th>margin</th></tr> </thead> <tbody> <tr><td><= 1.3 E-1</td><td>>= 2</td></tr> <tr><td><= 1.1 E-1</td><td>>= 6</td></tr> <tr><td><= 1.0 E-1</td><td>>= 10</td></tr> <tr><td><= 6E-2</td><td>>= 13</td></tr> <tr><td><= 4E-2</td><td>>= 15</td></tr> <tr><td><= 1E-3</td><td>>= 18</td></tr> </tbody> </table> <table border="1"> <caption>LDPC iterations</caption> <thead> <tr> <th></th><th>margin</th></tr> </thead> <tbody> <tr><td><= 40</td><td>>= 2</td></tr> <tr><td><= 25</td><td>>= 6</td></tr> <tr><td><= 17</td><td>>= 10</td></tr> <tr><td><= 15</td><td>>= 12</td></tr> <tr><td><= 12</td><td>>= 15</td></tr> <tr><td><= 7</td><td>>= 18</td></tr> </tbody> </table> | | margin | <= 1.3 E-1 | >= 2 | <= 1.1 E-1 | >= 6 | <= 1.0 E-1 | >= 10 | <= 6E-2 | >= 13 | <= 4E-2 | >= 15 | <= 1E-3 | >= 18 | | margin | <= 40 | >= 2 | <= 25 | >= 6 | <= 17 | >= 10 | <= 15 | >= 12 | <= 12 | >= 15 | <= 7 | >= 18 | <p>Lc_{sfn}</p> <table border="1"> <caption>BER</caption> <thead> <tr> <th>1e-2</th><th>2e-2</th><th>4e-2</th><th>6e-2</th><th>8e-2</th><th>1.1e-1</th></tr> </thead> <tbody> <tr><td>-40</td><td>0.4</td><td>0.6</td><td>0.8</td><td>2</td><td>4</td><td>5.9</td></tr> <tr><td>-50</td><td>0.4</td><td>0.6</td><td>0.8</td><td>2</td><td>4</td><td>5.9</td></tr> <tr><td>-60</td><td>0.45</td><td>0.65</td><td>0.85</td><td>2.05</td><td>4</td><td>5.9</td></tr> <tr><td>-65</td><td>0.6</td><td>0.7</td><td>0.95</td><td>2.1</td><td>4</td><td>5.9</td></tr> <tr><td>-70</td><td>0.8</td><td>0.8</td><td>1.1</td><td>2.2</td><td>4.1</td><td>6</td></tr> <tr><td>-72</td><td>1.2</td><td>1.1</td><td>1.25</td><td>2.3</td><td>4.1</td><td>6</td></tr> <tr><td>-75</td><td>1.6</td><td>1.4</td><td>1.4</td><td>2.4</td><td>4.1</td><td>6</td></tr> <tr><td>-77</td><td>2</td><td>1.7</td><td>1.5</td><td>2.5</td><td>4.1</td><td>6</td></tr> <tr><td>-78</td><td>2.5</td><td>2.2</td><td>1.75</td><td>2.5</td><td>3.8</td><td>6</td></tr> <tr><td>-79</td><td>3.5</td><td>2.7</td><td>1.95</td><td>2.6</td><td>3.8</td><td>5.8</td></tr> <tr><td>-80</td><td>4.6</td><td>3.3</td><td>2.2</td><td>2.7</td><td>3.8</td><td>5.3</td></tr> <tr><td>-81</td><td>6</td><td>4</td><td>2.7</td><td>2.9</td><td>3.8</td><td>5.1</td></tr> <tr><td>-82</td><td>6</td><td>5</td><td>3.5</td><td>3.3</td><td>4.2</td><td>5.1</td></tr> <tr><td>-83</td><td>6</td><td>6</td><td>4.8</td><td>3.9</td><td>4.4</td><td>5.1</td></tr> <tr><td>-84</td><td>6</td><td>6</td><td>6</td><td>4.5</td><td>5</td><td>5.3</td></tr> <tr><td>-85</td><td>6</td><td>6</td><td>6</td><td>5.5</td><td>5.5</td><td>5.8</td></tr> <tr><td>-86</td><td>6</td><td>6</td><td>6</td><td>6</td><td>6</td><td>6</td></tr> <tr><td>-87</td><td>6</td><td>6</td><td>6</td><td>6</td><td>6</td><td>6</td></tr> <tr><td>-88</td><td>6</td><td>6</td><td>6</td><td>6</td><td>6</td><td>6</td></tr> </tbody> </table> <p>dB Additional margin (function of the level and BER) SFN</p> | 1e-2 | 2e-2 | 4e-2 | 6e-2 | 8e-2 | 1.1e-1 | -40 | 0.4 | 0.6 | 0.8 | 2 | 4 | 5.9 | -50 | 0.4 | 0.6 | 0.8 | 2 | 4 | 5.9 | -60 | 0.45 | 0.65 | 0.85 | 2.05 | 4 | 5.9 | -65 | 0.6 | 0.7 | 0.95 | 2.1 | 4 | 5.9 | -70 | 0.8 | 0.8 | 1.1 | 2.2 | 4.1 | 6 | -72 | 1.2 | 1.1 | 1.25 | 2.3 | 4.1 | 6 | -75 | 1.6 | 1.4 | 1.4 | 2.4 | 4.1 | 6 | -77 | 2 | 1.7 | 1.5 | 2.5 | 4.1 | 6 | -78 | 2.5 | 2.2 | 1.75 | 2.5 | 3.8 | 6 | -79 | 3.5 | 2.7 | 1.95 | 2.6 | 3.8 | 5.8 | -80 | 4.6 | 3.3 | 2.2 | 2.7 | 3.8 | 5.3 | -81 | 6 | 4 | 2.7 | 2.9 | 3.8 | 5.1 | -82 | 6 | 5 | 3.5 | 3.3 | 4.2 | 5.1 | -83 | 6 | 6 | 4.8 | 3.9 | 4.4 | 5.1 | -84 | 6 | 6 | 6 | 4.5 | 5 | 5.3 | -85 | 6 | 6 | 6 | 5.5 | 5.5 | 5.8 | -86 | 6 | 6 | 6 | 6 | 6 | 6 | -87 | 6 | 6 | 6 | 6 | 6 | 6 | -88 | 6 | 6 | 6 | 6 | 6 | 6 | <p>$f(BER)$ for level > -60 dBm</p> |
| | margin | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 1.3 E-1 | >= 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 1.1 E-1 | >= 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 1.0 E-1 | >= 10 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 6E-2 | >= 13 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 4E-2 | >= 15 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 1E-3 | >= 18 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | margin | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 40 | >= 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 25 | >= 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 17 | >= 10 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 15 | >= 12 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 12 | >= 15 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 7 | >= 18 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1e-2 | 2e-2 | 4e-2 | 6e-2 | 8e-2 | 1.1e-1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -40 | 0.4 | 0.6 | 0.8 | 2 | 4 | 5.9 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -50 | 0.4 | 0.6 | 0.8 | 2 | 4 | 5.9 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -60 | 0.45 | 0.65 | 0.85 | 2.05 | 4 | 5.9 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -65 | 0.6 | 0.7 | 0.95 | 2.1 | 4 | 5.9 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -70 | 0.8 | 0.8 | 1.1 | 2.2 | 4.1 | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -72 | 1.2 | 1.1 | 1.25 | 2.3 | 4.1 | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -75 | 1.6 | 1.4 | 1.4 | 2.4 | 4.1 | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -77 | 2 | 1.7 | 1.5 | 2.5 | 4.1 | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -78 | 2.5 | 2.2 | 1.75 | 2.5 | 3.8 | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -79 | 3.5 | 2.7 | 1.95 | 2.6 | 3.8 | 5.8 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -80 | 4.6 | 3.3 | 2.2 | 2.7 | 3.8 | 5.3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -81 | 6 | 4 | 2.7 | 2.9 | 3.8 | 5.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -82 | 6 | 5 | 3.5 | 3.3 | 4.2 | 5.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -83 | 6 | 6 | 4.8 | 3.9 | 4.4 | 5.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -84 | 6 | 6 | 6 | 4.5 | 5 | 5.3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -85 | 6 | 6 | 6 | 5.5 | 5.5 | 5.8 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -86 | 6 | 6 | 6 | 6 | 6 | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -87 | 6 | 6 | 6 | 6 | 6 | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -88 | 6 | 6 | 6 | 6 | 6 | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

TABLE A3.8

Results (AWGN interference limited) with different input levels (MFN) (16k extended, PP2, 19/128, 64 QAM, 1/2)

TABLE A3.9

Results with different input levels (SFN)* (16k extended, PP2, 19/128, 64 QAM, 1/2)

(*) 1 Useful signal + 1 SFN auto-interference @600 microseconds.

TABLE A3.10
(32k extended, PP4, 1/32, 256 QAM, 3/5)

| | Ref MER | LDPC iter. and BER Tables | Lc | $f(BER)$ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|------------|---------|--|---|------------|---------|------|---------|------|---------|------|---------|------|---------|-------|--|--------|-------|------|-------|------|-------|------|------|------|------|------|------|-------|--|------------|------|------|------|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|---|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|---|-----|-----|-----|-----|-----|-----|-----|------|-----|---|-----|-----|-----|-----|-----|-----|-----|----------------------|-----|---|---|-----|-----|-----|---|-----|---|-----|-----|---|---|-----|-----|-----|---|---|-----|---|-----|---|---|---|-----|-----|---|---|---|-----|---|
| MFN | 17.3 dB | | <table border="1"> <caption>Lc_{mfn} BER</caption> <thead> <tr> <th>level(dBm)</th> <th>1e-2</th> <th>2e-2</th> <th>4e-2</th> <th>6e-2</th> </tr> </thead> <tbody> <tr><td>-60</td><td>1.3</td><td>0.9</td><td>0.5</td><td>0.6</td></tr> <tr><td>-61</td><td></td><td></td><td></td><td></td></tr> <tr><td>-62</td><td></td><td></td><td></td><td></td></tr> <tr><td>-63</td><td></td><td></td><td></td><td></td></tr> <tr><td>-64</td><td></td><td></td><td></td><td></td></tr> <tr><td>-65</td><td>1.3</td><td>0.9</td><td>0.5</td><td>0.6</td></tr> <tr><td>-66</td><td>1.8</td><td>1.1</td><td>0.7</td><td>0.7</td></tr> <tr><td>-67</td><td>2.8</td><td>1.6</td><td>1</td><td>0.9</td></tr> <tr><td>-68</td><td>4</td><td>2.4</td><td>1.4</td><td>1.1</td></tr> <tr><td>-69</td><td>5.5</td><td>3.8</td><td>1.9</td><td>1.4</td></tr> <tr><td>-70</td><td>6</td><td>5.5</td><td>2.5</td><td>1.8</td></tr> <tr><td>-71</td><td>6</td><td>6</td><td>3.3</td><td>2.1</td></tr> <tr><td>-72</td><td>6</td><td>6</td><td>4.5</td><td>2.6</td></tr> <tr><td>-73</td><td>6</td><td>6</td><td>5.5</td><td>3.5</td></tr> <tr><td>-74</td><td>6</td><td>6</td><td>6</td><td>6</td></tr> </tbody> </table> <p>dB Additional margin Lc (function of the level) MFN</p> <p>Legend: BER 1E-2 (red squares), BER 2E-2 (green triangles), BER 4E-2 (purple crosses), BER 6E-2 (blue diamonds)</p> | level(dBm) | 1e-2 | 2e-2 | 4e-2 | 6e-2 | -60 | 1.3 | 0.9 | 0.5 | 0.6 | -61 | | | | | -62 | | | | | -63 | | | | | -64 | | | | | -65 | 1.3 | 0.9 | 0.5 | 0.6 | -66 | 1.8 | 1.1 | 0.7 | 0.7 | -67 | 2.8 | 1.6 | 1 | 0.9 | -68 | 4 | 2.4 | 1.4 | 1.1 | -69 | 5.5 | 3.8 | 1.9 | 1.4 | -70 | 6 | 5.5 | 2.5 | 1.8 | -71 | 6 | 6 | 3.3 | 2.1 | -72 | 6 | 6 | 4.5 | 2.6 | -73 | 6 | 6 | 5.5 | 3.5 | -74 | 6 | 6 | 6 | 6 | Not relevant for MFN | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| level(dBm) | 1e-2 | 2e-2 | 4e-2 | 6e-2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -60 | 1.3 | 0.9 | 0.5 | 0.6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -61 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -62 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -63 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -64 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -65 | 1.3 | 0.9 | 0.5 | 0.6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -66 | 1.8 | 1.1 | 0.7 | 0.7 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -67 | 2.8 | 1.6 | 1 | 0.9 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -68 | 4 | 2.4 | 1.4 | 1.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -69 | 5.5 | 3.8 | 1.9 | 1.4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -70 | 6 | 5.5 | 2.5 | 1.8 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -71 | 6 | 6 | 3.3 | 2.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -72 | 6 | 6 | 4.5 | 2.6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -73 | 6 | 6 | 5.5 | 3.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -74 | 6 | 6 | 6 | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SFN | 17.3 dB | <table border="1"> <caption>BER before LDPC</caption> <thead> <tr> <th></th> <th>margin</th> </tr> </thead> <tbody> <tr><td><= 8E-2</td><td>>= 1</td></tr> <tr><td><= 6E-2</td><td>>= 3</td></tr> <tr><td><= 4E-2</td><td>>= 4</td></tr> <tr><td><= 1E-3</td><td>>= 8</td></tr> <tr><td><= 1E-4</td><td>>= 12</td></tr> </tbody> </table> <table border="1"> <caption>LDPC iterations</caption> <thead> <tr> <th></th> <th>margin</th> </tr> </thead> <tbody> <tr><td><= 20</td><td>>= 1</td></tr> <tr><td><= 15</td><td>>= 3</td></tr> <tr><td><= 10</td><td>>= 5</td></tr> <tr><td><= 6</td><td>>= 7</td></tr> <tr><td><= 5</td><td>>= 9</td></tr> <tr><td><= 4</td><td>>= 15</td></tr> </tbody> </table> | | margin | <= 8E-2 | >= 1 | <= 6E-2 | >= 3 | <= 4E-2 | >= 4 | <= 1E-3 | >= 8 | <= 1E-4 | >= 12 | | margin | <= 20 | >= 1 | <= 15 | >= 3 | <= 10 | >= 5 | <= 6 | >= 7 | <= 5 | >= 9 | <= 4 | >= 15 | <table border="1"> <caption>Lc_{sfn} BER</caption> <thead> <tr> <th>level(dBm)</th> <th>1e-2</th> <th>2e-2</th> <th>4e-2</th> <th>6e-2</th> </tr> </thead> <tbody> <tr><td>-60</td><td></td><td></td><td></td><td></td></tr> <tr><td>-61</td><td></td><td></td><td></td><td></td></tr> <tr><td>-62</td><td></td><td></td><td></td><td></td></tr> <tr><td>-63</td><td></td><td></td><td></td><td></td></tr> <tr><td>-64</td><td></td><td></td><td></td><td></td></tr> <tr><td>-65</td><td>1.7</td><td>1.4</td><td>1.3</td><td>1.6</td></tr> <tr><td>-66</td><td>2</td><td>1.6</td><td>1.4</td><td>1.6</td></tr> <tr><td>-67</td><td>2.6</td><td>1.9</td><td>1.5</td><td>1.65</td></tr> <tr><td>-68</td><td>4</td><td>2.5</td><td>1.6</td><td>1.7</td></tr> <tr><td>-69</td><td>5.2</td><td>3.5</td><td>1.8</td><td>1.8</td></tr> <tr><td>-70</td><td>6</td><td>5</td><td>2.1</td><td>1.9</td></tr> <tr><td>-71</td><td>6</td><td>5.8</td><td>3</td><td>2.3</td></tr> <tr><td>-72</td><td>6</td><td>6</td><td>4.8</td><td>3.1</td></tr> <tr><td>-73</td><td>6</td><td>6</td><td>5.8</td><td>4</td></tr> <tr><td>-74</td><td>6</td><td>6</td><td>6</td><td>4.9</td></tr> <tr><td>-75</td><td>6</td><td>6</td><td>6</td><td>5.5</td></tr> </tbody> </table> <p>dB Additional margin Lc (function of the level) SFN</p> <p>Legend: BER1E-2 (red squares), BER2E-2 (green triangles), BER4E-2 (purple crosses), BER6E-2 (blue diamonds)</p> | level(dBm) | 1e-2 | 2e-2 | 4e-2 | 6e-2 | -60 | | | | | -61 | | | | | -62 | | | | | -63 | | | | | -64 | | | | | -65 | 1.7 | 1.4 | 1.3 | 1.6 | -66 | 2 | 1.6 | 1.4 | 1.6 | -67 | 2.6 | 1.9 | 1.5 | 1.65 | -68 | 4 | 2.5 | 1.6 | 1.7 | -69 | 5.2 | 3.5 | 1.8 | 1.8 | -70 | 6 | 5 | 2.1 | 1.9 | -71 | 6 | 5.8 | 3 | 2.3 | -72 | 6 | 6 | 4.8 | 3.1 | -73 | 6 | 6 | 5.8 | 4 | -74 | 6 | 6 | 6 | 4.9 | -75 | 6 | 6 | 6 | 5.5 | <p>Y-axis: f(BER)</p> <p>X-axis: level (dBm) from 4.0E-05 to 8.0E-02</p> <p>Graph shows f(BER) increasing from approximately -0.35 at 4.0E-05 to 0.6 at 8.0E-02.</p> <p>$f(BER)$ for level > -60 dBm</p> |
| | margin | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 8E-2 | >= 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 6E-2 | >= 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 4E-2 | >= 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 1E-3 | >= 8 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 1E-4 | >= 12 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | margin | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 20 | >= 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 15 | >= 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 10 | >= 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 6 | >= 7 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 5 | >= 9 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <= 4 | >= 15 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| level(dBm) | 1e-2 | 2e-2 | 4e-2 | 6e-2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -60 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -61 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -62 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -63 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -64 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -65 | 1.7 | 1.4 | 1.3 | 1.6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -66 | 2 | 1.6 | 1.4 | 1.6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -67 | 2.6 | 1.9 | 1.5 | 1.65 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -68 | 4 | 2.5 | 1.6 | 1.7 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -69 | 5.2 | 3.5 | 1.8 | 1.8 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -70 | 6 | 5 | 2.1 | 1.9 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -71 | 6 | 5.8 | 3 | 2.3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -72 | 6 | 6 | 4.8 | 3.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -73 | 6 | 6 | 5.8 | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -74 | 6 | 6 | 6 | 4.9 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -75 | 6 | 6 | 6 | 5.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

TABLE A3.11

Results* (AWGN interference limited) with different input levels (MFN)

(32k extended, PP4, 1/32, 256 QAM, 3/5)

TABLE A3.12

Results with different input levels (SFN)*
(32k extended, PP4, 1/32, 256 QAM, 3/5)

| SFN | ref. MER (dB) | 17.3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|-------------|-------------------|-----------------|--------------|-------------|------------------|-----------------|--------------|-------------|------------------|-----------------|--------------|-------------|------------------|-----------------|--------------|-------------|------------------|-----------------|--------------|-------------|------------------|-----------------|--------------|-------------|------------------|-----------------|--------------|-------------|------------------|---------|---------|------|-----|------|------|----|
| level (dBm) | -50 | | | | -65 | | | | -68 | | | | -70 | | | | -72 | | | | -74 | | | | | | | | | | | | | | | |
| C/I (dB) | margin (MFN) (dB) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER ref (dB) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER ref (dB) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER ref (dB) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER ref (dB) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER ref (dB) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER ref (dB) | BER Before LDPC | MER PLP (dB) | margin (dB) | x = MER ref (dB) | | | | | | | |
| Int.off | 8.0E-05 | 40.1 | | 2.5E-04 | 30.1 | | | 3.1E-03 | 22.2 | | | 4.0E-02 | 25.3 | | | 2.4E-02 | 23.3 | | | 4.7E-02 | 21.0 | | | Int.off | | | | | | | | | | | | |
| 40 | 20.0 | 8.2E-05 | 35.4 | 20.0 | 18.1 | -1.9 | 4.9E-04 | 29.3 | 20.0 | 12.0 | -8.0 | 4.2E-03 | 26.8 | 19.5 | 9.5 | -10.0 | 1.2E-02 | 25.0 | 19.0 | 7.7 | -11.3 | 2.6E-02 | 23.1 | 19.0 | 5.8 | -13.2 | 4.8E-02 | 20.9 | 18.0 | 3.6 | -14.4 | 40 | | | | |
| 39 | 19.0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 39 | | | | | | |
| 38 | 18.0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 38 | | | | | | |
| 37 | 17.0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 37 | | | | | | |
| 36 | 16.0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 36 | | | | | | |
| 35 | 15.0 | 8.6E-05 | 31.6 | 15.0 | 14.3 | -0.7 | 1.6E-03 | 28.1 | 15.0 | 10.8 | -4.2 | 7.0E-03 | 26.0 | 14.5 | 8.7 | -5.8 | 1.6E-02 | 24.5 | 14.0 | 7.2 | -6.8 | 2.9E-02 | 22.7 | 14.0 | 5.4 | -8.6 | 5.1E-02 | 20.5 | 13.0 | 3.2 | -9.8 | 35 | | | | |
| 34 | 14.0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 5.1E-02 | 20.5 | 12.0 | 3.2 | -8.8 | 34 | |
| 33 | 13.0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 5.3E-02 | 20.3 | 11.0 | 3.0 | -8.0 | 33 | |
| 32 | 12.0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 5.5E-02 | 20.1 | 10.0 | 2.8 | -7.2 | 32 | |
| 31 | 11.0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 5.7E-02 | 19.8 | 9.0 | 2.5 | -6.5 | 31 | |
| 30 | 10.0 | 3.2E-03 | 27.0 | 10.0 | 9.7 | -0.3 | 9.8E-03 | 25.4 | 10.0 | 8.1 | -1.9 | 1.8E-02 | 24.1 | 9.5 | 6.8 | -2.7 | 2.7E-02 | 23.0 | 9.0 | 5.7 | -3.3 | 4.0E-02 | 21.5 | 9.0 | 4.2 | -4.8 | 5.9E-02 | 19.6 | 8.0 | 2.3 | -5.7 | 30 | | | | |
| 29 | 9.0 | 6.6E-03 | 26.0 | 9.0 | 8.7 | -0.3 | 1.4E-02 | 24.7 | 9.0 | 7.4 | -1.6 | 2.2E-02 | 23.6 | 8.5 | 6.3 | -2.2 | 3.1E-02 | 22.5 | 8.0 | 5.2 | -2.8 | | | | | | | | | | 6.1E-02 | 19.3 | 7.0 | 2.0 | -5.0 | 29 |
| 28 | 8.0 | 1.2E-02 | 25.0 | 8.0 | 7.7 | -0.3 | 1.9E-02 | 23.9 | 8.0 | 6.6 | -1.4 | 2.7E-02 | 22.9 | 7.5 | 5.6 | -1.9 | 3.5E-02 | 21.9 | 7.0 | 4.6 | -2.4 | 4.8E-02 | 20.5 | 7.0 | 3.2 | -3.8 | 6.5E-02 | 19.0 | 6.0 | 1.7 | -4.3 | 28 | | | | |
| 27 | 7.0 | 1.9E-02 | 23.9 | 7.0 | 6.6 | -0.4 | 2.6E-02 | 23.0 | 7.0 | 5.7 | -1.3 | 3.3E-02 | 22.1 | 6.5 | 4.8 | -1.7 | 4.1E-02 | 21.2 | 6.0 | 3.9 | -2.1 | 5.3E-02 | 19.9 | 6.0 | 2.6 | -3.4 | 6.9E-02 | 18.6 | 5.0 | 1.3 | -3.7 | 27 | | | | |
| 26 | 6.0 | 2.7E-02 | 22.9 | 6.0 | 5.6 | -0.4 | 3.4E-02 | 22.1 | 6.0 | 4.8 | -1.2 | 4.1E-02 | 21.2 | 5.5 | 3.9 | -1.6 | 4.8E-02 | 20.3 | 5.0 | 3.0 | -2.0 | 5.9E-02 | 19.2 | 5.0 | 1.9 | -3.1 | 7.4E-02 | 18.2 | 4.0 | 0.9 | -3.1 | 26 | | | | |
| 25 | 5.0 | 3.7E-02 | 21.7 | 5.0 | 4.4 | -0.6 | 4.3E-02 | 20.9 | 5.0 | 3.6 | -1.4 | 4.9E-02 | 20.1 | 4.5 | 2.8 | -1.7 | 5.6E-02 | 19.4 | 4.0 | 2.1 | -1.9 | 6.7E-02 | 18.6 | 4.0 | 1.3 | -2.7 | 7.9E-02 | 17.9 | 3.0 | 0.6 | -2.4 | 25 | | | | |
| 24 | 4.0 | 4.8E-02 | 20.4 | 4.0 | 3.1 | -0.9 | 5.3E-02 | 19.7 | 4.0 | 2.4 | -1.6 | 5.9E-02 | 19.1 | 3.5 | 1.8 | -1.7 | 6.5E-02 | 18.5 | 3.0 | 1.2 | -1.8 | 7.5E-02 | 18.0 | 3.0 | 0.7 | -2.3 | 8.6E-02 | 17.5 | 2.0 | 0.2 | -1.8 | 24 | | | | |
| 23 | 3.0 | 6.0E-02 | 19.1 | 3.0 | 1.8 | -1.2 | 6.4E-02 | 18.6 | 3.0 | 1.3 | -1.7 | 6.9E-02 | 18.2 | 2.5 | 0.9 | -1.6 | 7.4E-02 | 17.9 | 2.0 | 0.6 | -1.4 | 8.4E-02 | 17.5 | 2.0 | 0.2 | -1.8 | 9.3E-02 | 17.0 | 1.0 | -0.3 | -1.3 | 23 | | | | |
| 22 | 2.0 | 7.2E-02 | 18.0 | 2.0 | 0.7 | -1.3 | 7.6E-02 | 17.8 | 2.0 | 0.5 | -1.5 | 8.0E-02 | 17.5 | 1.5 | 0.2 | -1.3 | 8.5E-02 | 17.3 | 1.0 | 0.0 | -1.0 | 9.4E-02 | 16.9 | 1.0 | -0.4 | -1.4 | 1.0E-01 | 16.4 | 0.0 | -0.9 | -0.9 | 22 | | | | |
| 21 | 1.0 | 8.5E-02 | 17.2 | 1.0 | -0.1 | -1.1 | 8.8E-02 | 16.9 | 1.0 | -0.4 | -1.4 | 9.2E-02 | 16.7 | 0.5 | -0.6 | -1.1 | 9.6E-02 | 16.5 | 0.0 | -0.8 | -0.8 | 1.0E-01 | 16.2 | 0.0 | -1.1 | -1.1 | 1.1E-01 | 16.1 | -0.5 | -1.2 | -0.7 | 21.5 | | | | |
| 20.5 | 0.5 | 9.6E-02 | 16.7 | 0.5 | -0.6 | -1.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 20.5 | |
| 20 | 0.0 | 9.8E-02 | 16.2 | 0.0 | -1.1 | -1.1 | 1.0E-01 | 16.0 | 0.0 | -1.3 | -1.3 | 1.1E-01 | 15.8 | -0.5 | -1.5 | -1 | 1.0E-01 | 16.1 | -0.5 | -1.2 | -0.7 | 1.1E-01 | 15.8 | -0.5 | 0.0 | -1.1 | | | | | | | 20 | | | |
| 19.5 | -0.5 | 1.1E-01 | 15.6 | -0.5 | -1.7 | -1.2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 19.5 | |

(*) 1 Useful signal + 1 SFN auto-interference @600 microseconds.

Annex 4 to Part 1

Laboratory tests on DVB-T2 performed by Rai Way S.p.A

Some laboratory tests were performed in order to identify a method for the evaluation of DVB-T2 services.

The analysis was focused on the behaviour of the following parameters: MER of a PLP; BER before LDPC and BER before BCH.

Some trials have been carried out comparing DVB-T and DVB-T2.

Test in Band IV and Band III – SFN with a signal outside Guard Interval

A first set of trials were performed in order to study the variability of the MER of PLP and the BER, BER before LDPC and BER before BCH, in an SFN with a signal outside the Guard Interval. The trials were carried out changing the level of this interferer.

Tests have been executed in band IV and in band III. Various Pilot Pattern profiles (PP), Code Rates (CR) and Guard Interval (GI) have been selected.

A signal with the following general features was generated by a high level professional equipment:

- Single PLP
- Constellation: 256 QAM (rotated where specified)
- FFT variant: 32k Not Extended
- Single Input Single Output (SISO) transmission
- Signal level 47.8 dB μ V

Band IV measurements

Channel 21 (474 MHz) or CH 30 (546 MHz)

Interferer: delay 600 μ s, variable level

| | PP2 | PP4 | PP7 |
|----------------|---------------------------------------|-------------------|-------------------|
| Guard Interval | 1/16, 224 μ s 1/8, 448 μ s | 1/16, 224 μ s | 1/128, 28 μ s |
| Code Rate | 3/5 2/3 3/4 | 3/5 2/3 3/4 | 3/4 |

| PP2 | GI 1/16 – CR 3/5 | | | | GI 1/16 – CR 2/3 | | | |
|-------|---------------------|-----------|----------|-----------------|------------------|-----------|----------|-----------------|
| | Interferer level dB | Iteration | MER PLP | BER before LDPC | BER before BCH | Iteration | MER PLP | BER before LDPC |
| -40,0 | 1,1 | 33,3 | 1,30E-06 | 0,00E+00 | 1,1 | 33,2 | 2,20E-06 | 0,00E+00 |
| -35,0 | 2,1 | 30,4 | 7,00E-05 | 0,00E+00 | 2,0 | 30,4 | 8,00E-05 | 0,00E+00 |
| -30,0 | 4,5 | 26,4 | 5,00E-03 | 0,00E+00 | 3,5 | 26,4 | 5,00E-03 | 0,00E+00 |
| -25,0 | 11,3 | 21,1 | 4,00E-02 | 0,00E+00 | 7,3 | 21,1 | 4,00E-02 | 0,00E+00 |
| -22,0 | 22,0 | 17,7 | 7,60E-02 | 0,00E+00 | 15,9 | 17,7 | 7,00E-02 | 0,00E+00 |
| -21,9 | | | | | 16,8 | 17,6 | 8,00E-02 | 0,00E+00 |
| -21,8 | | | | | 17,7 | 17,5 | 8,00E-02 | 0,00E+00 |
| -21,7 | | | | | 19,0 | 17,4 | 8,00E-02 | 0,00E+00 |
| -21,6 | | | | | 20,5 | 17,4 | 8,00E-02 | 0,00E+00 |
| -21,5 | | | | | 22,5 | 17,3 | 8,00E-02 | 1,00E-04 |
| -21,4 | | | | | 27,0 | 17,2 | 8,00E-02 | 3,00E-03 |
| -21,0 | 30,3 | 17,2 | 8,80E-02 | 0,00E+00 | | | | |
| -20,0 | 36,1 | 16,2 | 1,00E-01 | 0,00E+00 | | | | |
| -19,9 | 36,1 | 16,1 | 1,00E-01 | 2,70E-09 | | | | |
| -19,8 | 36,2 | 16,0 | 1,00E-01 | 1,40E-07 | | | | |
| -19,7 | 36,2 | 15,9 | 1,00E-01 | 1,70E-06 | | | | |
| -19,6 | 36,2 | 15,8 | 1,00E-01 | 1,30E-05 | | | | |
| -19,5 | 36,3 | 15,7 | 1,00E-01 | 8,00E-05 | | | | |
| -19,4 | 36,4 | 15,6 | 1,00E-01 | 4,00E-04 | | | | |
| -19,3 | 36,5 | 15,5 | 1,00E-01 | 2,00E-03 | | | | |
| -19,2 | 36,5 | 15,3 | 1,00E-01 | 8,00E-03 | | | | |

| PP2 | GI 1/8 – CR 2/3 | | | | GI 1/8 – CR 3/4 | | | |
|-------|---------------------|-----------|------------|-----------------|-----------------|------------|-----------------|----------------|
| | Interferer level dB | Iteration | MER PLP dB | BER before LDPC | Iteration | MER PLP dB | BER before LDPC | BER before BCH |
| -40,0 | 1,1 | 33,2 | 3,00E-06 | 0,00E+00 | 1,3 | 33,2 | 6,00E-06 | 0,00E+00 |
| -35,0 | 2,0 | 30,4 | 7,00E-05 | 0,00E+00 | 2,0 | 30,4 | 8,00E-05 | 0,00E+00 |
| -30,0 | 3,5 | 26,3 | 5,00E-03 | 0,00E+00 | 3,5 | 26,3 | 5,00E-03 | 0,00E+00 |
| -25,0 | 7,4 | 21,0 | 4,00E-02 | 0,00E+00 | 9,5 | 21,0 | 4,00E-02 | 0,00E+00 |
| -24,0 | | | | | 13,9 | 19,6 | 5,00E-02 | 0,00E+00 |
| -23,5 | | | | | 19,4 | 19,0 | 6,00E-02 | 0,00E+00 |
| -23,4 | | | | | 21,6 | 18,8 | 6,00E-02 | 0,00E+00 |
| -23,3 | | | | | 26,0 | 18,7 | 6,00E-02 | 5,00E-04 |
| -22,0 | 16,4 | 17,7 | 7,80E-02 | 0,00E+00 | | | | |
| -21,9 | 17,8 | 17,6 | 8,00E-02 | 0,00E+00 | | | | |
| -21,8 | 18,7 | 17,5 | 8,00E-02 | 0,00E+00 | | | | |
| -21,7 | 20,0 | 17,4 | 8,20E-02 | 0,00E+00 | | | | |
| -21,6 | 22,3 | 17,3 | 8,30E-02 | 3,00E-06 | | | | |
| -21,5 | 26,0 | 17,2 | 8,40E-02 | 2,00E-03 | | | | |

| PP7 | GI 1/128 – CR 3/4 Rotated constellation | | | | |
|-------|--|-----------|------------|-----------------|----------------|
| | Interferer level dB | Iteration | MER PLP dB | BER before LDPC | BER before BCH |
| -40,0 | 1,1 | 33,9 | 2,60E-06 | 0,00E+00 | |
| -35,0 | 1,8 | 31,0 | 2,40E-05 | 0,00E+00 | |
| -30,0 | 3,2 | 27,0 | 2,60E-03 | 0,00E+00 | |
| -25,0 | 8,1 | 22,2 | 3,00E-02 | 0,00E+00 | |
| -23,0 | 18,1 | 19,6 | 5,70E-02 | 0,00E+00 | |
| -22,7 | 26,0 | 19,2 | 6,00E-02 | 7,00E-04 | |

Remarks on Band IV measurements

BER before BCH is generally equal to 0 and when it becomes greater, the failure threshold is reached.

The MER PLP has different lower limit, depending on the CR.

PP2

CR 3/5: 15.3 dB

CR 2/3: 17.2 dB

CR 3/4: 18.7 dB

PP4

CR 3/5: 15.2 dB

CR 2/3: 17.3 dB

CR 3/4: 18.9 dB

PP7

CR 3/4: 19.2 dB

Relation between the level of the interferer and the MER PLP: $\Delta = \text{Level of Interferer} - \text{MER}$

| Interferer level dB | PP2 | | PP4 | | PP7 | |
|---------------------|------------|------------------------------|------------|------------------------------|------------|------------------------------|
| | MER PLP dB | $\Delta = I - \text{MER}$ dB | MER PLP dB | $\Delta = I - \text{MER}$ dB | MER PLP dB | $\Delta = I - \text{MER}$ dB |
| -40,0 | 33,2 | 6,8 | 33,3 | 6,7 | 33,9 | 6,1 |
| -35,0 | 30,4 | 4,6 | 30,5 | 4,5 | 31,0 | 4,0 |
| -30,0 | 26,4 | 3,7 | 26,5 | 3,5 | 27,0 | 3,0 |
| -25,0 | 21,1 | 4,0 | 21,5 | 3,5 | 22,2 | 2,8 |
| -24,0 | 19,6 | 4,4 | 20,2 | 3,8 | | |
| -23,9 | | | 20,1 | 3,8 | | |
| -23,8 | | | 19,9 | 3,9 | | |
| -23,7 | | | 19,8 | 3,9 | | |
| -23,6 | | | 19,6 | 4,0 | | |
| -23,5 | 19,0 | 4,5 | 19,5 | 4,0 | | |

| Interferer level dB | PP2 | | PP4 | | PP7 | |
|------------------------|---------------|-----------------------|---------------|-----------------------|---------------|-----------------------|
| | MER PLP dB | $\Delta=I$ -MER dB | MER PLP dB | $\Delta=I$ -MER dB | MER PLP dB | $\Delta=I$ -MER dB |
| -23,4 | 18,8 | 4,6 | 19,4 | 4,0 | | |
| -23,3 | 18,7 | 4,6 | 19,3 | 4,0 | | |
| -23,2 | | | 19,1 | 4,1 | | |
| -23,1 | | | 19,0 | 4,1 | | |
| -23,0 | | | 18,9 | 4,1 | 19,6 | 3,4 |
| -22,7 | | | | | 19,2 | 3,5 |
| -22,0 | 17,7 | 4,3 | 17,9 | 4,1 | | |
| -21,9 | 17,6 | 4,3 | 17,9 | 4,0 | | |
| -21,8 | 17,5 | 4,3 | 17,8 | 4,0 | | |
| -21,7 | 17,4 | 4,3 | 17,7 | 4,0 | | |
| -21,6 | 17,4 | 4,3 | 17,6 | 4,0 | | |
| -21,5 | 17,3 | 4,3 | 17,5 | 4,0 | | |
| -21,4 | 17,2 | 4,2 | 17,4 | 4,0 | | |
| -21,3 | | | 17,4 | 4,0 | | |
| -21,2 | | | 17,3 | 3,9 | | |
| -21,0 | 17,2 | 3,8 | 17,1 | 3,9 | | |
| -20,0 | 16,2 | 3,8 | 16,1 | 3,9 | | |
| -19,9 | 16,1 | 3,8 | 16,0 | 3,9 | | |
| -19,8 | 16,0 | 3,8 | 15,9 | 3,9 | | |
| -19,7 | 15,9 | 3,8 | 15,7 | 4,0 | | |
| -19,6 | 15,8 | 3,8 | 15,6 | 4,0 | | |
| -19,5 | 15,7 | 3,8 | 15,5 | 4,0 | | |
| -19,4 | 15,6 | 3,8 | 15,4 | 4,0 | | |
| -19,3 | 15,5 | 3,8 | 15,3 | 4,0 | | |
| -19,2 | 15,3 | 3,9 | 15,2 | 4,0 | | |

Band III measurements

Channel 9 (205.5 MHz – 7 MHz channel)

Interferer: delay 600 μ s/150 μ s, variable level

| | PP2 | PP7 |
|----------------|--|---|
| Guard Interval | 1/8, 512 μ s Interferer 600 μ s | 1/128, 32 μ s Interferer 150 μ s |
| Code Rate | 3/5 2/3 3/4 | 3/5 |

| PP2 | CR 3/5 | | | | CR 2/3 | | | | CR 3/4 | | | |
|-------|---------------------|-------|------------|-----------------|----------------|-------|------------|-----------------|----------------|-------|------------|-----------------|
| | Interferer level dB | Iter. | MER PLP dB | BER before LDPC | BER before BCH | Iter. | MER PLP dB | BER before LDPC | BER before BCH | Iter. | MER PLP dB | BER before LDPC |
| -40,0 | 1,5 | 33,8 | 9,00E-06 | 0,00E+00 | 1,4 | 34,0 | 1,00E-05 | 0,00E+00 | 1,5 | 34,0 | 1,30E-05 | 0,00E+00 |
| -35,0 | 2,1 | 30,7 | 3,00E-05 | 0,00E+00 | 1,9 | 30,8 | 2,70E-05 | 0,00E+00 | 1,8 | 30,8 | 2,80E-05 | 0,00E+00 |
| -30,0 | 3,8 | 26,5 | 4,00E-03 | 0,00E+00 | 3,3 | 26,5 | 4,00E-03 | 0,00E+00 | 3,2 | 26,5 | 4,00E-03 | 0,00E+00 |
| -25,0 | 12,6 | 21,1 | 4,20E-02 | 0,00E+00 | 8,3 | 21,1 | 4,00E-02 | 0,00E+00 | 9,3 | 21,1 | 4,00E-02 | 0,00E+00 |
| -23,5 | | | | | | | | | 16,0 | 19,2 | 5,90E-02 | 0,00E+00 |
| -23,2 | | | | | | | | | 20,6 | 18,9 | 6,20E-02 | 0,00E+00 |
| -23,1 | | | | | | | | | 23,8 | 18,8 | 6,30E-02 | 0,00E+00 |
| -23,0 | | | | | | | | | 30,0 | 18,7 | 6,40E-02 | 1,50E-03 |
| -22,0 | 24,3 | 17,8 | 7,70E-02 | 0,00E+00 | 15,6 | 17,8 | 7,70E-02 | 0,00E+00 | | | | |
| -21,5 | | | | | 20,0 | 17,4 | 8,30E-02 | 0,00E+00 | | | | |
| -21,4 | | | | | 21,5 | 17,3 | 8,50E-02 | 0,00E+00 | | | | |
| -21,3 | | | | | 23,2 | 17,3 | 8,60E-02 | 0,00E+00 | | | | |
| -21,2 | | | | | 26,0 | 17,2 | 8,70E-02 | 0,00E+00 | | | | |
| -21,1 | | | | | 30,0 | 17,1 | 8,90E-02 | 7,00E-05 | | | | |
| -21,0 | 32,0 | 17,0 | 9,00E-02 | 0,00E+00 | | | | | | | | |
| -20,0 | 36,2 | 16,0 | 1,00E-01 | 1,00E-07 | | | | | | | | |
| -19,9 | 36,3 | 15,9 | 1,00E-01 | 1,50E-06 | | | | | | | | |
| -19,8 | 36,3 | 15,7 | 1,00E-01 | 1,00E-05 | | | | | | | | |
| -19,7 | 36,4 | 15,6 | 1,00E-01 | 6,00E-05 | | | | | | | | |
| -19,6 | 36,5 | 15,5 | 1,00E-01 | 4,00E-04 | | | | | | | | |
| -19,5 | 36,5 | 15,4 | 1,00E-01 | 2,00E-03 | | | | | | | | |
| -19,4 | 36,5 | 15,3 | 1,00E-01 | 7,00E-03 | | | | | | | | |

| PP7 | CR 3/5 | | | | |
|-------|---------------------|-----------|------------|-----------------|----------------|
| | Interferer level dB | Iteration | MER PLP dB | BER before LDPC | BER before BCH |
| -40,0 | 2,7 | | 33,9 | 6,40E-05 | 0,00E+00 |
| -35,0 | 2,9 | | 30,8 | 7,00E-05 | 0,00E+00 |
| -30,0 | 4,5 | | 26,7 | 4,40E-03 | 0,00E+00 |
| -25,0 | 10,9 | | 22,0 | 4,00E-02 | 0,00E+00 |
| -23,0 | 17,0 | | 19,5 | 6,20E-02 | 0,00E+00 |
| -22,0 | 21,6 | | 18,3 | 7,00E-02 | 0,00E+00 |
| -21,0 | 28,6 | | 17,3 | 8,00E-02 | 0,00E+00 |
| -20,0 | 35,8 | | 16,2 | 9,00E-02 | 4,90E-09 |
| -19,5 | 36,3 | | 15,5 | 1,00E-01 | 5,00E-05 |
| -19,4 | 36,3 | | 15,4 | 1,00E-01 | 7,00E-04 |

Remarks on Band III measurements

BER before BCH is generally equal to 0 and when it becomes greater, the failure threshold is reached.

PP2

CR 3/5: 15.3 dB

CR 2/3: 17.1 dB

CR 3/4: 18.7 dB

PP7

CR 3/5: 15.4 dB

Relation between the level of the interferer and the MER PLP: Δ =Level of Interferer – MER

| Interferer level dB | PP2 | | PP7 | |
|------------------------|------------------|----------------------|------------------|----------------------|
| | MER PLP dB | $\Delta=I-MER$ dB | MER PLP dB | $\Delta=I-MER$ dB |
| -40,0 | 33,9 | 6,1 | 33,9 | 6,1 |
| -35,0 | 30,8 | 4,2 | 30,8 | 4,2 |
| -30,0 | 26,5 | 3,5 | 26,7 | 3,3 |
| -25,0 | 21,1 | 3,9 | 22,0 | 3,0 |
| -23,5 | 19,2 | 4,3 | | |
| -23,2 | 18,9 | 4,3 | | |
| -23,1 | 18,8 | 4,3 | | |
| -23,0 | 18,7 | 4,3 | 19,5 | 3,5 |
| -22,0 | 17,8 | 4,2 | 18,3 | 3,7 |
| -21,5 | 17,4 | 4,1 | | |
| -21,4 | 17,3 | 4,1 | | |
| -21,3 | 17,3 | 4,0 | | |
| -21,2 | 17,2 | 4,0 | | |
| -21,1 | 17,1 | 4,0 | | |
| -21,0 | 17,0 | 4,0 | 17,3 | 3,7 |
| -20,0 | 16,0 | 4,0 | 16,2 | 3,8 |
| -19,9 | 15,9 | 4,0 | | |
| -19,8 | 15,7 | 4,1 | | |
| -19,7 | 15,6 | 4,1 | | |
| -19,6 | 15,5 | 4,1 | | |
| -19,5 | 15,4 | 4,1 | 15,5 | 4,0 |
| -19,4 | 15,3 | 4,1 | 15,4 | 4,0 |

General remarks

The results obtained in the two bands are comparable.

BER before BCH is not a useful parameter for the assessment of the quality of service.

Test in Band IV. SFN with a signal outside GI. DVB-T vs DVB-T2

Two tests were focused on the comparison between DVB-T and DVB-T2 performance in a SFN with a signal outside GI.

In the first trial only the level of the interferer was varying. In the second one, the level and the delay have been modified.

First test

DVB-T2:

- CH 30
- 32k Not Extended
- 256 QAM
- SISO
- PP2
- Guard Interval: 1/16, 224 µs
- Code Rate: 2/3 – 34.5 Mbit/s

DVB-T:

- CH 30
- 64 QAM
- Guard Interval: 1/4, 224 µs
- Code Rate: 2/3 – 19.9 Mbit/s

SFN:

- Main signal 47 dBµV
- 2° signal: delay 8 µs, level –5 dB
- 3° signal: delay 57 µs, level –5 dB
- 4° signal: delay 148 µs, level –5 dB
- interferer: delay 234 µs (outside GI), variable level

| Level interferer | DVB-T2 | | | | DVB-T | | |
|---------------------|-----------|--------------------|-------------------|------------|----------|----------|------|
| | Iteration | BER before LDPC | BER before BCH | MER PLP | bBER | aBER | MER |
| –30.0 | 4.8 | 4.70E-03 | 0 | 30.0 | 1.50E-03 | 0 | 29.3 |
| –15.0 | 5.0 | 7.00E-03 | 0 | 29.3 | 4.30E-03 | 0 | 25.5 |
| –10.0 | 5.4 | 1.00E-02 | 0 | 27.9 | 9.00E-03 | 0 | 22.9 |
| –5.0 | 6.5 | 2.30E-02 | 0 | 25.2 | 2.30E-02 | 9.00E-07 | 20.3 |
| –3.0 | 7.5 | 3.10E-02 | 0 | 23.8 | 3.30E-02 | 1.20E-05 | 19.0 |

Second test

DVB-T2:

- CH 30
- 32k Not Extended
- 256 QAM
- SISO
- PP2
- Guard Interval: 1/16, 224 µs

- Code Rate: 2/3 – 34.5 Mbit/s

DVB-T:

- CH 30
- 64 QAM
- Guard Interval: 1/4, 224 µs
- Code Rate: 2/3 – 19.9 Mbit/s

SFN:

- Main signal 47 dBµV
- 2° signal: delay 8 µs, level –5 dB
- 3° signal: delay 57 µs, level –5 dB
- 4° signal: delay 148 µs, level –5 dB
- interferer: variable delay (outside GI), variable level:
 - 234 µs; –5 dB
 - 244 µs; –5 dB
 - 254 µs; –10 dB
 - 264 µs; –15 dB
 - 274 µs; –16 dB
 - 284 µs; –16 dB
 - 334 µs; –16 dB
 - 384 µs; –18 dB
 - 400 µs; –21.5 dB
 - 500 µs; –21.5 dB

| Interferer delay and level | DVB-T2 | | | DVB-T | | |
|-------------------------------|-----------------------|-------------------|------------------|----------|----------|-----------|
| | BER before LDPC | BER before BCH | MER PLP dB | bBER | aBER | MER dB |
| 234 µs; –5 dB | 2,30E-02 | 0,00E+00 | 25,1 | 2,30E-02 | 9,00E-07 | 20,3 |
| 244 µs; –5 dB | 3,00E-02 | 0,00E+00 | 22,3 | 5,70E-02 | 2,00E-03 | 17,2 |
| 254 µs; –10 dB | 2,30E-02 | 0,00E+00 | 25,5 | 6,10E-02 | 2,30E-03 | 16,8 |
| 264 µs; –15 dB | 1,30E-02 | 0,00E+00 | 27,4 | 5,40E-02 | 7,60E-04 | 17,2 |
| 274 µs; –16 dB | 1,30E-02 | 0,00E+00 | 27,7 | 7,10E-02 | 2,60E-03 | 16,4 |
| 284 µs; –16 dB | 1,30E-02 | 0,00E+00 | 27,0 | 8,70E-02 | 1,00E-02 | 15,7 |
| 334 µs; –16 dB | 2,00E-02 | 0,00E+00 | 25,6 | 8,60E-02 | 1,10E-02 | 15,8 |
| 384 µs; –18 dB | 9,40E-02 | 0,00E+00 | 13,1 | | | |
| 400 µs; –21,5 dB | 7,20E-02 | 0,00E+00 | 15,4 | | | |
| 500 µs; –21,5 dB | 8,40E-02 | 0,00E+00 | 14,0 | | | |

PART 2

Laboratory and field measurement results on DVB-T2 in France

1 Introduction

Following a consultation on the evolution of the terrestrial platform by the CSA end of 2017, France is currently considering a potential migration from DVB-T to DVB-T2 before the 2024 Olympic Games, the higher capacity provided by DVB-T2 enabling the broadcasting of UHD programmes.

Different technical subjects are being considered regarding this migration, among which the choice of DVB-T2 profiles to “seamlessly” replace the existing DVB-T profile in use for the national multiplexes: i.e. robustness and coverage should be maintained as they are currently so that the operation should not lead to a loss in viewers, while maintaining the existing network architecture and frequency plan in their current state (or at least to the state that they will be once the migration outside of the 700 MHz band is finalized, circa June 2019).

Currently, the DVB-T configuration used in France is 8K FFT, 64-QAM 3/4 with a 1/8 guard interval (112 µs). This configuration benefits from an 18.6 dB C/N for Ricean channel (fixed reception being the main target) and provide around 24.8 Mbits/s capacity.

Two DVB-T2 profiles have been identified on this basis, providing similar or equal robustness:

- “C1” profile: 32k FFT, extended bandwidth, 256-QAM 3/5 PP6 with a 1/32 guard interval.
The corresponding C/N for a Ricean channel is 18 dB, and the capacity is 34.9 Mbits/s
- “C’1” profile: 32k FFT, extended bandwidth, 256-QAM 3/5 PP4 with a 1/32 guard interval.
The corresponding C/N for a Ricean channel is 18.6 dB, and the capacity is 34.2 Mbits/s

As can be seen, the main difference between those two profiles lies in the choice of the pilot pattern, which may lead to a substantial behaviour difference when receiving the corresponding signals in a SFN configuration, which is common in the current network architecture. Despite the small difference in capacity between the two profiles, it might be useful for some broadcasters to be able to use the C1 profile, in a context where UHD is considered as a strong use case.

While PP4 DVB-T2 profiles are already in use in some European countries (Finland, Germany, Austria...) and feedback can be sought from those countries, PP6 DVB-T2 profiles do not seem to benefit from the same interest. In consequence it was decided to investigate further the difference between the two selected profiles at the French level.

Thus, investigations were lead both in laboratory and in the field, to have a better view of what the two profiles can provide.

2 Laboratory measurements

To check the in-lab behaviour of receivers with respect to the two selected DVB-T2 profiles, 15 receivers from different manufacturers were examined (10 TV sets – 4 from 2014, 6 from 2018 –, 4 Set-top-boxes and 1 USB key). While all receivers were DVB-T2 compatible, only a subset of them were HEVC compatible and yet a more reduced set UHD compatible. Since the focus of the measurements was on RF performances, those limitations have no practical impact on the results.

A first set of measurements was done to determine the basic behaviour of the receivers: sensitivity, robustness and noise figure in the case of Gaussian channel, Ricean channel, 0 dB echo channel (with echo inside guard interval, see below) and variable amplitude pre-echo inside the guard interval. For this last channel type, only robustness was measured.

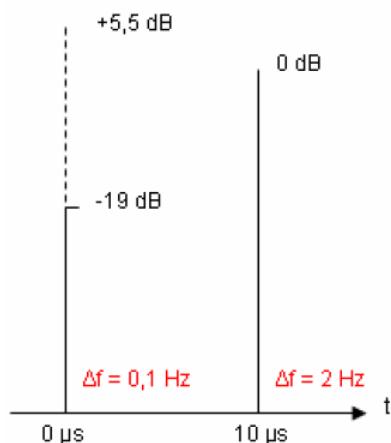
TABLE 1
0 dB echo configuration (based on Nordig requirements)

| | Delay | Att | Δf | Phase | Status |
|----------------------|---------|------|------------|-------|-----------|
| 1 st path | 0 µs | 0 dB | 0 Hz | 0° | Main path |
| 2 nd path | 1.95 µs | 0 dB | 0 Hz | 0° | 0 dB echo |

TABLE 2
Variable pre-echo configuration

| | Delay | Att | Δf | Status |
|----------------------|-------|-------|------------|-------------------|
| 1 st path | 0 µs | 0 dB | 0 Hz | Variable pre-echo |
| 2 nd path | 0 µs | -1 dB | 0.1 Hz | |
| 3 rd path | 10 µs | 0 dB | 2 Hz | Main path |

FIGURE 1
Channel impulse response for variable pre-echo configuration



The input level was set at -50 dBm for the robustness measurement. All measured parameters are determined based on a QEF situation (no picture impairment for at least 30 seconds), at 514 MHz (channel 26).

TABLE 3
Expected vs measured parameters (worst case) for C1 profile

| C1 DVB-T2 Profile (Bw = 8 MHz) 256-QAM, CR = 3/5, 32 k ext, LDPC = 64k, PP6, GI = 1/32 (112 µs) | | Channel | | | |
|--|--------------|-----------------|-------------|--------------------|---------------|
| | | Gaussian (ETSI) | Rice (ETSI) | 0 dB Echo (NorDig) | Variable echo |
| Sensitivity | C min | -81,4 dBm | -81,2 dBm | -77,1 dBm | - |
| Robustness | (C/N) Min | 17,8 dB | 18,0 dB | 22,1 dB | 25,1 dB |
| Measurements | C min | -81,8 dBm | -81,3 dBm | -78,7 dBm | |
| | (C/N) Min | 17,6 dB | 18,2 dB | 20,6 dB | 25,3 dB |
| | Noise figure | 6,1 dB | 6,0 dB | 6,1 dB | |

TABLE 4
Expected vs measured parameters (worst case) for C'1 profile

| C'1 DVB-T2 Profile (Bw = 8 MHz) 256-QAM, CR = 3/5, 32 k ext, LDPC = 64k, PP4, GI = 1/32 (112 µs) | | Channel | | | |
|---|--------------|-----------------|-------------|--------------------|---------------|
| | | Gaussian (ETSI) | Rice (ETSI) | 0 dB Echo (NorDig) | Variable echo |
| Sensitivity | C min | -80,8 dBm | -80,6 dBm | -76,6 dBm | - |
| Robustness | (C/N) Min | 18,4 dB | 18,6 dB | 22,6 dB | 25,6 dB |
| Measurements | C min | -81,8 dBm | -81,3 dBm | -78,7 dBm | |
| | (C/N) Min | 17,6 dB | 18,2 dB | 20,6 dB | 24,0 dB |
| | Noise figure | 6,1 dB | 6,0 dB | 6,2 dB | |

The two Tables above summarize the expected and measured values for each selected profile. Based on those basic measurements, no real difference can be drawn between the two profiles, except for the behaviour in the case of a variable pre-echo:

- Robustness and sensitivity are really close for the examined receivers for gaussian, ricean and 0 dB echo channels.
- Measurements for the C'1 profile exhibit better than expected values (between 0.5 and 1 dB) for gaussian and ricean channels.
- The case of 0 dB echo channel shows good behavior, bearing in mind that the examined situation represents only a part of the full Nordig expected behavior (2nd path echo delay should be varied between 1.95 µs and 95% of the guard interval duration).
- Variable echo results are a bit more specific
 - Setting aside 2014 TV receivers and one low-end set-top-box, the remaining TV receivers behave identically when switching from one profile to another, with a C/N close to 22.3 dB.
 - The situation is the same for 3 STB among the 4 and for the USB key.
 - It is assumed that the difference lies in the AGC part of the chipset, which adapts faster to the channel variation.
 - No clear conclusion can be drawn from those results, which are specific to some difficult receiving situations encountered in France in past DTT deployments.

The second set of measurements addressed the receivers' behaviour in SFNs with echoes outside of the guard interval, as the expectations were to have something similar or better to the existing DVB-T situation. The theoretical difference between C1 and C'1 profiles lie in the equalization interval duration, due to the difference in pilot patterns: equalization interval for the C1 profile is 133 µs while

it is 266 μs for the C'1 profile (considering a 57/64 ratio). For the current DVB-T French configuration, the equalization interval is 133 μs , meaning that the C1 profile should fulfil the requirements.

Two SFN profiles were used for the assessment of the receivers' behaviour:

- “Simple channel” profile: the profile is composed of two paths, one main path and one secondary path with variable delay (outside of the guard interval) / variable amplitude.

TABLE 5

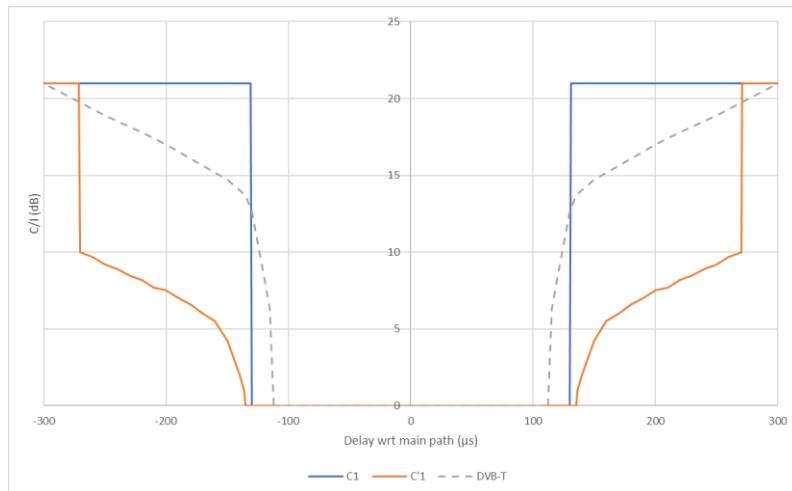
“Simple channel” impulse response for echo outside of the guard interval

| | Delay | Att | Δf | Phase | Status |
|----------------------|--|------------|------------------------------|--------------|---------------------------|
| 1 st path | 0 μs | 0 dB | 0 Hz | 0° | Main path |
| 2 nd path | Variable (-300 to -112, +112 to +300 μs) | Variable | 0 Hz | 0° | Echo outside of the GI |

The corresponding measurements are presented in Fig. 2: the C1/C'1 curves represent the “envelope” characterizing the set of considered receivers, while the DVB-T curve represents the modeled behavior for the selected French profile.

As can be seen, while theoretically equivalent to the DVB-T profile, the C1 profile presents a sharper transition between full constructive / full destructive contribution, and hence has a risk of inducing a loss in existing difficult DVB-T reception conditions. The C'1 profile on the contrary is more tolerant than the DVB-T profile when the echo is between 133-260 μs . Despite these differences, the behavior of the receivers is in line with the theoretically expected behavior for the corresponding DVB-T2 profile.

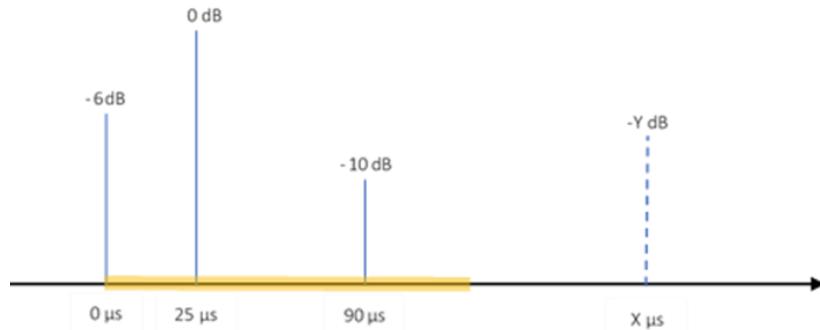
FIGURE 2
“Simple channel” measurement results



- “Complex channel” profile: this profile is inspired by the second SFN profile from § 4.2, adapted to the C1 / C'1 DVB-T2 profiles. It comprises 3 paths inside the guard interval with fixed delays / amplitude, and an additional path outside of the guard interval with variable delay and amplitude.

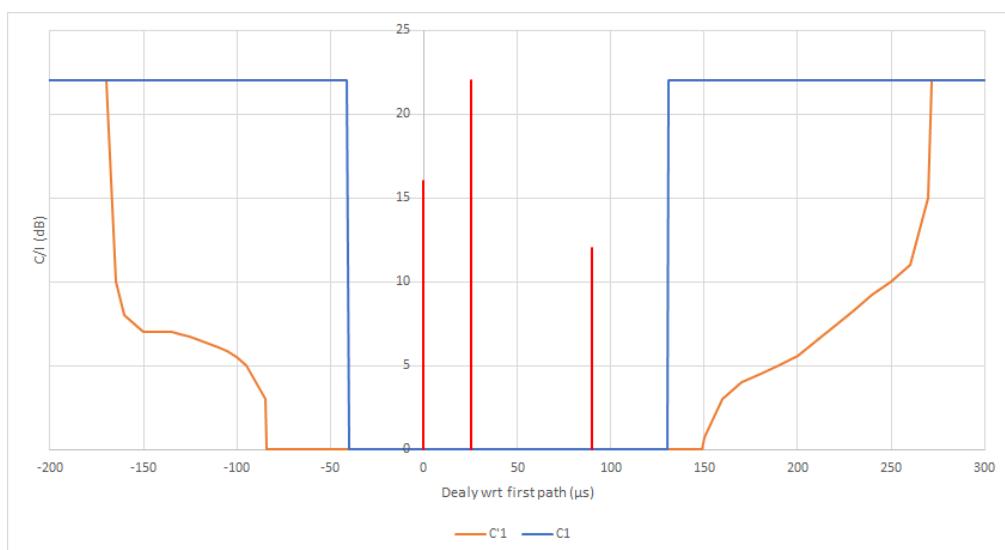
This channel profile has the advantage of forcing the receiver on a specific receiving window positioning, contrary to the simple profile, which may produce “strange” results (in some cases when presented with a simple profile, the behavior of the receiver may oscillate between good reception / no reception for a given delay / amplitude for the echo outside of the guard interval, because the synchronization algorithm is oscillating between two window positions).

FIGURE 3
“Complex channel” impulse response for echo outside of the guard interval



The corresponding measurements for the whole set of receivers are presented below, in the same way as for the simple channel profile case. For the C1 profile, we can note a correct equalization (fully constructive signals) when all signals lie in a $\sim 130 \mu\text{s}$ time span; for the C'1 profile, the equalization interval represents a $\sim 270 \mu\text{s}$ time span, with partially constructive / fully constructive signals depending on the echo timing. For this last profile, the behavior between pre-echo and post-echo is non symmetrical (at least for the envelope, in the case of individual receivers it might be variable, i.e. symmetrical or non-symmetrical behavior depending on the receiver).

FIGURE 4
“Complex channel” measurement results

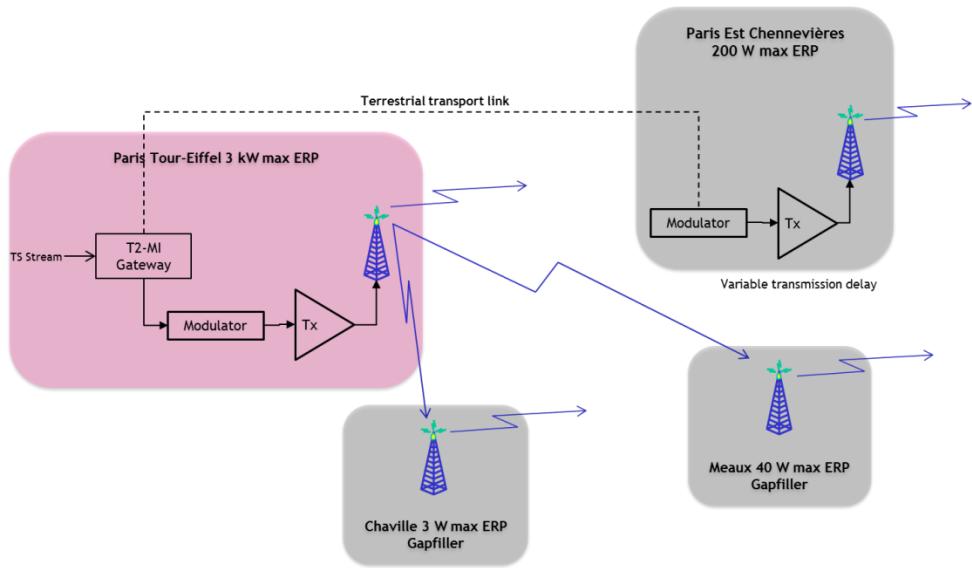


3 On field measurements

In parallel with the laboratory measurements, a field trial was set-up on the area of Paris to evaluate the real-life performance of the two selected DVB-T2 profiles. This field trial was built upon the existing DVB-T2 trial on the Eiffel Tower, partially copying existing network configurations from the national DVB-T multiplexes except for a reduced ERP on the involved sites, with the following objectives:

- Expand the existing coverage and set-up an SFN network for the trial, through the increased ERP on the Eiffel Tower and deployment of three additional sites (one transmitter, two repeaters)
- Experiment with on-channel repeaters for DVB-T2 (in the context of an adjacent existing DVB-T channel, ~13 dB above in ERP)
- Experiment with T2-MI signal transport (terrestrial link)
- Set-up a flexible configuration for real-life measurements, allowing live modifications of transmitters delay emulating various SFN situations from one network configuration, and live modifications of DVB-T2 profile to allow for the evaluation of the two profiles in the same conditions.

FIGURE 5
SFN experiment set-up in the Paris area



Following an agreement by the CSA (French regulation authority), the network has been operational since early May 2018. The increase in ERP on the Eiffel Tower has proven necessary for the correct on-channel repetition of the signal on the Meaux gap filler (increasing the output MER from a fairly low 24 dB value to an acceptable 32 dB value).

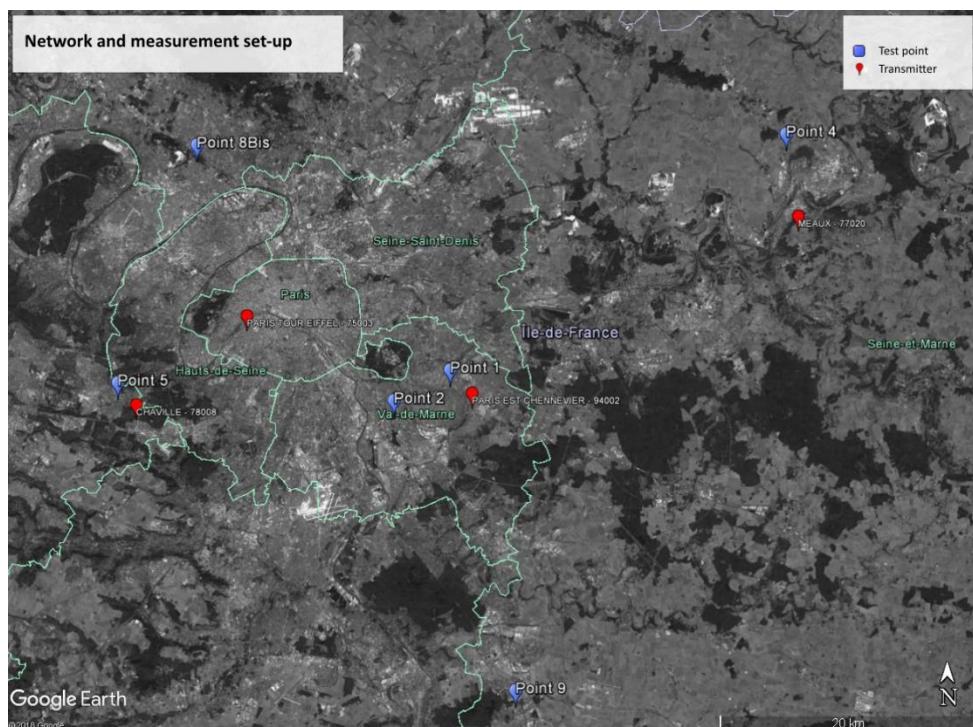
Based on this network set-up, several test points were defined to try and characterize the receiving conditions and have a global view of the situation near each of the transmitter / repeater. On each test-point, the following actions were taken, once the correct receiving location/orientation was set:

- 1 Set-up profile / delay configuration
- 2 Qualitative measurements (professional test equipment + monitoring test equipment): MER, channel impulse response, before BCH error-rate, after BCH error-rate, number of LDPC iterations, spectrum analysis, demodulated constellation...
- 3 I/Q recording for further in-lab playback

- 4 Quantitative measurements: assessment of reception on a dedicated TV-set, reception margin (using an adjustable attenuator, determine the level at QEF reception failure)
- 5 Go-back to step 2 until all configurations are measured for the current test-point

Since the field-trial was limited in time (one week) and due to the large amount of measurements on each test point, the initial set of 10 test-points (representing virtually 60 different receiving conditions when varying the DVB-T2 profiles and the Chennevières transmitter delay) was in the end limited to six test-points (see Figure below). Despite this limitation, all the expected representative delays / profiles configurations have been covered in the timeframe.

FIGURE 6
Location of transmitters / test points



Tables 6 and 7 illustrate the situation for test-point 4, showing the six different configurations examined (three different delays on Chennevières for two different DVB-T2 profiles), noting that:

- The presence of echoes outside the guard interval may decrease significantly the measured MER, while still allowing the good reception of the signal in some cases.
- A bad MER value may still allow to benefit from a good reception margin on the signal level in some cases.

TABLE 6

Channel impulse response for 3 different delay configurations on the Chennevières transmitter

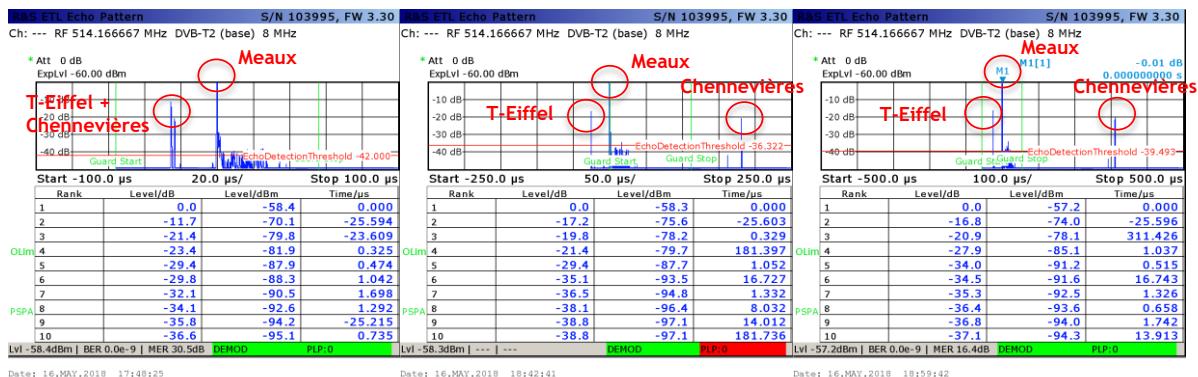


TABLE 7

Corresponding measurements for the 3 delay configurations / 2 DVB-T2 profiles

| Configuration | Measurement | C1 Profile | C'1 Profile |
|---------------------------------|------------------|---------------------------------|----------------|
| All echoes within GI | Reception level | -54.7 dBm | -53.4 dBm |
| | MER | 29.3 – 30.2 dB | 30.9 – 31.1 dB |
| | Reception margin | 26 dB | 29 dB |
| One echo outside of GI (181 μs) | Reception level | -53.8 dBm | -53.2 dBm |
| | MER | 20.7 – 21 dB | 19.6 – 19.8 dB |
| | Reception margin | 22.9 dB | 29 dB |
| One echo outside GI (311 μs) | Reception level | -53.4 dBm | -53.0 dBm |
| | MER | 16.7 dB | 17.5 dB |
| | Reception margin | No margin (difficult reception) | 19 dB |

Considering the various test-points, the conclusions of the real-life measurements are in line with lab measurements:

- In the case of nominal SFN reception (optimal delay on Chennevières transmitter)
 - No distinction is possible between the two profiles, based on the receiver behaviour
 - The reception margin is similar between the two profiles on the six test-points
- In the case of a degraded SFN reception (Chennevières transmitter delay artificially changed to have at least one echo outside of the guard interval)
 - If the main path level is significantly above the level of the echo outside of the guard interval ($C/I >> 21$ dB, test-points 5 & 8Bis)
 - The receiver behaviour does not depend on the position of the echo outside of the guard interval (271, 281, 401 and 411 μs).
 - The reception margin is identical between the two DVB-T2 profiles, despite a significant loss in MER for some configurations.

- With echoes outside the guard interval having a level close to the interference threshold ($C/I \sim > 21$ dB)
 - With 190 and 320 μ s echoes, good reception is possible.
 - With a 190 μ s echo, the reception margin for C1 profile is degraded (~5 dB) while the reception margin for C'1 profile remains stable.
 - With a 320 μ s echo, the reception margin is degraded identically for both DVB-T2 profiles.
- With echoes above the interference threshold ($C/I < 21$ dB between main path and echo out of the guard interval, points 2 and 4)
 - The C'1 profile allows the good reception in most configurations (-200, 153, 283 μ s echoes). The case of a -330 μ s echo leads to no reception at all.
 - The C1 profile only allows a good reception for a 153 μ s echo. All other echo configurations (-330, -200, 283 μ s) lead to difficult or no reception.

Annex 1 to Part 2

Professional vs monitoring DVB-T2 test equipment comparison

During the field trial, there was the opportunity to use two different DVB-T2 test equipment from well-known manufacturers: one professional test equipment and one monitoring test equipment. Both are bound to be used for field tests. The professional test equipment is supposedly superior in terms of performances and remained the reference for all the measurements we conducted but as can be seen below, the monitoring test equipment offers a fair view of the situation, despite not completely identical to what the professional test equipment provides.

The following Tables show the comparison of the two equipment for measuring/controlling DVB-T2 signals (all measurements were done using the DVB-T2 C1 profile; no substantial differences were observed using the C'1 profile).

TABLE A1.1

Professional vs Monitoring test equipment performances for different input levels (no noise added)

| Input Level | Professional test equipment | | | | | Monitoring test equipment | | | | | | |
|-------------|-----------------------------|------|----------|----------|-----------|---------------------------|-------|------|----------|----------|-----------|----------|
| | Level | MER | #LDPC It | Pre LDPC | Post LDPC | Post BCH | Level | MER | #LDPC It | Pre LDPC | Post LDPC | Post BCH |
| -50 | -50,2 | 40,9 | 1,3 | 3,40E-06 | 0 | 0 | -51,5 | 39,2 | 1 | 3,60E-05 | 0 | 0 |
| -55 | -55,2 | 38,7 | 1,3 | 3,60E-06 | 0 | 0 | -56,3 | 39,2 | 1 | 3,80E-05 | 0 | 0 |
| -60 | -60,2 | 35,2 | 1,3 | 4,00E-06 | 0 | 0 | -60,6 | 38,7 | 1 | 3,10E-05 | 0 | 0 |
| -65 | -65,1 | 30,9 | 2,2 | 4,90E-05 | 0 | 0 | -66,6 | 34,6 | 2 | 4,90E-05 | 0 | 0 |
| -70 | -70,2 | 26 | 4,4 | 6,90E-03 | 0 | 0 | -70,7 | 28,8 | 2 | 1,40E-03 | 0 | 0 |
| -75 | -75,2 | 20,9 | 14,7 | 5,10E-02 | 0 | 0 | -75,7 | 23,5 | 4 | 2,20E-02 | 0 | 0 |
| -78 | -78,2 | 18,2 | 31,8 | 9,20E-02 | 0 | 0 | -78,9 | 20,6 | 9 | 5,00E-02 | 0 | 0 |
| -79 | -79,2 | 17,6 | 36,2 | 1,00E-01 | 3,10E-07 | 1,00E-05 | -79,7 | 19,7 | 13 | 6,20E-02 | 0 | 0 |
| -80 | -80,2 | - | - | - | - | - | -80,4 | 18,7 | 17 | 7,40E-02 | 0 | 0 |
| -81 | -81,2 | - | - | - | - | - | -81,2 | 17,7 | 25 | 8,70E-02 | 1,00E-07 | 0 |
| -82 | -82,2 | - | - | - | - | - | -82,5 | 16,6 | 36 | 1,00E-01 | 5,00E-07 | 0 |
| -83 | -83,2 | - | - | - | - | - | -83,2 | 15 | 40 | - | - | - |

The comparison between the two apparatus is quite difficult as MER values differ significantly even for comfortable input level values. Close to the sensitivity level of the equipment, the MER value

degrades very fast. The monitoring equipment has an edge in terms of sensitivity level but is slower when doing the measurements and/or to follow a change in the input signal characteristics.

TABLE A1.2

Professional vs Monitoring test equipment performances for different C/N values (input level @ -50 dBm)

| C/N | Professional test equipment | | | | | | Monitoring test equipment | | | | | |
|------|-----------------------------|------|----------|----------|-----------|----------|---------------------------|------|----------|----------|-----------|----------|
| | Level | MER | #LDPC It | Pre LDPC | Post LDPC | Post BCH | Level | MER | #LDPC It | Pre LDPC | Post LDPC | Post BCH |
| 30 | -50,5 | 29,2 | 2,8 | 4,0E-04 | 0 | 0 | -51,5 | 29,1 | 1 | 1,0E-03 | 0 | 0 |
| 29 | -50,5 | 28,3 | 3,1 | 1,1E-03 | 0 | 0 | -51,5 | 28,1 | 2 | 2,2E-03 | 0 | 0 |
| 28 | -50,5 | 27,3 | 3,5 | 2,7E-03 | 0 | 0 | -51,5 | 27,1 | 2 | 4,3E-03 | 0 | 0 |
| 27 | -50,5 | 26,3 | 4,2 | 5,6E-03 | 0 | 0 | -51,5 | 26 | 2 | 7,5E-03 | 0 | 0 |
| 26 | -50,5 | 25,3 | 6,4 | 1,0E-02 | 0 | 0 | -51,5 | 25 | 3 | 1,2E-02 | 0 | 0 |
| 25 | -50,2 | 24,4 | 7,6 | 1,7E-02 | 0 | 0 | -51,4 | 23,9 | 4 | 1,9E-02 | 0 | 0 |
| 24 | -50,2 | 23,4 | 9,3 | 2,5E-02 | 0 | 0 | -51,4 | 22,9 | 4 | 2,7E-02 | 0 | 0 |
| 23 | -50,2 | 22,3 | 11,2 | 3,5E-02 | 0 | 0 | -51,4 | 21,9 | 6 | 3,7E-02 | 0 | 0 |
| 22 | -50,2 | 21,3 | 13,8 | 4,7E-02 | 0 | 0 | -51,4 | 21 | 11 | 4,8E-02 | 0 | 0 |
| 21 | -50,2 | 20,2 | 17 | 5,9E-02 | 0 | 0 | -51,4 | 20 | 12 | 6,0E-02 | 0 | 0 |
| 20 | -50,2 | 19,3 | 21,5 | 7,2E-02 | 0 | 0 | -51,4 | 18,9 | 15 | 7,4E-02 | 0 | 0 |
| 19 | -50,2 | 18,5 | 28,3 | 8,6E-02 | 0 | 0 | -51,4 | 17,8 | 23 | 8,6E-02 | 0 | 0 |
| 18 | -50,2 | 17,9 | 35,8 | 1,0E-01 | 0 | 0 | -51,4 | 16,8 | 37 | 1,0E-01 | 2,0E-07 | 0 |
| 17,5 | -50,1 | 17,5 | 36,3 | 1,1E-01 | 2,9E-06 | 3,9E-04 | -51,4 | 16,3 | 40 | 1,1E-01 | 1,4E-05 | 1,2E-02 |
| 17,3 | -50,1 | 17,4 | 36,4 | 1,1E-01 | 2,0E-04 | 1,7E-01 | -51,4 | 15,9 | 40 | - | - | - |
| 17 | -50,2 | 17,2 | 36,5 | - | - | - | -51,4 | 15,5 | 40 | - | - | - |

For sufficiently high C/N values (> 20/21 dB), the two equipment offer similar readings in terms of MER, and bit error rates; the number of LDPC iterations is somewhat more an indication of the situation than a usable metric. They start diverging when the C/N values come close to the specific C/N threshold for the DVB-T2 C1 profile.

FIGURE A1.1
MER vs C/N for tested equipment

