

Report ITU-R BS.2214-2 (10/2016)

# Planning parameters for terrestrial digital sound broadcasting systems in VHF bands

BS Series
Broadcasting service (sound)



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#### REPORT ITU-R BS.2214-2

## Planning parameters for terrestrial digital sound broadcasting systems in VHF bands

(2011-2015-2016)

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#### 1 Introduction

This Report provides planning parameters for digital terrestrial broadcasting systems G (also known as DRM+) and RAVIS in VHF Bands. DRM+ is designed for use in VHF Bands I, II and III, RAVIS is designed for use in VHF Bands I and II.

The report defines a framework for calculating all relevant network planning parameters that are very similar for both systems.

The system characteristics of digital System G are included in Recommendation ITU-R BS.1114 and the description of RAVIS is contained in Report ITU-R BT.2049.

Framework for evaluation of planning parameters is given in Parts 2 to 5.

Part 6 gives planning parameter for DRM+.

Part 7 gives planning parameter for RAVIS.

Normative and technical references are given in Attachments 1 and 2 respectively.

To calculate the relevant planning parameters minimum median field strength and protection ratios, firstly receiver and transmitter characteristics, system parameters as well as transmission aspects as common basis for concrete digital broadcasting transmission network planning are determined. All parameters are either derived or the reference to the source of origin is given. Various typical reception scenarios are taken into account to match as much as possible planning and prediction scenarios.

#### **2** Reception modes

#### 2.1 Fixed reception

Fixed reception (FX) is defined as reception where a receiving antenna mounted at roof level is used. It is assumed that near-optimal reception conditions (within a relatively small volume on the roof) are found when the antenna is installed. In calculating the field-strength levels for fixed antenna reception, a receiving antenna height of 10 m above ground level is considered to be representative for the broadcasting service [1].

A location probability of 70% is assumed to obtain a good reception situation.

#### 2.2 Portable reception

In general, portable reception means a reception where a portable receiver with an attached or built-in antenna is used outdoors or indoors at no less than 1.5 m above ground level.

A location probability of 95% is assumed to obtain a good reception situation.

Two receiving locations will be distinguished:

- Indoor reception with a reception place in a building.
- Outdoor reception with a reception place outside a building.

Within these receiving locations two opposed receiving conditions will be distinguished additionally due to the great variability of portable reception situations with different receiver-/antenna-types and also different reception conditions:

- Portable reception: This situation models the reception situation with good reception conditions for both situations indoor and outdoor, resp., and a receiver with an omnidirectional VHF antenna pattern as given in GE06 [1].
- Portable handheld reception: This situation models the reception situation with bad reception conditions and a receiver with an external antenna (for example telescopic antennas or the cable of wired headsets) as given in EBU-3317 [2].

#### 2.2.1 Portable indoor reception

Portable indoor (PI) reception is defined by a portable receiver with stationary power supply and a built-in (folded)-antenna or with a plug for an external antenna. The receiver is used indoors at no less than 1.5 m above floor level in rooms on the ground floor and with a window in an external wall. It is assumed that optimal receiving conditions will be found by moving the antenna up to 0.5 m in any direction and the portable receiver is not moved during reception and large objects near the receiver are also not moved [1]. A suburban area is assumed.

#### 2.2.2 Portable outdoor reception

Portable outdoor (PO) reception is defined as reception by a portable receiver with battery supply and an attached or built-in antenna which is used outdoors at no less than 1.5 m above ground level [1]. A suburban area is assumed in this case.

#### 2.2.3 Portable handheld reception (PI-H, PO-H)

Portable reception is defined as reception by a portable handheld receiver with battery supply and an external antenna as given in EBU-3317 [2] for both reception situations indoor and outdoor, respectively. An urban area is assumed in this case.

#### 2.3 Mobile reception

Mobile reception (MO) is defined as reception by a receiver in motion also at high speed with a matched antenna situated at no less than 1.5 m above ground level or floor level [1]. A rural area with hilly terrain is assumed in this case.

#### 3 Correction factors for field-strength predictions

Recommendation ITU-R P.1546 forms the basis of a field-strength prediction method applicable for the broadcasting services amongst other services. Predictions can be made from 30 MHz up to 3 000 MHz within a path distance of 1 to 1 000 km, percentage of time of 1 to 50%, and for various

transmitting antenna heights. The method draws a distinction between paths over land, cold seas and warm seas, makes due allowance for location variability for land area-service predictions and takes account of local clutter surrounding the receiving location. It also provides procedures for handling negative effective transmitting antenna heights and mixed-path propagation (i.e. with combinations of land and sea).

The wanted field-strength level values predicted (see Recommendation ITU-R P.1546) refer always to the median value at a receiving location with a receiving antenna in 10 m height above ground level. This antenna height is a generic value, used as stated only in rural or suburban areas, with constructions or vegetation below 10 m height. Otherwise the wanted field-strength values are predicted at the average construction or vegetation height at the receiving location. The true receiving antenna height influences the height loss correction factor (see § 3.4).

To take into account different receiving modes and circumstances into network planning correction factors have to be included to carry the minimum receiver input power level or the minimum field-strength level over to the median minimum field-strength level for predictions (see Recommendation ITU-R P.1546).

#### 3.1 Reference frequencies

The planning parameters and correction factors in this document are calculated for the reference frequencies given in Table 1.

TABLE 1
Reference frequencies for calculations

VHF band	I	II	III
(frequency range)	(47-68 MHz)	(87.5-108 MHz)	(174-230 MHz)
Reference frequency (MHz)	65	100	200

#### 3.2 Antenna gain

The antenna gain  $G_D$  (dBd) references to a half-wave dipole.

#### 3.2.1 Antenna gain for fixed reception

In Recommendation ITU-R BS.599 and GE06 [1], the antenna pattern for fixed reception are given for both VHF Band II (4 dB) and VHF Band III (7 dB). In ETSI-DVB [3] the antenna pattern for fixed reception is given for VHF Band I (3 dB).

Taking into account the current use of roof-top antenna systems with omnidirectional dipole antennas or ground plane antennas for future planning it is recommended that an omnidirectional antenna pattern with a gain of 0 dBd is used (see Table 2).

TABLE 2 Antenna gain  $G_D$  for fixed reception

Frequency (MHz)	65	100	200
Antenna gain $G_D(dBd)$	0	0	0

#### 3.2.2 Antenna gain for portable reception

GE06 [1] assumes an omnidirectional VHF antenna pattern with an antenna gain of -2.2 dBd for standard portable receiver planning, e.g. for DAB reception. From this reference, the antenna gains  $G_D$  for portable reception are assumed to -2.2 dBd as given in Table 3.

TABLE 3 Antenna gain  $G_D$  for portable reception

Frequency (MHz)	65	100	200
Antenna gain $G_D$ (dBd)	-2.2	-2.2	-2.2

#### 3.2.3 Antenna gain for portable handheld reception

Antenna gains  $G_D$  for portable handheld reception in VHF Band III (200 MHz) are given by EBU-3317[2]:

- Receiver integrated antenna:  $G_D = -17 \text{ dBd}$ - External antenna (telescopic or wired headsets):  $G_D = -13 \text{ dBd}$ - Adapted antenna (for mobile reception):  $G_D = -2.2 \text{ dBd}$ 

The antenna gain for portable handheld reception in VHF Band I and VHF Band II can be calculate by the computation given in Annex 2, section 0 [4]. From it the antenna gains  $G_D$  (dB) for portable handheld reception modes with an external antenna are given in Table 4.

TABLE 4 Antenna gains  $G_D$  for portable handheld reception

Frequency (MHz)	65	100	200
Gain variation $\Delta G$ referenced to 200 MHz (dB)	-9.76	-6.02	0.00
Antenna gain $G_D$ for receiver integrated antenna (dBd)	-26.76	-23.02	-17.00
Antenna gain $G_D$ for portable handheld reception (external antenna, telescopic or wired headsets) (dBd)	-22.76	-19.02	-13.00

#### 3.2.4 Antenna gain for mobile reception

For mobile reception an omnidirectional VHF antenna pattern with an antenna gain  $G_D$  of  $-2.2 \, \text{dBd}$  [1] is assumed, see Table 5.

TABLE 5 Antenna gains  $G_D$  for mobile reception

Frequency (MHz)	65	100	200
Antenna gain $G_D$ for adapted antenna (mobile reception) (dBd)	-2.2	-2.2	-2.2

#### 3.3 Feeder loss

The feeder loss  $L_f$  expresses the signal attenuation from the receiving antenna to the receiver's RF input. The feeder loss  $L_f$  for fixed reception at 200 MHz is given in GE06 [1] with 2 dB for 10 m cable length. The frequency dependent cable attenuation per unit length  $L_f$  is assumed to be equal to:

$$L_f'\left(dB/m\right) = \frac{2}{10} \sqrt{\frac{f\left(MHz\right)}{200}} \tag{1}$$

with f the frequency (MHz). The feeder loss values per unit length  $L'_f$  are given in Table 6.

TABLE 6 Feeder loss  $L'_f$  per unit length

Frequency (MHz)	65	100	200
Feeder loss $L'_f(dB/m)$	0.11	0.14	0.2

The feeder loss  $L_f$  is given by:

$$L_f \text{ (dB)} = L'_f l = \frac{2}{10} \sqrt{\frac{f(\text{MHz})}{200}} l$$
 (m)

with *l* the length of the feeder cable (m).

The cable length l for the different reception modes are given in Table 7, and the feeder losses  $L_f$  for different frequencies and reception modes are given in Table 8.

TABLE 7 Cable length  $\boldsymbol{l}$  for reception modes

Reception mode	Fixed reception (FX)	Portable reception (PO, PI, PO-H, PI-H)	Mobile reception (MO)
Cable length $l$ (m)	10	0	2

TABLE 8 Feeder loss  $L_f$  for different reception modes

Frequency (MHz	65	100	200	
Feeder loss $L_f$	$s L_f$ for fixed reception (FX) (dB)		1.4	2.0
	for portable reception (PO, PI, PO-H, PI-H) (dB)	0.0	0.0	0.0
	for mobile reception (MO) (dB)	0.22	0.28	0.4

#### 3.4 Height loss correction factor

For portable reception a receiving antenna height of 1.5 m above ground level (outdoor and mobile) or above floor level (indoor) is assumed. The propagation prediction method usually provides

field-strength values at 10 m. To correct the predicted value from 10 m to 1.5 m above ground level a height loss factor  $L_h$  (dB) has to be applied.

The height loss correction factor  $L_h$  for an antenna height of 1.5 m is given in GE06 [1] as follows:

 $L_h = 12 \text{ dB at } 200 \text{ MHz}$ 

 $L_h = 16 \text{ dB}$  at 500 MHz

 $L_h = 18 \text{ dB at } 800 \text{ MHz}$ 

Therefore, the height loss correction factor  $L_h$  (dB) at 100 MHz is assumed to 10 dB, and at 65 MHz to 8 dB, for portable and mobile reception modes The height loss correction factor  $L_h$  for handheld reception with external antenna is given in EBU-3317 [2] for VHF Band III as 19 dB in urban areas and is assumed to 17 dB at 100 MHz and to 15 dB at 65 MHz.

The height loss correction factor  $L_h$  for different reception modes is given in Table 9.

TABLE 9

Height loss correction factor  $L_h$  for different reception modes

Frequency (MHz)		65	100	200
Height loss	for fixed reception (FX) (dB)	0	0	0
correction factor	for portable and mobile reception (PO, PI, MO) (dB)	8	10	12
$L_h$	for portable handheld reception (PO-H, PI-H) (dB)	15	17	19

#### 3.5 Building penetration loss

The ratio between the mean field strength inside a building at a given height above ground level and the mean field strength outside the same building at the same height above ground level expressed in (dB) is the mean building penetration loss.

The mean building penetration loss  $L_b$  in VHF Band III is given in GE06 [1] and EBU-3317 [2] as 9 dB which is proposed to be used for VHF Band II, too. The mean building penetration loss for VHF Band I is given in ETSI-DVB [3] as 8 dB. The standard deviation of the building penetration loss  $\sigma_b$  is always given by 3 dB.

The mean building penetration losses  $L_b$  and standard deviations  $\sigma_b$  are given in Table 10.

TABLE 10 Building penetration loss  $L_b$  and standard deviation  $\sigma_b$ 

Frequency (MHz)	65	100	200
Mean building penetration loss $L_b(dB)$	8	9	9
Standard deviation of the building penetration loss $\sigma_b$ (dB)	3	3	3

#### 3.6 Allowance for man-made noise

The allowance for man-made noise (MMN) (dB), takes into account the effect of the MMN received by the antenna on the system performance. The system equivalent noise figure  $F_s$  (dB) to be used for coverage calculations is calculated from the receiver noise figure  $F_r$  (dB) and MMN (dB) (for details see Attachment 2, § 2.2):

$$F_s (dB) = F_r + MMN$$
 (dB)

The allowance for man-made noise is calculated from an antenna noise factor  $f_a$ , which takes into account the man-made noise received by the antenna:

$$MMN ext{ (dB)} = 10 \log_{10} \left( 1 + \frac{f_a - 1}{f_r} \right)$$
 (dB)

where:

 $f_r$ : the receiver noise factor:

$$f_r = 10^{\frac{F_r}{10}} \tag{5}$$

 $f_a$ : the antenna noise factor:

$$f_a = 10^{\frac{F_a}{10}} \tag{6}$$

where:

 $F_a$ : the antenna noise figure.

#### 3.6.1 Allowance for man-made noise for fixed, portable and mobile reception

Recommendation ITU-R P.372 gives the legal values to calculate the allowance of man-man noise in different areas and frequencies with the definitions of the antenna noise figure, its mean values  $F_{a,med}$  and the values of decile variations (10% and 90%) measured in different regions as a function of the frequency. The equation to calculate the antenna noise figure is given in Recommendation ITU-R P.372 by:

$$F_{a,med} (dB) = c - d \cdot \log_{10}(f (MHz) (dB)$$
(7)

For all reception modes the residential area (Curve B in Recommendation ITU-R P.372) is assumed. In this case the values for the variables c and d are given by:

$$c = 72.5$$
  $d = 27.7$ 

Herewith the values of the medium antenna noise figure  $F_{a,med}$  (dB) can be computed. The results are shown in Table 11.

TABLE 11 Medium antenna noise figure  $F_{a,med}$ 

Frequency (MHz)	65	100	200
Medium antenna noise figure $F_{a,med}$ for residential area (curve B) (dB)	22.28	17.10	8.76

Herewith the MMN (dB), taking into account a receiver noise figure  $F_r$  of 7 dB, can be computed. The results are shown in Table 12.

TABLE 12
Allowance for man-made noise (MMN) for fixed, portable and mobile reception

Frequency (MHz)	65	100	200
Allowance for man-made noise for fixed, portable and mobile reception ( $F_r = 7 \text{ dB}$ ) (dB)	15.38	10.43	3.62

Recommendation ITU-R P.372 gives the value of decile location variations (10% and 90%) in residential area by 5.8 dB. For 90% location probability the distribution factor  $\mu = 1.28$ . Therefore the standard deviation of MMN for fixed, portable and mobile reception  $\sigma_{MMN} = 4.53$  dB, see Table 13.

TABLE 13 Standard deviation of MMN  $\sigma_{MMN}$  for fixed, portable and mobile reception

Frequency (MHz)	65	100	200
Standard deviation of MMN $\sigma_{MMN}(dB)$	4.53	4.53	4.53

The standard deviation of MMN has to be considered in the calculation of the combined standard deviation for the wanted field-strength level (see § 3.8.2).

#### 3.6.2 Allowance for man-made noise for portable handheld reception

The antenna gain is the product of directivity and efficiency. The lowest realistic directivity is the one of a short dipole (length  $l << \lambda$ ) and it has the value 1.5 (1.8 dBi). Any gain lower than 1.8 dBi (-0.4 dBd) is due to an antenna efficiency  $\eta$  lower than 1. The interference power at the receiver input is reduced accordingly and the MMN equation is (see Attachment 2, § 2.2):

$$MMN(dB) = 10 \log_{10} \left( 1 + \eta \frac{f_a - 1}{f_r} \right)$$
 (dB)

The efficiency  $\eta$  can be calculated from the antenna gain  $G_D$  (dB) for gains lower than -0.4 dBd:

$$\eta = 10^{\frac{G_D + 0.4}{10}} \tag{9}$$

The MMN for portable handheld reception, taking the receiver noise figure as 7 dB, are given in Table 14.

TABLE 14
Allowance for man-made noise for portable handheld reception (external antenna)

Frequency (MHz)	65	100	200
Handheld antenna gain $G_D(dBd)$	-22.8	-19	-13
Efficiency η	0.0058	0.0138	0.055
Calculated MMN allowance (dB)	0.42	0.30	0.14
Allowance for man-made noise for portable handheld reception (dB)	0.0	0.0	0.0

In the further calculations the allowance for man-made noise is specified to 0 dB due to the very low calculated values.

#### 3.7 Implementation loss factor

Implementation loss of the non-ideal receiver is considered in the calculation of the minimum receiver input power level with an additional implementation loss factor  $L_i$  of 3 dB, see Table 15.

TABLE 15 Implementation loss factor  $L_i$ 

Frequency (MHz)	65	100	200
Implementation loss factor $L_i(dB)$	3	3	3

#### 3.8 Correction factors for location variability

The random variation of the received signal field strength with location due to terrain irregularities and the effect of obstacles in the near vicinity of the receiver location is modelled by a statistical distribution (typically log normal) over a specified macro-scale area (typically a square with edge lengths of 100 m to 500 m). Considering the received signal field-strength level E (dB( $\mu$ V/m)), the lognormal distribution is transformed in a Gaussian distribution with mean (and median)  $E_{med}$  (dB) and standard deviation  $\sigma$  (dB).

The field-strength level E(p) (dB( $\mu$ V/m)), used for coverage and interference predictions in the different reception modes, which will be exceeded for p (%) of locations for a land receiving/mobile antenna location, is given by:

$$E(p)\left(dB(\mu V/m)\right) = E_{med}\left(dB(\mu V/m)\right) + C_1(p)\left(dB\right) \quad \text{for } 50\% \le p \le 99\%$$
(10)

with:

 $C_1(p)$  (dB): location correction factor;

 $E_{med}$  (dB( $\mu$ V/m): field-strength value for 50% of locations and 50% of time.

The location correction factor  $C_1(p)$  (dB) depends on the so called combined standard deviation  $\sigma_c$  (dB) of the wanted field-strength level that sums the single standard deviations of all relevant signal parts that have to be taken into account and the so-called distribution factor  $\mu(p)$ , namely:

$$C_1(p)(dB) = \mu(p) \cdot \sigma_C \qquad (dB)$$

with:

$$\mu(p) = \phi^{-1}\left(\frac{p}{100}\right)$$
: the distribution factor and  $\phi(x) = \int_{-\infty}^{x} \frac{1}{\sqrt{2\pi}} e^{-\frac{z^2}{2}} dz$  (standard normal Gaussian CDF)

 $\sigma_C$ : the combined standard deviation of the wanted field-strength level (dB).

#### 3.8.1 Distribution factor

The distribution factors  $\mu(p)$  of the different location probabilities taking into account the different receiving modes (see § 2) are given in Table 16.

TABLE 16

Distribution factor μ

Percentage of receiving locations $p$ (%)	70	95	99
Reception mode	fixed	portable	mobile
Distribution factor μ	0.524	1.645	2.326

#### 3.8.2 Combined standard deviation

The combined standard deviation  $\sigma_c$  (dB) takes into account the standard deviation of the wanted field-strength level  $\sigma_m$  (dB), the standard deviation of the MMN  $\sigma_{MMN}$  (dB), and, in the case of indoor reception, the standard deviation of the building penetration loss,  $\sigma_b$  (dB), respectively.

Since the statistics of the received wanted field-strength level for macro-scale, the statistics of the MMN  $\sigma_{MMN}$  (dB), and the statistics of the building attenuation can be assumed to be statistically uncorrelated, the combined standard deviation  $\sigma_c$  (dB) is calculated by:

$$\sigma_c (dB) = \sqrt{\sigma_m^2 + \sigma_b^2 + \sigma_{MMN}^2}$$
 (12)

The values of the standard deviations of the building penetration loss  $\sigma_b$  (dB) and of the MMN  $\sigma_{MMN}$  (dB) are given in §§ 3.5 and 3.6, respectively.

The values of standard deviation  $\sigma_m$  (dB) of the wanted field-strength level E are dependent on frequency and environment, and empirical studies have shown a considerable spread. Representative values for areas of 500 m × 500 m are given by Recommendation ITU-R P.1546 as well as the expression to calculate the standard deviation  $\sigma_m$  (dB):

$$\sigma_m(dB) = K(dB) + 1.3\log_{10}(f(MHz)) \tag{13}$$

where:

K= 1.2, for receivers with antennas below clutter height in urban or suburban environments for mobile systems with omnidirectional antennas at car-roof height

K=1.0, for receivers with rooftop antennas near the clutter height

K = 0.5, for receivers in rural areas

f: required frequency (MHz).

Furthermore, the following fixed values are given:

 $\sigma_m = 8.3 \text{ dB}$  for broadcasting, analogue at 100 MHz (i.e. FM)

 $\sigma_m = 5.5 \text{ dB}$  for broadcasting, digital (more than 1 MHz bandwidth, i.e. DAB)

The standard deviations  $\sigma_m$  (dB) for FM and DAB are given in Table 17 whereas those for DRM and RAVIS in urban and suburban areas as well as in rural areas are given in Table 18.

TABLE 17 Standard deviation for DAB  $\sigma_{m,DAB}$  and FM  $\sigma_{m,FM}$ 

Frequency (MHz)		65	100	200
Standard deviation	for FM $\sigma_{m,FM}(dB)$	_	8.3	_
	for DAB $\sigma_{m,DAB}$ (dB)	_	_	5.5

TABLE 18 Standard deviation for DRM and RAVIS  $\sigma_m$ 

Frequency (MHz)		65	100	200
Standard deviation for	in urban and suburban areas (dB)	3.56	3.80	4.19
DRM and RAVIS $\sigma_m$	in rural areas (dB)	2.86	3.10	3.49

These values of the standard deviation take into account only the effects of slow fading, but not the effects of fast fading. Therefore it must be ensured that the determination of the minimum C/N value consider the effects of the fast fading. Otherwise a margin depending to the bandwidth of the signal of 1.6 dB at 8 MHz, 2.3 dB at 1.5 MHz and 4.6 dB at 120 kHz has to be added.

For DRM and RAVIS the effects of fast fading are included into the measurement method and therefore they do not have to be added.

For the different reception modes more or less parts of the given particular standard deviations have to be taken into account, see Table 19.

Due to these differences the combined standard deviation  $\sigma_c$  (dB) for the respective reception modes are given in Table 20.

TABLE 19
Allowance for the particular standard deviations for the different reception modes

Particular standard deviations		$\sigma_m$	$\sigma_m$	$\sigma_m$	$\sigma_{MMN}$	$\sigma_b$
Frequency (MHz)		65	100	200	all	all
Reception modes	fixed (FX) and portable outdoor (PO) (dB)	3.56	3.80	4.19	4.53	0.00
	portable handheld outdoor (PO-H) (dB)	3.56	3.80	4.19	0.00	0.00
	mobile (MO) (dB)	2.86	3.10	3.49	4.53	0.00
	portable indoor (PI) (dB)	3.56	3.80	4.19	4.53	3.00
	portable handheld indoor (PI-H) (dB)	3.56	3.80	4.19	0.00	3.00

65 200 Frequency (MHz) 100 Combined standard fixed (FX) and portable outdoor (PO) (dB) 5.76 5.91 6.17 deviation  $\sigma_c$  for portable handheld outdoor (PO-H) (dB) 3.56 3.80 4.19 reception mode mobile (MO) (dB) 5.36 5.49 5.72 6.49 portable indoor (PI) (dB) 6.63 6.86

TABLE 20 Combined standard deviation  $\sigma_c$  for the different reception modes

#### 3.8.3 Combined location correction factor for protection ratios

portable handheld indoor (PI-H) (dB)

The needed protection of a wanted signal against an interfering signal is given as the basic protection ratio  $PR_{basic}$  (dB) for 50% of location probability.

In the case of higher location probability as given for all reception modes a so called combined location correction factor CF (dB) is used as a margin that has to be added to the basic protection ratio  $PR_{basic}$ , valid for the wanted field-strength level and the nuisance field-strength level, to the protection ratio PR(p) corresponding to the needed percentage p (%) of locations for the wanted service [1].

$$PR(p) (dB) = RPR_{basic} (dB) + CF(p) (dB)$$
 for  $50\% \le p \le 99\%$  (14)

with:

$$CF(p) (dB) = \mu(p) \sqrt{\sigma_w^2 + \sigma_n^2}$$
 (dB)

4.65

4.84

5.15

where  $\sigma_w$  and  $\sigma_n$ , both in (dB), denote the standard deviation of location variation for the wanted signal for the nuisance signal, respectively. The values for  $\sigma_w$  and  $\sigma_n$  are given in § 3.8.2 for the different broadcasting systems as  $\sigma_m$ .

#### 3.9 Polarization discrimination

In principal it is possible to take advantage of polarization discrimination for fixed reception. GE84 [5] does not take into account polarization discrimination in the planning procedure for VHF Band II, except in specific cases with the agreement of administrations concerned. In such cases, a value of 10 dB was used for orthogonal polarization discrimination.

GE06 [1] gives that in VHF Band III polarization discrimination shall not be taken into account in the DAB planning procedures.

For the planning procedures of digital sound broadcasting systems in the VHF bands no polarization discrimination will be taken into account for all reception modes.

#### 3.10 Calculation of minimum median field-strength level

The calculation of the minimum median field-strength level at 10 m above ground level for 50% of time and for 50% of locations is given in GE06 [1] by the following steps:

Step 1: Determine the receiver noise input power level  $P_n$ :

$$P_n (dBW) = F (dB) + 10\log_{10}(k \cdot T_0 \cdot B)$$
 (16)

where:

F: receiver noise figure (dB);

k: Boltzmann's constant,  $k = 1.38 \ 10^{-23} \ (J/K)$ ;

 $T_0$ : absolute temperature (K);

B: receiver noise bandwidth (Hz).

Step 2: Determine the minimum receiver input power level  $P_{s,min}$ :

$$P_{s,min} (dBW) = (C/N)_{min} (dB) + P_n (dBW)$$
(17)

where:

 $(C/N)_{min}$ : minimum carrier-to-noise ratio at the digital broadcasting decoder input (dB).

Step 3: Determine the minimum power flux-density (i.e. the magnitude of the Poynting vector) at receiving place  $\varphi_{min}$ :

$$\phi_{min} (dBW/m^2) = p_{smin} (dBW) - A_a (dBm^2) + L_f (dB)$$
(18)

where:

 $L_f$ : feeder loss (dB);

 $A_a$ : effective antenna aperture (dBm<sup>2</sup>).

$$A_a \text{ (dBm}^2\text{)} = 10 \cdot \log \left(\frac{1.64}{4\pi} \left(\frac{300}{f(\text{MHz})}\right)^2\right) + G_D \text{ (dB)}$$
 (19)

Step 4: Determine the minimum RMS field-strength level at the location of the receiving antenna  $E_{min}$ :

$$E_{min} \left( dB(\mu V/m) \right) = \varphi_{min} \left( dBW/m^2 \right) + 10 \log_{10} \left( Z_{F0} \right) \left( dB\Omega \right) + 20 \log_{10} \left( \frac{1 \text{ V}}{1 \mu V} \right)$$
 (20)

with:

$$Z_{F0} = \sqrt{\frac{\mu_0}{\varepsilon_0}} \approx 120 \,\pi \,(\Omega)$$
, the characteristic impedance in free space (21)

resulting in:

$$E_{min}\left(dB(\mu V/m)\right) = \varphi_{min}\left(dBW/m^2\right) + 145.8\left(dB\Omega\right)$$
 (22)

Step 5: Determine the minimum median RMS field-strength level  $E_{med}$ :

For the different receiving scenarios the minimum median RMS field strength is calculated as follows:

for fixed reception:

$$E_{med} = E_{min} + P_{mmn} + C_l \tag{23}$$

for portable outdoor and mobile reception:

$$E_{med} = E_{min} + P_{mmn} + C_l + L_h \tag{24}$$

for portable indoor reception:

$$E_{med} = E_{min} + P_{mmn} + C_l + L_h + L_b (25)$$

### 4 Planning parameters for digital terrestrial broadcasting system DRM robustness mode E in VHF Bands I, II and III

Digital Radio Mondiale<sup>TM</sup> (DRM) was originally designed by the DRM Consortium as a digital broadcasting system for the radio bands below 30 MHz and it is standardized as ETSIES 201 980 [6]. In 2009, DRM was extended by a mode E – called "DRM+" – to use DRM in radio bands up to 174 MHz.

The University of Applied Sciences in Kaiserslautern<sup>1</sup> (Germany) and the University of Hannover<sup>2</sup> (Germany) successfully conducted laboratory measurements and field trials with DRM in VHF Band II and in VHF Band III, respectively. Demonstrations were also given successfully in Paris in VHF Band I by the University of Applied Sciences in Kaiserslautern. Other field trials all over the world, especially in Brazil, Italy, Sri Lanka, the United Kingdom and in the Republic of Korea, have completed the tests.

The measurements and field trials have confirmed the technical parameters, and comparisons of coverage area have been performed between FM in VHF Band II and DRM also as with DAB in VHF Band III and DRM. In addition, protection ratio measurements have been performed and planning models have been used to predict coverage. The results from both German sites show that DRM works well in all VHF bands including VHF Band III.

From these results and based on relevant ITU Recommendations, this Report defines a framework for calculating all relevant DRM network planning parameters in all VHF bands. The focus lies on VHF Band II (87.5-108 MHz) and VHF Band III (174-230 MHz) in ITU Region 1, however where the values for the VHF Band I (47-68 MHz) are available, they are given.

Other frequency allocations in VHF bands assigned to broadcasting services are not exhaustively covered yet, e.g. areas in ITU Region 1 where allocations of the Wiesbaden T-DAB Agreement 1995 are still used (230-240 MHz) or in some Southern African countries, where the VHF Band III is allocated to the broadcasting services up to 254 MHz, or the broadcasting bands in ITU Regions 2 and 3, perhaps the OIRT FM band (65.8-74 MHz) or the Japanese FM band (76-90 MHz), respectively, that can later be adapted. Planning parameters for these unconsidered cases can be derived or taken from the given values, considering 254 MHz as the international top boundary of the VHF broadcasting spectrum<sup>3</sup>.

<sup>1</sup> http://www.fh-kl.de; http://www.drm-radio-kl.eu.

<sup>&</sup>lt;sup>2</sup> http://www.ikt.uni-hannover.de/.

Radio Regulations No. **5.252**: in Botswana, Lesotho, Malawi, Mozambique, Namibia, South Africa, Swaziland, Zambia and Zimbabwe, the bands 230-238 MHz and 246-254 MHz are allocated to the broadcasting service on a primary basis, subject to agreement obtained under No. **9.21**.

#### 4.1 DRM system parameters

The description of the DRM system parameters refers to Mode E of the DRM system [6].

#### 4.1.1 Modes and code rates

#### 4.1.1.1 Overview of SDC and MSC code rates

ETSI-DRM [6] defines the SDC code rates summarized in Table 21 and the MSC modes with code rates *R* given in Table 22.

TABLE 21

SDC code rates

	node 11 AM)	MSC-mode 00 (16-QAM)	
SDC-mode	Code rate R	SDC-mode Code ra	
0	0.5	0	0.5
1	0.25	1	0.25

TABLE 22

MSC code rates

Protection level		te R for 11: 4-QAM	Code rate R combinations for MSC mode 00: 16-QAM			
	$R_{all}$	$R_0$	$R_{all}$	$R_0$	$R_1$	$RY_{lcm}$
0	0.25	1/4	0.33	1/6	1/2	6
1	0.33	1/3	0.41	1/4	4/7	28
2	0.4	2/5	0.5	1/3	2/3	3
3	0.5	1/2	0.62	1/2	3/4	4

The net bit rate of the MSC varies from 37 kbit/s to 186 kbit/s depending of the used parameter set.

#### 4.1.1.2 SDC and MSC code rates for calculations

Several of the derived parameters depend on the characteristic of the transmitted DRM signal. To limit the amount of tests two typical parameters sets were chosen as basic sets, see Table 23:

- DRM with 4-QAM as a high protected signal with a lower data rate which is suited for a robust audio signal with a low data rate data service.
- **DRM with 16-QAM** as a low protected signal with a high data rate which is suited for several audio signals or for an audio signal with a high data rate data service.

 MSC mode
 11-4-QAM
 00-16-QAM

 MSC protection level
 1
 2

 MSC code rate R
 1/3
 1/2

 SDC mode
 1
 1

 SDC code rate R
 0.25
 0.25

49.7 kbit/s

149.1 kbit/s

TABLE 23

MSC code rates for calculations

#### 4.1.2 Propagation-related OFDM parameters

Bit rate approx.

The propagation-related OFDM parameters of DRM are given in Table 24.

TABLE 24 **OFDM parameters** 

Elementary time period T	83 1/3 μs
Duration of useful (orthogonal) part $T_u = 27 \cdot T$	2.25 ms
Duration of guard interval $T_g = 3 \cdot T$	0.25 ms
Duration of symbol $T_s = T_u + T_g$	2.5 ms
$T_g/T_u$	1/9
Duration of transmission frame $T_f$	100 ms
Number of symbols per frame $N_s$	40
Channel bandwidth B	96 kHz
Carrier spacing $1/T_u$	444 4/9 Hz
Carrier number space	$K_{min} = -106;$ $K_{max} = 106$
Unused carriers	none

#### 4.1.3 Single frequency operation capability

DRM transmitter can be operating in single frequency networks (SFN). The maximum transmitter distance that has to go below to prevent self-interferences depends on the length of the OFDM guard interval.

The maximum transmitter distance is calculated with the maximum echo delay which is given by:

$$D_{echo(max)} (km) = T_g \cdot c_0 \tag{26}$$

where:

$$c_0 = 300 \cdot 10^3 \text{ (km/s)};$$
  
 $T_g = 0.25 \text{ (s)}.$ 

Since the length  $T_g$  of the DRM guard interval is 0.25 ms, see Table 24, the maximum echo delay, and, therefore, the maximum transmitter distance, yields 75 km.

#### 4.1.4 Channel models

Radio wave propagation in VHF bands is characterized by diffraction, scattering and reflection of the electromagnetic waves on their way between the transmitter and the receiver. Typically the waves arrive at different times and different angles at the receiver (multipath propagation) resulting in more or less strong frequency-selective fading (dependent on system bandwidth). In addition movements of the receiver or surrounding objects cause a time variation of the channel characteristic and can result in Doppler shift.

For calculation of the different reception modes the channel models are given in Table 25 [6] have been assumed and investigated. These channel models are considering the fading characteristics for different reception environments. For receivers with higher frequencies the fading in time direction is normally short, so the interleaving and error correction algorithms can work. With slow receiver velocities flat fading over a time, longer than the interleaver (600 ms) can result in signal drop outs.

TABLE 25
Channel models in the ETSI standard for DRM

Channel model (name)	Velocity	Remark
Channel 7 (AWGN)	0 km/h	no time variation
Channel 8 (urban)	2 km/h and 60 km/h	pedestrian and vehicle speed
Channel 9 (rural)	150 km/h	vehicle speed on highways
Channel 10 (terrain obstructed)	60 km/h	vehicle speed within built-in areas
Channel 11 (hilly terrain)	100 km/h	vehicle speed along country roads
Channel 12 (SFN)	150 km/h	vehicle speed on highways

#### 4.2 DRM receiver parameters

#### 4.2.1 General characteristics

A DRM receiver is intended to receive and decode programmes transmitted according to the DRM system specification Mode E (DRM+) [6].

The parameters relevant for determining the required minimum field-strength levels are:

- noise figure  $F_r$  (dB), measured from the antenna input to the I/Q base band DRM decoder input (including down conversion and A/D conversion);
- receiver noise input power  $P_n$  (dBW);
- minimum carrier-to-noise ratio  $(C/N)_{min}$  (dB) at the DRM decoder input;
- minimum receiver input power level  $P_{s,min}$  (dBW).

#### 4.2.2 Receiver noise figure

In GE06 a receiver noise figure of 7 dB is been used for both DVB-T and T-DAB. For having cost effective DRM receiver solutions the receiver noise figure F is assumed to be  $F_r = 7$  dB too for all VHF bands, see Table 26.

TABLE 26 Receiver noise figure  $F_r$ 

Frequency (MHz)	65	100	200
Receiver noise figure $F_r(dB)$	7	7	7

#### 4.2.3 Receiver noise input power

With B = 100 kHz and T = 290 K, the thermal receiver noise input power level  $P_n$  for DRM Mode E yields:

$$P_n(dBW) = F_r(dB) + 10 \log_{10}(k \cdot T_0 \cdot B) = -146.98 (dBW)$$
 (27)

#### 4.2.4 Minimum carrier to noise ratio

On basis of the channel models in the respective reception mode the required minimum values of the  $(C/N)_{min}$  had been calculated. Therefore effects of the narrow-band system like fast fading are included in the calculated values of the  $(C/N)_{min}$ .

ETSI-DRM [6] gives a required  $(C/N)_{min}$  for a transmission in VHF Band II to achieve an average coded bit error ratio BER =  $1 \cdot 10^{-4}$  (bit) after the channel decoder for different channel models, see Table 27.

TABLE 27 (C/N)<sub>min</sub> with different channel models

		$(CN)_{min}$ (dB) for		
Reception mode	Channel model	4-QAM, $R = 1/3$	16-QAM, $R = 1/2$	
Fixed reception	Channel 7 (AWGN)	1.3	7.9	
Portable reception	Channel 8 (urban@60 km/h)	7.3	15.4	
	Channel 9 (rural)	5.6	13.1	
	Channel 10 (terrain obstructed)	5.4	12.6	
Mobile reception	Channel 11 (hilly terrain)	5.5	12.8	
	Channel 12 (SFN)	5.4	12.3	

#### 4.2.5 Minimum receiver input power level

Based on the above equations and including the implementation loss factor, the minimum receiver input power level at the receiving location can be calculated for both 16-QAM and 4-QAM, see Table 28 and Table 29.

TABLE 28 Minimum receiver input power level  $P_{s,min}$  for 4-QAM, R = 1/3

Reception mode		Fixed	Portable	Mobile
Receiver noise figure	$F_r$ (dB)	7	7	7
Receiver noise input power level	$P_n$ (dBW)	-146.98	-146.98	-146.98
Representative minimum <i>C/N</i> ratio	$(C/N)_{min}$ (dB)	1.3	7.3	5.5
Implementation loss factor	$L_i$ (dB)	3	3	3
Minimum receiver input power level	$P_{s,min}$ (dBW)	-142.68	-136.68	-138.48

TABLE 29 Minimum receiver input power level  $P_{s,min}$  for 16-QAM, R = 1/2

Reception mode		Fixed	Portable	Mobile
Receiver noise figure	$F_r$ (dB)	7	7	7
Receiver noise input power level	$P_n$ (dBW)	-146.98	-146.98	-146.98
Representative minimum <i>C/N</i> ratio	$(C/N)_{min}$ (dB)	7.9	15.4	12.8
Implementation loss factor	$L_i$ (dB)	3	3	3
Minimum receiver input power level	$P_{s,min}$ (dBW)	-136.08	-128.58	-131.18

#### 4.3 DRM planning parameters

#### 4.3.1 Minimum median field-strength level

Based on the equations in § 3, the minimum median field-strength level for the respective reception modes had been calculated for both 16-QAM and 4-QAM, for VHF Bands I, II and III, see Table 30 to Table 35.

#### 4.3.1.1 VHF Band I

TABLE 30 Minimum median field-strength level  $E_{med}$  for 4-QAM, R=1/3 in VHF Band I

DRM modulation	ation 4-Q				QAM. $R = 1/3$		
Receiving situation		FX	PI	PI-H	PO	РО-Н	МО
Minimum receiver input power level	$P_{s,min}$ (dBW)	-142.68	-136.6 8	-136.68	-136.68	-136.68	-138.4 8
Antenna gain	$G_D$ (dBd)	0.00	-2.20	-22.76	-2.20	-22.76	-2.20
Effective antenna aperture	$A_a$ (dBm <sup>2</sup> )	4.44	2.24	-18.32	2.24	-18.32	2.24
Feeder-loss	$L_c  ext{ dB}$	1.10	0.00	0.00	0.00	0.00	0.22
Minimum power flux-density at receiving place	$\phi_{min}$ (dBW/m <sup>2</sup> )	-146.02	-138.9 2	-118.36	-138.92	-118.36	-140.5 0
Minimum field-strength level at receiving antenna	$E_{min}$ (dB( $\mu$ V/m))	-0.25	6.85	27.41	6.85	27.41	5.27
Allowance for man-made noise	P <sub>mmn</sub> (dB)	15.38	15.38	0.00	15.38	0.00	15.38

TABLE 30 (end)

Antenna height loss	$L_h$ (dB)	0.00	8.00	15.00	8.00	15.00	8.00
Building penetration loss	$L_b$ (dB)	0.00	8.00	8.00	0.00	0.00	0.00
Location probability		70%	95%	95%	95%	95%	99%
Distribution factor	μ	0.52	1.64	1.64	1.64	1.64	2.33
Standard deviation of DRM field strength	$\sigma_m$ (dB)	3.56	3.56	3.56	3.56	3.56	2.86
Standard deviation of MMN	$\sigma_{MMN}$ (dB)	4.53	4.53	0.00	4.53	0.00	4.53
Standard deviation of building penetration loss	$\sigma_b (dB)$	0.00	3.00	3.00	0.00	0.00	0.00
Location correction factor	$C_l$ (dB)	3.02	10.68	7.65	9.47	5.85	12.46
Minimum median field-strength level	$\frac{E_{med}}{(dB(\mu V/m))}$	18.15	48.91	58.06	39.71	48.26	41.11

DRM modulation		16-QAM. <i>R</i> = 1/2					
Receiving situation		FX	PI	PI-H	PO	РО-Н	MO
Minimum receiver input power level	P <sub>s,min</sub> (dBW)	-136.08	-128.58	-128.58	-128.58	-128.58	-131.18
Antenna gain	$G_D$ (dBd)	0.00	-2.20	-22.76	-2.20	-22.76	-2.20
Effective antenna aperture	$A_a$ (dBm <sup>2</sup> )	4.44	2.24	-18.32	2.24	-18.32	2.24
Feeder-loss	$L_c$ (dB)	1.10	0.00	0.00	0.00	0.00	0.22
Minimum power flux- density at receiving place	$\phi_{min}$ (dBW/m <sup>2</sup> )	-139.42	-130.82	-110.26	-130.82	-110.26	-133.20
Minimum field-strength level at receiving antenna	$\frac{E_{min}}{(dB(\mu V/m))}$	6.35	14.95	35.51	14.95	35.51	12.57
Allowance for man-made noise	$P_{mmn}$ (dB)	15.38	15.38	0.00	15.38	0.00	15.38
Antenna height loss	$L_h$ (dB)	0.00	8.00	15.00	8.00	15.00	8.00
Building penetration loss	$L_b$ (dB)	0.00	8.00	8.00	0.00	0.00	0.00
Location probability		70%	95%	95%	95%	95%	99%
Distribution factor	μ	0.52	1.64	1.64	1.64	1.64	2.33
Standard deviation of DRM field strength	$\sigma_m$ (dB)	3.56	3.56	3.56	3.56	3.56	2.86
Standard deviation of MMN	$\sigma_{MMN}$ (dB)	4.53	4.53	0.00	4.53	0.00	4.53
Standard deviation of building penetration loss	$\sigma_b (dB)$	0.00	3.00	3.00	0.00	0.00	0.00
Location correction factor	$C_l(dB)$	3.02	10.68	7.65	9.47	5.85	12.46
Minimum median field- strength level	$\frac{E_{med}}{(dB(\mu V/m))}$	24.75	57.01	66.16	47.81	56.36	48.41

#### **4.3.1.2 VHF Band II**

TABLE 32 Minimum median field-strength level  $E_{med}$  for 4-QAM, R=1/3 in VHF Band II

DRM modulation	PRM modulation $4-QAM. R = 1/3$						
Receiving situation		FX	PI	PI-H	PO	РО-Н	MO
Minimum receiver input power level	$P_{s,min}$ (dBW)	-142.68	-136.68	-136.68	-136.68	-136.68	-138.48
Antenna gain	$G_D$ (dBd)	0.00	-2.20	-19.02	-2.20	-19.02	-2.20
Effective antenna aperture	$A_a$ (dBm <sup>2</sup> )	0.70	-1.50	-18.32	-1.50	-18.32	-1.50
Feeder-loss	$L_c$ (dB)	1.40	0.00	0.00	0.00	0.00	0.28
Minimum power flux-density at receiving place	$\phi_{min}$ (dBW/m <sup>2</sup> )	-141.97	-135.17	-118.35	-135.17	-118.35	-136.69
Minimum field-strength level at receiving antenna	$E_{min}$ (dB( $\mu$ V/m))	3.79	10.59	27.41	10.59	27.41	9.07
Allowance for man-made noise	$P_{mmn}$ (dB)	10.43	10.43	0.00	10.43	0.00	10.43
Antenna height loss	$L_h$ (dB)	0.00	10.00	17.00	10.00	17.00	10.00
Building penetration loss	$L_b$ (dB)	0.00	9.00	9.00	0.00	0.00	0.00
Location probability		70%	95%	95%	95%	95%	99%
Distribution factor	μ	0.52	1.64	1.64	1.64	1.64	2.33
Standard deviation of DRM field strength	$\sigma_m (dB)$	3.80	3.80	3.80	3.80	3.80	3.10
Standard deviation of MMN	$\sigma_{MMN}$ (dB)	4.53	4.53	0.00	4.53	0.00	4.53
Standard deviation of building penetration loss	$\sigma_b (dB)$	0.00	3.00	3.00	0.00	0.00	0.00
Location correction factor	$C_l(dB)$	3.10	10.91	7.96	9.73	6.25	12.77
Minimum median field-strength level	$\frac{E_{med}}{(dB(\mu V/m))}$	17.32	50.92	61.37	40.74	50.66	42.27

TABLE 33 Minimum median field-strength level  $E_{med}$  for 16-QAM, R=1/2 in VHF Band II

DRM modulation				16-QAM	1 R = 1/2		
Receiving situation		FX	PI	PI-H	PO	РО-Н	MO
Minimum receiver input power level	$P_{s,min}$ (dBW)	-136.08	-128.58	-128.58	-128.58	-128.58	-131.18
Antenna gain	$G_D$ (dBd)	0.00	-2.20	-19.02	-2.20	-19.02	-2.20
Effective antenna aperture	$A_a$ (dBm <sup>2</sup> )	0.70	-1.50	-18.32	-1.50	-18.32	-1.50
Feeder-loss	$L_c$ (dB)	1.40	0.00	0.00	0.00	0.00	0.28
Minimum power flux-density at receiving place	$\frac{\phi_{min}}{(dBW/m^2)}$	-135.37	-127.07	-110.25	-127.07	-110.25	-129.39
Minimum field-strength level at receiving antenna	$E_{min}$ (dB( $\mu$ V/m))	10.39	18.69	35.51	18.69	35.51	16.37
Allowance for man-made noise	$P_{mmn}$ (dB)	10.43	10.43	0.00	10.43	0.00	10.43
Antenna height loss	$L_h$ (dB)	0.00	10.00	17.00	10.00	17.00	10.00
Building penetration loss	$L_b$ (dB)	0.00	9.00	9.00	0.00	0.00	0.00
Location probability		70%	95%	95%	95%	95%	99%
Distribution factor	μ	0.52	1.64	1.64	1.64	1.64	2.33
Standard deviation of DRM field strength	$\sigma_m$ (dB)	3.80	3.80	3.80	3.80	3.80	3.10
Standard deviation of MMN	$\sigma_{MMN}$ (dB)	4.53	4.53	0.00	4.53	0.00	4.53
Standard deviation of building penetration loss	$\sigma_b (dB)$	0.00	3.00	3.00	0.00	0.00	0.00
Location correction factor	$C_l(dB)$	3.10	10.91	7.96	9.73	6.25	12.77
Minimum median field-strength level	$E_{med} \\ (dB(\mu V/m))$	23.92	59.02	69.47	48.84	58.76	49.57

#### **4.3.1.3 VHF Band III**

TABLE 34 Minimum median field-strength level  $E_{med}$  for 4-QAM, R=1/3 in VHF Band III

DRM modulation	4-QAM. $R = 1/3$						
Receiving situation	FX	PI	PI-H	PO	РО-Н	MO	
Minimum receiver input power level	P <sub>s,min</sub> (dBW)	-142.68	-136.68	-136.68	-136.68	-136.68	-138.48
Antenna gain	$G_D$ (dBd)	0.00	-2.20	-13.00	-2.20	-13.00	-2.20
Effective antenna aperture	$A_a$ (dBm <sup>2</sup> )	-5.32	-7.52	-18.32	-7.52	-18.32	-7.52
Feeder-loss	$L_c$ (dB)	2.00	0.00	0.00	0.00	0.00	0.40
Minimum power flux-density at receiving place	φ <sub>min</sub> (dBW/m <sup>2</sup> )	-135.35	-129.15	-118.35	-129.15	-118.35	-130.55

TABLE 34 (end)

Minimum field-strength level at receiving antenna	$\frac{E_{min}}{(dB(\mu V/m))}$	10.41	16.61	27.41	16.61	27.41	15.21
Allowance for man-made noise	$P_{mmn}$ (dB)	3.62	3.62	0.00	3.62	0.00	3.62
Antenna height loss	$L_h$ (dB)	0.00	12.00	19.00	12.00	19.00	12.00
Building penetration loss	$L_b$ (dB)	0.00	9.00	9.00	0.00	0.00	0.00
Location probability		70%	95%	95%	95%	95%	99%
Distribution factor	μ	0.52	1.64	1.64	1.64	1.64	2.33
Standard deviation of DRM field strength	$\sigma_m$ (dB)	4.19	4.19	4.19	4.19	4.19	3.49
Standard deviation of MMN	$\sigma_{MMN}$ (dB)	4.53	4.53	0.00	4.53	0.00	4.53
Standard deviation of building penetration loss	$\sigma_b (dB)$	0.00	3.00	3.00	0.00	0.00	0.00
Location correction factor	$C_l(dB)$	3.24	11.29	8.48	10.15	6.89	13.31
Minimum median field-strength level	$\frac{E_{med}}{(dB(\mu V/m))}$	17.26	52.52	63.89	42.38	53.30	44.13

DRM modulation		16-QAM. $R = \frac{1}{2}$					
Receiving situation		FX	PI	PI-H	PO	РО-Н	МО
Minimum receiver input power level	$P_{s,min}$ (dBW)	-136.08	-128.58	-128.58	-128.58	-128.58	-131.18
Antenna gain	$G_D$ (dBd)	0.00	-2.20	-13.00	-2.20	-13.00	-2.20
Effective antenna aperture	$A_a$ (dBm <sup>2</sup> )	-5.32	-7.52	-18.32	-7.52	-18.32	-7.52
Feeder-loss	$L_c$ (dB)	2.00	0.00	0.00	0.00	0.00	0.40
Minimum power flux-density at receiving place	$\varphi_{min}$ (dBW/m <sup>2</sup> )	-128.75	-121.05	-110.25	-121.05	-110.25	-123.25
Minimum field-strength level at receiving antenna	$\frac{E_{min}}{(dB(\mu V/m))}$	17.01	24.71	35.51	24.71	35.51	22.51
Allowance for man-made noise	$P_{mmn}$ (dB)	3.62	3.62	0.00	3.62	0.00	3.62
Antenna height loss	$L_h$ (dB)	0.00	12.00	19.00	12.00	19.00	12.00
Building penetration loss	$L_b$ (dB)	0.00	9.00	9.00	0.00	0.00	0.00
Location probability		70%	95%	95%	95%	95%	99%
Distribution factor	μ	0.52	1.64	1.64	1.64	1.64	2.33
Standard deviation of DRM field strength	$\sigma_m$ (dB)	4.19	4.19	4.19	4.19	4.19	3.49
Standard deviation of MMN	$\sigma_{MMN}(dB)$	4.53	4.53	0.00	4.53	0.00	4.53
Standard deviation of building penetration loss	$\sigma_b (dB)$	0.00	3.00	3.00	0.00	0.00	0.00
Location correction factor	$C_l(dB)$	3.24	11.29	8.48	10.15	6.89	13.31
Minimum median field- strength level	$\frac{E_{med}}{(dB(\mu V/m))}$	23.86	60.62	71.99	50.48	61.40	51.43

#### 4.3.2 Position of DRM frequencies

The DRM system is designed to be used at any frequency with variable channelization constraints and propagation conditions throughout these bands [6].

Referring to the legal frequency plans in ITU Region 1 this Report covers DRM:

- in VHF Band I as well as in VHF Band II regarding to GE84 [5];
- in VHF Band III regarding to GE06 [1].

Other areas in the VHF bands assigned for sound broadcasting services, e.g. areas in ITU Region 1 where allocations of the Wiesbaden T-DAB Agreement 1995 are still used (230-240 MHz) or in southern Africa, where the VHF Band III is allocated to the broadcasting services up to 254 MHz, or the broadcasting bands in ITU Region 2 and 3, perhaps the OIRT FM band (65.8-74 MHz) or the Japanese FM band (76-90 MHz), respectively, are not yet covered in this section and can be adapted later.

#### 4.3.2.1 VHF Band I and VHF Band II

The DRM centre frequencies are positioned in 100 kHz distance according to the FM frequency grid in VHF Band II. The nominal carrier frequencies are, in principle, integral multiples of 100 kHz [5]. The DRM system is designed to be used with this raster [6].

The table of centre frequencies of DRM in VHF Band II is given in Attachment 2.

On the other hand it has to be considered to allow a spacing of 50 kHz in VHF Band II to achieve the full potential of the DRM hybrid mode and to alleviate the deployment of new DRM transmitters in the overcrowded FM band.

#### 4.3.2.2 VHF Band III

The frequency band of a DAB block has a bandwidth of 1.536 MHz [1] with lower and upper guard channels to fit into the 7 MHz channels of VHF Band III.

The DRM centre frequencies are positioned in 100 kHz distance beginning by 174.05 MHz and integral multiples of 100 kHz up to the end of VHF Band III.

The table of the centre frequencies of DRM in VHF Band III in the range from 174 to 230 MHz is given in Attachment 2.

#### 4.3.3 Out-of-band spectrum mask

The power density spectrum at the transmitter output is important to determine the adjacent channel interference.

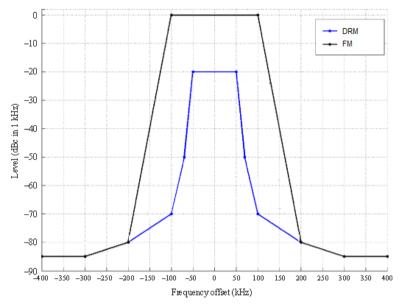
The spectrum characteristics of an OFDM system are given in Recommendation ITU-R SM.328, Annex 6, Chapter 5.

#### 4.3.3.1 VHF Band I and VHF Band II

An out-of-band spectrum mask for DRM in VHF Band I and VHF Band II, respectively, as minimum transmitter requirement is proposed in Fig. 1 and Table 36. The vertices of the symmetric out-of-band spectrum mask for FM transmitters are given in ETSI-FM [7].

Note that the out-of-band spectrum masks are defined for a resolution bandwidth (RBW) of 1 kHz.

 $FIGURE\ 1$  Out-of-band spectrum masks for FM in VHF Band II and DRM in VHF Bands I and II



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TABLE 36

Out-of-band spectrum masks for FM in VHF Band II and DRM in VHF Bands I and II

Spectrum mask (100 kHz channel)/ relative level for FM					
Frequency offset (kHz)	Level (dBc)/ (1 kHz)				
0	0				
±50	0				
±70	0				
±100	0				
±200	-80				
±300	-85				
±400	-85				

Spectrum mask (100 kHz channel)/ relative level for DRM					
Frequency offset (kHz)	Level (dBc)/ (1 kHz)				
0	-20				
±50	-20				
±70	-50				
±100	-70				
±200	-80				
±300	-85				
±400	-85				

#### **4.3.3.2 VHF Band III**

The vertices of the symmetric out-of-band spectrum masks for DAB transmitters are given in Recommendation ITU-R BS.1660. An out-of-band spectrum mask for DRM is proposed that fits into the DAB masks, see Fig. 2 and Table 37.

Note that the out-of-band spectrum masks are defined for a resolution bandwidth (RBW) of 4 kHz. Thus the value of -14 dBr results for DRM.

Out-of-band spectrum masks for DAB and DRM in VHF Band III

-20
-40
-40
-80
-80
-120
-120
-140
-4 -3 -2 -1 0 1 2 3 4

Frequency offset (MHz)

FIGURE 2
Out-of-band spectrum masks for DAB and DRM in VHF Band III

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DAB critical 12D

DAB critical

Spectrum mask (1.54 MHz channel)/ relative level for DAB							
Frequency offset (MHz)	Level (dBc) (non-critical cases)	Level (dBc) (critical cases)	Level (dBc) (critical cases/12D)				
±0.77	_	-26	-26				
< ±0.97	-26	_	_				
±0.97	-56	-71	-78				
±1.75	_	-106	_				
±2.2	_	_	-126				
±3.0	-106	-106	-126				

DAB uncritical

Spectrum mask (100 kHz channel) relative level for DRM					
Frequency offset (kHz)	Level (dBc)				
0	-14				
±50	-14				
±60	-44				
±181.25	-59				
±200	-74				
±300	-79				
±500	-84				

#### **4.3.4** Protection ratios

The minimum acceptable ratio between a wanted signal and interfering signals to protect the reception of the wanted signal is defined as the protection ratio PR (dB). The values of protection ratios are given as:

- **Basic protection ratio**  $PR_{basic}$  for a wanted signal interfered with by an unwanted signal at 50% location probability. These values are determined in accordance with Recommendation ITU-R BS.641.
- **Combined location correction factor** *CF* (dB) as a margin that has to be added to the basic protection ratio for a wanted signal interfered with by an unwanted signal for the

- calculation of protection ratios at location probability greater as 50%. The equation for the calculation is given in § 3.8.3.
- Corresponding protection ratio PR(p) for a wanted digital signal interfered with by an unwanted signal at location probability greater than 50% taking into account the respective location probability of the corresponding reception modes that have higher protection requirements due to the higher location probability to be protected.

#### 4.3.4.1 Protection ratios for DRM

The DRM signal parameters are given in § 4.1.

#### 4.3.4.1.1 DRM interfered with by DRM

The basic protection ratio  $PR_{basic}$  for DRM is valid for all VHF bands, see Table 38. For the standard deviation of DRM differs in the respective VHF bands the combined location correction factors CF, see Table 39, are different in the respective VHF bands as well as the corresponding protection ratios PR(p), see Table 40 for 4-OAM and Table 41 for 16-OAM.

TABLE 38 Basic protection ratios  $PR_{basic}$  for DRM interfered with by DRM

Frequency offset (kHz)		0	±100	±200
DRM (4-QAM, $R = 1/3$ )	PR <sub>basic</sub> (dB)	4	-16	-40
DRM (16-QAM, $R = 1/2$ )	PR <sub>basic</sub> (dB)	10	-10	-34

 $\begin{tabular}{ll} TABLE~39 \\ \begin{tabular}{ll} Combined location correction factor~\it{CF}~for~DRM~interfered~with~by~DRM \\ \end{tabular}$ 

Reference frequency band (MHz)		65 MHz VHF Band I		100 MHz VHF Band II		200 MHz VHF Band III				
Location probability p (%)		70	95	99	70	95	99	70	95	99
Combined location correction factor in urban and suburban area for fixed and portable reception	CF (dB)	2.64	8.27	11.70	2.82	8.84	12.50	3.11	9.75	13.79
Combined location correction factor in rural area for mobile reception	CF (dB)	2.12	6.65	9.40	2.30	7.21	10.20	2.59	8.12	11.49

TABLE 40 Corresponding protection ratios PR(p) to reception modes for DRM (4-QAM. R=1/3) interfered with by DRM

Reference frequency band (MHz		65 MHz VHF Band I		
Frequency offset (kHz)	0	±100	±200	
Fixed reception (FX)	PR(p) (dB)	6.64	-13.36	-37.36
Portable reception (PO, PI, PO-H, PI-H)	PR(p) (dB)	12.27	-7.73	-31.73
Mobile reception (MO)	PR(p) (dB)	13.40	-6.60	-30.60

Reference frequency band (MHz		100 MHz VHF Band II		
Frequency offset (kHz)	0	±100	±200	
Fixed reception (FX)	PR(p) (dB)	6.82	-13.18	-37.18
Portable reception (PO, PI, PO-H, PI-H) $PR(p)$ (dB)		12.84	-7.16	-31.16
Mobile reception (MO)	PR(p) (dB)	14.20	-5.80	-29.80

Reference frequency band (MHz	200 MHz VHF Band III			
Frequency offset (kHz)	0	±100	±200	
Fixed reception (FX)	PR(p) (dB)	7.11	-12.89	-36.89
Portable reception (PO. PI. PO-H. PI-H)	PR(p) (dB)	13.75	-6.25	-30.25
Mobile reception (MO)	PR(p) (dB)	15.49	-4.51	-28.51

TABLE 41 Corresponding protection ratios PR(p) to reception modes for DRM (16-QAM. R=1/2) interfered with by DRM

Reference frequency band (MHz)		65 MHz VHF Band I			
Frequency offset (kHz)		0	±100	±200	
Fixed reception (FX)	PR(p) (dB)	12.64	-7.36	-31.36	
Portable reception (PO. PI. PO-H. PI-H)	PR(p) (dB)	18.27	-1.73	-25.73	
Mobile reception (MO)	PR(p) (dB)	19.40	-0.60	-24.60	

Reference frequency band (MHz)		100 MHz VHF Band II			
Frequency offset (kHz)		0	±100	±200	
Fixed reception (FX)	PR(p) (dB)	12.82	-7.18	-31.18	
Portable reception (PO, PI, PO-H, PI-H)	PR(p) (dB)	18.84	-1.16	-25.16	
Mobile reception (MO)	PR(p) (dB)	20.20	0.20	-23.80	

TABLE 41 (end)

Reference frequency band (MHz)		200 MHz VHF Band III			
Frequency offset (kHz)		0	±100	±200	
Fixed reception (FX)	PR(p) (dB)	13.11	-6.89	-30.89	
Portable reception (PO, PI, PO-H, PI-H)	PR(p) (dB)	19.75	-0.25	-24.25	
Mobile reception (MO)	PR(p) (dB)	21.49	1.49	-22.51	

#### 4.3.4.1.2 DRM interfered with by FM in VHF Band II

The basic protection ratio  $PR_{basic}$  for DRM interfered with by FM in VHF Band II is given in Table 42. The values for the combined location correction factors CF are given in Table 43, and for the corresponding protection ratios PR(p), are given in Table 44 for 4-QAM and in Table 45 for 16-QAM, respectively.

TABLE 42 Basic protection ratios  $PR_{basic}$  for DRM interfered with by FM

Frequency offset (kHz)		0	±100	±200
DRM (4-QAM. $R = 1/3$ ) interfered with by FM (stereo)	PR <sub>basic</sub> (dB)	11	-13	-54
DRM (16-QAM. $R = 1/2$ ) interfered with by FM (stereo)	PR <sub>basic</sub> (dB)	18	-9	-49

 ${\it TABLE~43}$  Combined location correction  ${\it CF}$  factor for DRM interfered with by FM

Location probability <i>p</i> (%)		70	95	99
Combined location correction factor in urban and suburban area for fixed and portable reception	CF (dB)	4.79	15.02	21.24
Combined location correction factor in rural area for mobile reception	CF (dB)	4.65	14.57	20.61

TABLE 44 Corresponding protection ratios PR(p) to reception modes for DRM (4-QAM. R=1/3) interfered with by FM stereo

Frequency offset (kHz)		0	±100	±200
Fixed reception (FX)	PR(p) (dB)	15.79	-8.21	-49.21
Portable reception (PO, PI, PO-H, PI-H)	PR(p) (dB)	26.02	2.02	-38.98
Mobile reception (MO)	PR(p) (dB)	31.61	7.61	-33.39

TABLE 45 Corresponding protection ratios PR(p) to reception modes for DRM (16-QAM. R=1/2) interfered with by FM stereo

Frequency offset (kHz)		0	±100	±200
Fixed reception (FX)	PR(p) (dB)	22.79	-4.21	-44.21
Portable reception (PO, PI, PO-H, PI-H)	PR(p) (dB)	33.02	6.02	-33.98
Mobile reception (MO)	PR(p) (dB)	38.61	11.61	-28.39

#### 4.3.4.1.3 DRM interfered with by DAB in VHF Band III

The basic protection ratio  $PR_{basic}$  for DRM interfered with by DAB in VHF Band III is given in Table 46. The values for the combined location correction factors CF are given in Table 47, and for the corresponding protection ratios PR(p), are given in Table 48 for 4-QAM and in Table 49 for 16-QAM, respectively.

 ${\it TABLE~46}$  Basic protection ratios  ${\it PR}_{\it basic}$  of DRM interfered with by DAB

Frequency offset (kHz)		0	±100	±200
Basic protection ratio for DRM (4-QAM. $R = 1/3$ )	$PR_{basic}$ (dB)	-7	-36	-40
Basic protection ratio for DRM (16-QAM. $R = 1/2$ )	PR <sub>basic</sub> (dB)	-2	-18	-40

 ${\bf TABLE~47}$  Combined location correction factor  ${\it CF}$  of DRM interfered with by DAB

Location probability p (%)		70	95	99
Combined location correction factor in urban and suburban area for fixed and portable reception	CF (dB)	3.63	11.37	16.09
Combined location correction factor in rural area for mobile reception	CF (dB)	3.42	10.72	15.16

TABLE 48 Corresponding protection ratios PR(p) to reception modes for DRM (4-QAM. R=1/3) interfered with by DAB

Frequency offset (kHz)		0	±100	±200
Fixed reception (FX)	PR(p) (dB)	-3.37	-32.37	-50.37
Portable reception (PO, PI, PO-H, PI-H)	PR(p) (dB)	4.37	-24.63	-42.63
Mobile reception (MO)	PR(p) (dB)	8.16	-20.84	-38.84

TABLE 49

Corresponding protection ratios PR(p) to reception modes for DRM (16-QAM. R=1/2) interfered with by DAB

Frequency offset (kHz)		0	±100	±200
Fixed reception (FX)	PR(p) (dB)	1.63	-14.37	-45.37
Portable reception (PO, PI, PO-H, PI-H)	PR(p) (dB)	9.37	-6.63	-37.63
Mobile reception (MO)	PR(p) (dB)	13.16	-2.84	-33.84

#### 4.3.4.1.4 DRM interfered with by DVB-T in VHF Band III

Since the impact mechanisms of DAB into DRM is the same as that of DVB-T it is proposed that the same protection ratios for DRM interfered with by DVB-T in VHF Band III can be assumed as for DRM interfered with by DAB in VHF Band III.

#### 4.3.4.2 Protection ratios for broadcasting systems interfered with by DRM

#### 4.3.4.2.1 Protection ratios for FM in VHF Band II

The FM signal parameters are given in Recommendation ITU-R BS.412.

Recommendation ITU-R BS.412, Annex 5 states that interferences can be caused by intermodulation of strong FM signals in a frequency offset greater than 400 kHz. This cross modulation effect from a high interfering signal level in a range up to 1 MHz offset has also to be taken into account when planning OFDM systems into the VHF Band II. Therefore not only the protection ratios  $PR_{basic}$  are given in the range 0 kHz to  $\pm 400$  kHz, and for  $\pm 500$  kHz and  $\pm 1~000$  MHz, see Table 50. The values for  $\pm 600$  kHz to  $\pm 900$  kHz can be found by linear interpolation.

TABLE 50 Basic protection ratios  $PR_{basic}$  for FM interfered with by DRM

Frequency offset (kHz)		0	±100	±200	±300	±400	±500	±1 000
Basic protection ratio for FM (stereo)	PR <sub>basic</sub> (dB)	49	30	3	-8	-11	-13	-21

#### 4.3.4.2.2 Protection ratios for DAB in VHF Band III

The DAB signal parameters are given in Recommendation ITU-R BS.1660. In GE06 [1] it is given that the T-DAB planning should be able to deal with mobile reception with a location probability of 99%, and with portable indoor reception with a location probability of 95%, respectively. In addition the values for fixed reception with a location probability of 70% are given.

The basic protection ratios for DAB interfered with by DRM are given in Table 51, the related combined location correction factors are given in Table 52, and the corresponding protection ratios PR(p) are given in Table 53, respectively.

TABLE 51 Basic protection ratios  $PR_{basic}$  for DAB interfered with by DRM

Frequency offset (kHz)		0	±100	±200
Basic protection ratio for T-DAB	PR <sub>basic</sub> (dB)	10	-40	-40

TABLE 52

Combined location correction factor *CF* for DAB interfered with by DRM

Location probability <i>p</i> (%)		70	95	99
Combined location correction factor in urban and suburban area for fixed and portable reception	CF (dB)	3.63	11.37	16.09
Combined location correction factor in rural area for mobile reception	CF (dB)	3.42	10.72	15.16

TABLE 53

Corresponding protection ratios PR(p) to reception modes for DAB interfered with by DRM

Frequency offset (kHz)		0	±100	±200
DAB fixed reception	PR(p) (dB)	13.63	-36.37	-36.37
DAB portable reception	PR(p) (dB)	21.37	-28.63	-28.63
DAB mobile reception	PR(p) (dB)	25.16	-24.84	-24.84

#### 4.3.4.2.3 Protection ratios for DVB-T in VHF Band III

The DVB-T signal parameters are given in Recommendation ITU-R BT.1368.

In VHF Band III not only DAB but also may be DVB-T operated additionally as an interferer into DRM or to be interfered with by DRM.

DRM as an interferer against a DAB wanted signal has the same impact as a DAB interferer under the assumption that more than one DRM interferer with different frequencies in a DAB block has to be included, see Table 51.

The same proposal can be assumed if DVB-T is the wanted signal. If there is more than one DRM interferer with different frequencies in a DVB-T channel the impact may be the same as it is caused by a DAB signal. Therefore, it is proposed that the protection ratios of DVB-T interfered with by DRM are the same as DVB-T is interfered with by DAB.

In Recommendation ITU-R BT.1368 the basic protection ratios for DVB-T interfered with DAB are given, see Table 54. These protection rations are proposed for the interferences by a DRM signal also. In the adjacent channels no impact is proposed.

TABLE 54 Co-channel basic protection ratios  $PR_{basic}$  for DVB-T interfered with by DAB (Recommendation ITU-R BT.1368) and by DRM

Wanted signal DVB-T constellation-code rate	PR (dB)
QPSK-1/2	10
QPSK-2/3	12
QPSK-3/4	14
16-QAM-1/2	15
16-QAM-2/3	18
16-QAM-3/4	20
64-QAM-1/2	20
64-QAM-2/3	24
64-QAM-3/4	26
64-QAM-7/8	31

#### 4.3.4.3 Protection ratios for other services interfered with by DRM

## 4.3.4.3.1 Other services below the radio broadcasting VHF Band II

Below the VHF Band II broadcasting band, land mobile services with security tasks are located. The interference potential of DRM into these services is not higher as the one of FM signals. Provided sufficient additional band-pass filtering of the output of the transmitter is applied, the interference potential of DRM into narrow-band FM (BOS) reception is not substantially higher than that of a standard FM broadcast signal [8].

#### 4.3.4.3.2 Other services above the radio broadcasting VHF Band II

Above the VHF Band II broadcasting band, aeronautical radio navigation services are located. The interference potential of DRM into these services is not higher as the one of FM signals. For frequency offsets of less than 200 kHz, the interference potential of DRM into VOR and ILS localizer reception is much less than of a standard FM broadcast signal (up to 30 dB less). For larger frequency offsets, both signals produce roughly the same interference, provided sufficient additional band-pass filtering of the output of the transmitter is deployed [8].

#### 4.3.4.3.3 Other services in the radio broadcasting VHF Band III

The values and the procedures to take into account other services in VHF Band III is given in GE06. For DRM the same values as for DAB shall be applied.

## 4.3.5 Calculation of the resulting sum field strength of interferers

To calculate the resulting interfering sum field-strength level from several signal sources  $E_{sum}$ 

- in VHF Band I and VHF Band II the simplified multiplication method (see Report ITU-R BS.945) shall be applied according to GE84 [5];
- **in VHF Band III** the log-normal methods (see Report ITU-R BS.945) according to the planning procedures of T-DAB and DVB-T [1] shall be applied.

# 5 Planning parameters for digital terrestrial broadcasting system RAVIS in VHF Bands I and II

The RAVIS system is designed for digital sound and multimedia broadcasting in VHF Bands I and II. The system is nationally standardized in the Russian Federation [9-13]. Main characteristics and features of RAVIS can be found in Report ITU-R BT.2049 – Broadcasting of multimedia and data applications for mobile reception.

## 5.1 System parameters of RAVIS

## 5.1.1 RAVIS signal parameters

RAVIS supports three types of radio channel bandwidth: 100, 200 and 250 kHz.

RAVIS supports three different coding rates for logical channel of main service: 1/2, 2/3 and 3/4.

RAVIS supports three different modulation types for logical channel of main service: QPSK, 16-OAM and 64-OAM.

Rounded bit rates for different combinations of system parameters are given in Table 55.

TABLE 55
Bit rates for RAVIS

Modulation	Code rate		Bit rate (kbit/s)	
type	Code rate	100 kHz channel	200 kHz channel	250 kHz channel
QPSK	1/2	80	160	200
	2/3	100	210	270
	3/4	120	240	300
16-QAM	1/2	150	320	400
	2/3	210	420	530
	3/4	230	470	600
64-QAM	1/2	230	470	600
	2/3	310	630	800
	3/4	350	710	900

Main OFDM parameters of RAVIS signal are given in Table 56.

TABLE 56 **OFDM parameters of RAVIS** 

Channel bandwidth B	100 kHz	200 kHz	250 kHz		
Number of curriers	215	439	553		
Number of information curriers	196	400	504		
Distance between first and last curriers	95.1 kHz	194.7 kHz	245.3 kHz		
Carrier spacing $1/T_u$	4 000/9 Hz = 444 4/9 Hz				
Duration of useful part of symbol $T_u$		2.25 ms			

Duration of guard interval  $T_g$ 281.25 msDuration of symbol  $T_s = T_u + T_g$ 2.53125 ms $T_g/T_u$ 1/8Duration of transmission frame  $T_f$ 103.8 msNumber of symbols per frame  $N_s$ 41

TABLE 56 (end)

## 5.1.2 SFN operation capabilities

RAVIS can operate in single frequency networks (SFN). The maximum transmitter distance that has to go below to prevent self-interferences depends on the length of the OFDM guard interval. The maximum transmitter distance defined by (26) is calculated through the multiplication of velocity of light  $(3 \cdot 10^5 \text{ km/s})$  by guard interval duration (~0.28 ms for RAVIS). So maximum transmitter distance is about 84 km.

#### **5.1.3** Channel models

Channel models used for simulation of RAVIS operation corresponds to the models defined in DRM standard [6] and used for DRM operation simulation (see Table 25).

#### 5.2 RAVIS radio receiver related parameters

RAVIS receiver is intended to receive and decode programmes transmitted according to the RAVIS system standard [9].

The parameters relevant for determining the required minimum field-strength levels are:

- noise figure  $F_r$  (dB), measured from the antenna input to the I/Q base band RAVIS decoder input (including down conversion and A/D conversion);
- receiver noise input power  $P_n$  (dBW);
- minimum carrier-to-noise ratio  $(C/N)_{min}$  (dB) at the RAVIS decoder input;
- minimum receiver input power level  $P_{s,min}$  (dBW).

For having cost effective RAVIS receiver solutions the receiver noise figure F is assumed to be  $F_r = 7$  dB as for DRM receiver for all VHF bands, see Table 26.

Receiver noise input power  $P_n$  is calculated according to (16) and depends on input signal bandwidth (T = 290 K):

 $P_n$  (dBW) = -146.98 (dBW) for 100 kHz signal bandwidth;

 $P_n$  (dBW) = -143.97 (dBW) for 200 kHz signal bandwidth;

 $P_n$  (dBW) = -143.00 (dBW) for 250 kHz signal bandwidth.

Required  $(C/N)_{min}$  for a transmission in VHF Band II to achieve an average coded bit error ratio BER =  $1 \cdot 10^{-4}$  (bit) after the channel decoder for system parameters and different channel models are given in Tables 57 to 59. Channel models correspond to the models from [6], Annex B.2. Channel 7 (AWGN) models fixed reception mode, channel 8 (Urban) models portable reception mode, channel 11 (Hilly terrain) models mobile reception mode.

TABLE 57  $(C/N)_{min} \ \text{for RAVIS with 100 kHz channel bandwidth}$ 

Channel model/		$(C/N)_{min}$ (dB)								
reception mode		QPSK			16-QAM			64-QAM		
	R=1/2	R = 2/3	R = 3/4	R = 1/2	R = 2/3	R = 3/4	R = 1/2	R=2/3	R = 3/4	
Channel 7 (AWGN)/fixed reception	5 1.2	6 3.4	6 4.3	8 6.6	1 9.2	1 10.3	1 10.9	1 14.2	1 15.6	
Channel 8 (urban)/ portable reception	1 6.5	1 9.5	1 11.7	1 12.6	1 15.1	1 17.2	2 16.3	2 19.6	2 22.2	
Channel 11 (hilly terrain)/mobile reception	9 5.6	1 8.7	1 10.0	1 10.5	1 13.3	1 15.8	1 14.8	2 18.1	2 20.7	

TABLE 58  $(C/N)_{min} \ \mbox{for RAVIS with 200 kHz channel bandwidth}$ 

Channel model/		$(C/N)_{min}$ (dB)								
reception mode		QPSK		16-QAM				64-QAM		
	R=1/2	R = 2/3	R = 3/4	R = 1/2	R = 2/3	R = 3/4	R = 1/2	R=2/3	R = 3/4	
Channel 7 (AWGN)/fixed reception	4 1.1	5 3.3	6 4.2	8 6.4	1 9.1	1 10.2	1 10.8	1 14.0	1 15.4	
Channel 8 (urban)/ portable reception	1 6.4	1 9.4	1 11.5	1 12.5	1 14.9	1 17.0	2 16.2	2 19.4	2 22.0	
Channel 11 (hilly terrain)/mobile reception	1 5.5	1 8.6	1 9.8	1 10.4	1 13.2	1 15.6	1 14.7	2 17.9	2 20.5	

TABLE 59 (C/N)<sub>min</sub> for RAVIS with 250 kHz channel bandwidth

Channel model	(C/N) <sub>min</sub> (dB)									
/reception mode		QPSK		16-QAM				64-QAM		
	R = 1/2	R=2/3	R = 3/4	R = 1/2	R = 2/3	R = 3/4	R = 1/2	R=2/3	R=3/4	
Channel 7 (AWGN) /fixed reception	5	5	6	8	1	1	1	1	1	
	1.1	3.2	4.2	6.3	9.1	10.2	10.6	14.0	15.4	
Channel 8 (urban)	1	1	1	1	2	2	2	2	2	
/portable reception	6.4	9.4	11.5	12.4	14.9	17.0	16.1	19.4	22.0	
Channel 11 (hilly terrain)/mobile reception	1	1	1	1	1	1	2	2	2	
	5.5	8.5	9.8	10.3	13.2	15.6	14.6	17.9	20.5	

# 5.3 RAVIS planning parameters

## 5.3.1 Minimum median field-strength

Based on the parameters and equations set above, the minimum median field-strength level for different reception modes and frequency Bands I and II can be calculated for all sets of RAVIS system parameters, as shown in Tables 60 to 77.

TABLE 60Minimum median field-strength level  $E_{med}$  for  $100~\rm kHz$  channel bandwidth and QPSK modulation in Band I

Reception mode			FX	PI	РІ-Н	PO	РО-Н	МО
Receiver noise figure	F (dB)		7.00	7.00	7.00	7.00	7.00	7.00
Receiver noise input power	$P_n(dBW)$		-146.98	-146.98	-146.98	-146.98	-146.98	-146.98
Minimum C/N ratio	(C/N) <sub>min</sub>	R = 1/2	51.2	16.5	16.5	16.5	16.5	95.6
	(dB)	R = 2/3	63.4	19.5	19.5	19.5	19.5	18.7
		R = 3/4	64.3	111.7	111.7	111.7	111.7	110.0
Implementation loss	$L_i(dB)$		3.00	3.00	3.00	3.00	3.00	3.00
Minimum receiver input	$P_{s,min}(dBW)$	R = 1/2	-142.78	-137.48	-137.48	-137.48	-137.48	-138.38
power level		R = 2/3	-140.58	-134.48	-134.48	-134.48	-134.48	-135.28
		R = 3/4	-139.68	-132.28	-132.28	-132.28	-132.28	-133.98
Antenna gain	$G_d$ (dBd)		0.00	-2.20	-22.76	-2.20	-22.76	-2.20
Effective antenna aperture	$A_a$ (dBm <sup>2</sup> )		4.44	2.24	-18.32	2.24	-18.32	2.24
Feeder-loss	$L_f(dB)$		1.10	0.00	0.00	0.00	0.00	0.22
Minimum power	$\phi_{min}$	R = 1/2	-146.12	-139.72	-119.16	-139.72	-119.16	-140.40
flux-density at receiving place	(dBW/m <sup>2</sup> )	R = 2/3	-143.92	-136.72	-116.16	-136.72	-116.16	-137.30
prace		R = 3/4	-143.02	-134.52	-113.96	-134.52	-113.96	-136.00
Minimum field-strength	$E_{min}$	R = 1/2	-0.32	6.08	26.64	6.08	26.64	5.40
level at receiving antenna	$(dB(\mu V/m))$	R = 2/3	1.88	9.08	29.64	9.08	29.64	8.50
		R = 3/4	2.78	11.28	31.84	11.28	31.84	9.80
Allowance for man-made noise	$P_{MMN}(dB)$		15.38	15.38	0.00	15.38	0.00	15.38
Location probability	p (%)		70.00	95.00	95.00	95.00	95.00	99.00
Distribution factor	μ		0.52	1.65	1.65	1.65	1.65	2.33
Standard deviation of field strength	$\sigma_m(dB)$		3.56	3.56	3.56	83.56	83.56	82.86
Standard deviation of man-made noise	$\sigma_{MMN}$ (dB)		4.53	4.53	0.00	4.53	0.00	4.53
Standard deviation of building penetration loss	$\sigma_b(dB)$		0.00	3.00	3.00	0.00	0.00	0.00
Combined standard deviation of field strength	$\sigma_c$ (dB)		5.76	6.50	4.66	5.76	3.56	5.36
Location correction factor	$C_l(dB)$		3.00	10.72	7.68	9.51	5.87	12.48

TABLE 60 (end)

Reception mode			FX	PI	PI-H	PO	РО-Н	MO
Antenna height loss	$L_h(dB)$		0.00	8.00	815.00	8.00	815.00	8.00
Building penetration loss	$L_b(dB)$		0.00	98.00	98.00	0.00	0.00	0.00
Minimum median	$E_{med}$	R = 1/2	18.06	48.18	57.32	38.97	47.51	41.26
field-strength level	$(dB(\mu V/m))$	R = 2/3	20.26	51.18	60.32	41.97	50.51	44.36
		R = 3/4	21.16	53.38	62.52	44.17	52.71	45.66

TABLE 61  $\label{eq:table_entropy} \mbox{Minimum median field-strength level $E_{med}$ for 100 kHz channel bandwidth and QPSK modulation in Band II }$ 

Reception mode			FX	PI	PI-H	PO	РО-Н	МО
Receiver noise figure	F (dB)		7.00	7.00	7.00	7.00	7.00	7.00
Receiver noise input power	$P_n(dBW)$		-146.98	-146.98	-146.98	-146.98	-146.98	-146.98
Minimum C/N ratio	$(C/N)_{min}$	R = 1/2	1.20	6.50	6.50	6.50	6.50	5.60
	(dB)	R = 2/3	3.40	9.50	9.50	9.50	9.50	8.70
		R = 3/4	4.30	11.70	11.70	11.70	11.70	10.00
Implementation loss	$L_i(dB)$		3.00	3.00	3.00	3.00	3.00	3.00
Minimum receiver input	$P_{s,min}$ (dBW)	R = 1/2	-142.78	-137.48	-137.48	-137.48	-137.48	-138.38
power level		R = 2/3	-140.58	-134.48	-134.48	-134.48	-134.48	-135.28
		R = 3/4	-139.68	-132.28	-132.28	-132.28	-132.28	-133.98
Antenna gain	$G_d$ (dBd)		0.00	-2.20	-19.02	-2.20	-19.02	-2.20
Effective antenna aperture	$A_a$ (dBm <sup>2</sup> )		0.70	-1.50	-18.32	-1.50	-18.32	-1.50
Feeder-loss	$L_f(dB)$		1.40	0.00	0.00	0.00	0.00	0.28
Minimum power	$\phi_{min}$ (dBW/m <sup>2</sup> )	R = 1/2	-142.08	-135.98	-119.16	-135.98	-119.16	-136.60
flux-density at receiving place		R = 2/3	-139.88	-132.98	-116.16	-132.98	-116.16	-133.50
prace		R = 3/4	-138.98	-130.78	-113.96	-130.78	-113.96	-132.20
Minimum field-strength	$E_{min}$	R = 1/2	3.72	9.82	26.64	9.82	26.64	9.20
level at receiving antenna	$(dB(\mu V/m))$	R = 2/3	5.92	12.82	29.64	12.82	29.64	12.30
antenna		R = 3/4	6.82	15.02	31.84	15.02	31.84	13.60
Allowance for man-made noise	$P_{MMN}(dB)$		10.43	10.43	0.00	10.43	0.00	10.43
Location probability	p (%)		70.00	95.00	95.00	95.00	95.00	99.00
Distribution factor	μ		0.52	1.65	1.65	1.65	1.65	2.33
Standard deviation of field strength	$\sigma_m$ (dB)		3.80	3.80	3.80	3.80	3.80	3.10
Standard deviation of man-made noise	$\sigma_{MMN}$ (dB)		4.53	4.53	0.00	4.53	0.00	4.53

TABLE 61 (end)

Reception mode			FX	PI	PI-H	PO	РО-Н	МО
Standard deviation of building penetration loss	$\sigma_b(\mathrm{dB})$		0.00	3.00	3.00	0.00	0.00	0.00
Combined standard deviation of field strength	$\sigma_c(\mathrm{dB})$		5.91	6.63	4.84	5.91	3.80	5.49
Location correction factor	$C_l(dB)$		3.07	10.94	7.99	9.76	6.27	12.79
Antenna height loss	$L_h(dB)$		0.00	10.00	17.00	10.00	17.00	10.00
Building penetration loss	$L_b(dB)$		0.00	9.00	9.00	0.00	0.00	0.00
Minimum median	$E_{med}$	R = 1/2	17.23	50.19	60.63	40.01	49.91	42.42
field-strength level	$(dB(\mu V/m))$	R = 2/3	19.43	53.19	63.63	43.01	52.91	45.52
		R = 3/4	20.33	55.39	65.83	45.21	55.11	46.82

TABLE 62  $\label{eq:med_for_strength} \mbox{Minimum median field-strength level $E_{med}$ for 100 kHz channel bandwidth and 16-QAM modulation in Band I }$ 

Reception mode			FX	PI	PI-H	PO	РО-Н	МО
Receiver noise figure	F (dB)		7.00	7.00	7.00	7.00	7.00	7.00
Receiver noise input power	$P_n(dBW)$		-146.98	-146.98	-146.98	-146.98	-146.98	-146.98
Minimum <i>C/N</i> ratio	$(C/N)_{min}(dB)$	R = 1/2	6.60	12.60	12.60	12.60	12.60	10.50
		R = 2/3	9.20	15.10	15.10	15.10	15.10	13.30
		R = 3/4	10.30	17.20	17.20	17.20	17.20	15.80
Implementation loss	$L_i(dB)$		3.00	3.00	3.00	3.00	3.00	3.00
Minimum receiver input	$P_{s,min}(dBW)$	R = 1/2	-137.38	-131.38	-131.38	-131.38	-131.38	-133.48
power level		R = 2/3	-134.78	-128.88	-128.88	-128.88	-128.88	-130.68
		R = 3/4	-133.68	-126.78	-126.78	-126.78	-126.78	-128.18
Antenna gain	$G_d(\mathrm{dBd})$		0.00	-2.20	-22.76	-2.20	-22.76	-2.20
Effective antenna aperture	$A_a$ (dBm <sup>2</sup> )		4.44	2.24	-18.32	2.24	-18.32	2.24
Feeder-loss	$L_f(dB)$		1.10	0.00	0.00	0.00	0.00	0.22
Minimum power	$\phi_{min}$	R = 1/2	-140.72	-133.62	-113.06	-133.62	-113.06	-135.50
flux-density at receiving place	$(dBW/m^2)$	R = 2/3	-138.12	-131.12	-110.56	-131.12	-110.56	-132.70
piace		R = 3/4	-137.02	-129.02	-108.46	-129.02	-108.46	-130.20
Minimum field-strength	$E_{min}$	R = 1/2	5.08	12.18	32.74	12.18	32.74	10.30
level at receiving antenna	$(dB(\mu V/m))$	R = 2/3	7.68	14.68	35.24	14.68	35.24	13.10
		R = 3/4	8.78	16.78	37.34	16.78	37.34	15.60
Allowance for man-made noise	$P_{MMN}(dB)$		15.38	15.38	0.00	15.38	0.00	15.38
Location probability	p (%)		70.00	95.00	95.00	95.00	95.00	99.00

TABLE 62 (end)

Reception mode			FX	PI	PI-H	PO	РО-Н	МО
Distribution factor	μ		0.52	1.65	1.65	1.65	1.65	2.33
Standard deviation of field strength	$\sigma_m (dB)$		3.56	3.56	3.56	3.56	3.56	2.86
Standard deviation of man-made noise	$\sigma_{MMN}$ (dB)		4.53	4.53	0.00	4.53	0.00	4.53
Standard deviation of building penetration loss	$\sigma_b(\mathrm{dB})$		0.00	3.00	3.00	0.00	0.00	0.00
Combined standard deviation of field strength	$\sigma_c(dB)$		5.76	6.50	4.66	5.76	3.56	5.36
Location correction factor	$C_l(dB)$		3.00	10.72	7.68	9.51	5.87	12.48
Antenna height loss	$L_h(dB)$		0.00	8.00	815.00	8.00	815.00	8.00
Building penetration loss	$L_b$		0.00	98.00	98.00	0.00	0.00	0.00
Minimum median	$E_{med}$	R = 1/2	23.46	54.28	63.42	45.07	53.61	46.16
field-strength level	$(dB(\mu V/m))$	R = 2/3	26.06	56.78	65.92	47.57	56.11	48.96
		R = 3/4	27.16	58.88	68.02	49.67	58.21	51.46

 ${\it TABLE~63}$  Minimum median field-strength level  $E_{med}$  for 100 kHz channel bandwidth and 16-QAM modulation in Band II

Reception mode			FX	PI	PI-H	PO	РО-Н	МО
Receiver noise figure	F (dB)		7.00	7.00	7.00	7.00	7.00	7.00
Receiver noise input power	$P_n(dBW)$		-146.98	-146.98	-146.98	-146.98	-146.98	-146.98
Minimum C/N ratio	(C/N) <sub>min</sub>	R = 1/2	6.60	12.60	12.60	12.60	12.60	10.50
	(dB)	R = 2/3	9.20	15.10	15.10	15.10	15.10	13.30
		R = 3/4	10.30	17.20	17.20	17.20	17.20	15.80
Implementation loss	$L_i$ (dB)		3.00	3.00	3.00	3.00	3.00	3.00
Minimum receiver input	$P_{s,min}(dBW)$	R = 1/2	-137.38	-131.38	-131.38	-131.38	-131.38	-133.48
power level		R = 2/3	-134.78	-128.88	-128.88	-128.88	-128.88	-130.68
		R = 3/4	-133.68	-126.78	-126.78	-126.78	-126.78	-128.18
Antenna gain	$G_d$ (dBd)		0.00	-2.20	-19.02	-2.20	-19.02	-2.20
Effective antenna aperture	$A_a$ (dBm <sup>2</sup> )		0.70	-1.50	-18.32	-1.50	-18.32	-1.50
Feeder-loss	$L_f(dB)$		1.40	0.00	0.00	0.00	0.00	0.28
Minimum power flux-density at receiving	$\phi_{min}$	R = 1/2	-136.68	-129.88	-113.06	-129.88	-113.06	-131.70
	(dDW//m²)	R = 2/3	-134.08	-127.38	-110.56	-127.38	-110.56	-128.90
place		R = 3/4	-132.98	-125.28	-108.46	-125.28	-108.46	-126.40

TABLE 63 (end)

Reception mode			FX	PI	PI-H	PO	РО-Н	МО
Minimum field-strength	$E_{min}$	R = 1/2	9.12	15.92	32.74	15.92	32.74	14.10
level at receiving antenna	$(dB(\mu V/m))$	R = 2/3	11.72	18.42	35.24	18.42	35.24	16.90
antenna		R = 3/4	12.82	20.52	37.34	20.52	37.34	19.40
Allowance for man- made noise	$P_{MMN}(dB)$		10.43	10.43	0.00	10.43	0.00	10.43
Location probability	p (%)		70.00	95.00	95.00	95.00	95.00	99.00
Distribution factor	μ		0.52	1.65	1.65	1.65	1.65	2.33
Standard deviation of field strength	$\sigma_m$ (dB)		3.80	3.80	3.80	3.80	3.80	3.10
Standard deviation of man-made noise	$\sigma_{MMN}$ (dB)		4.53	4.53	0.00	4.53	0.00	4.53
Standard deviation of building penetration loss	$\sigma_b(dB)$		0.00	3.00	3.00	0.00	0.00	0.00
Combined standard deviation of field strength	$\sigma_c(\mathrm{dB})$		5.91	6.63	4.84	5.91	3.80	5.49
Location correction factor	$C_l$ (dB)		3.07	10.94	7.99	9.76	6.27	12.79
Antenna height loss	$L_h(dB)$		0.00	10.00	17.00	10.00	17.00	10.00
Building penetration loss	$L_b(dB)$		0.00	9.00	9.00	0.00	0.00	0.00
Minimum median	$E_{med}$	R = 1/2	22.63	56.29	66.73	46.11	56.01	47.32
field-strength level	$(dB(\mu V/m))$	R = 2/3	25.23	58.79	69.23	48.61	58.51	50.12
		R = 3/4	26.33	60.89	71.33	50.71	60.61	52.62

 ${\it TABLE~64}$  Minimum median field-strength level  $E_{med}$  for 100 kHz channel bandwidth and 64-QAM modulation in Band I

Reception mode			FX	PI	PI-H	PO	РО-Н	МО
Receiver noise figure	F (dB)		7.00	7.00	7.00	7.00	7.00	7.00
Receiver noise input power	$P_n(dBW)$		-146.98	-146.98	-146.98	-146.98	-146.98	-146.98
Minimum C/N ratio	(C/N) <sub>min</sub> (dB)	R = 1/2	10.90	16.30	16.30	16.30	16.30	14.80
		R = 2/3	14.20	19.60	19.60	19.60	19.60	18.10
		R = 3/4	15.60	22.20	22.20	22.20	22.20	20.70
Implementation loss	$L_i(dB)$		3.00	3.00	3.00	3.00	3.00	3.00
Minimum receiver input	$P_{s,min}(dBW)$	R = 1/2	-133.08	-127.68	-127.68	-127.68	-127.68	-129.18
power level		R = 2/3	-129.78	-124.38	-124.38	-124.38	-124.38	-125.88
		R = 3/4	-128.38	-121.78	-121.78	-121.78	-121.78	-123.28
Antenna gain	$G_d(\mathrm{dBd})$		0.00	-2.20	-22.76	-2.20	-22.76	-2.20
Effective antenna aperture	$A_a$ (dBm <sup>2</sup> )		4.44	2.24	-18.32	2.24	-18.32	2.24
Feeder-loss	$L_f(dB)$		1.10	0.00	0.00	0.00	0.00	0.22

TABLE 64 (end)

Reception mode			FX	PI	РІ-Н	РО	РО-Н	МО
Minimum power	$\phi_{min}$	R = 1/2	-136.42	-129.92	-109.36	-129.92	-109.36	-131.20
flux-density at receiving	$(dBW/m^2)$	R = 2/3	-133.12	-126.62	-106.06	-126.62	-106.06	-127.90
place		R = 3/4	-131.72	-124.02	-103.46	-124.02	-103.46	-125.30
Minimum field-strength	$E_{min}$	R = 1/2	9.38	15.88	36.44	15.88	36.44	14.60
level at receiving antenna	$(dB(\mu V/m))$	R = 2/3	12.68	19.18	39.74	19.18	39.74	17.90
antenna		R = 3/4	14.08	21.78	42.34	21.78	42.34	20.50
Allowance for man- made noise	$P_{MMN}(dB)$		15.38	15.38	0.00	15.38	0.00	15.38
Location probability	p (%)		70.00	95.00	95.00	95.00	95.00	99.00
Distribution factor	μ		0.52	1.65	1.65	1.65	1.65	2.33
Standard deviation of field strength	$\sigma_m (\mathrm{dB})$		3.56	3.56	3.56	3.56	3.56	2.86
Standard deviation of man-made noise	$\sigma_{MMN}$ (dB)		4.53	4.53	0.00	4.53	0.00	4.53
Standard deviation of building penetration loss	$\sigma_b(dB)$		0.00	3.00	3.00	0.00	0.00	0.00
Combined standard deviation of field strength	$\sigma_c(\mathrm{dB})$		5.76	6.50	4.66	5.76	3.56	5.36
Location correction factor	$C_l(dB)$		3.00	10.72	7.68	9.51	5.87	12.48
Antenna height loss	$L_h(dB)$		0.00	8.00	815.00	8.00	815.00	8.00
Building penetration loss	$L_b(dB)$		0.00	98.00	98.00	0.00	0.00	0.00
Minimum median field-	$E_{med}$	R = 1/2	27.76	57.98	67.12	48.77	57.31	50.46
strength level	$(dB(\mu V/m))$	R = 2/3	31.06	61.28	70.42	52.07	60.61	53.76
		R = 3/4	32.46	63.88	73.02	54.67	63.21	56.36

TABLE 65  $\label{eq:med} \mbox{Minimum median field-strength level $E_{med}$ for 100 kHz channel bandwidth and 64-QAM modulation in Band II}$ 

Reception mode			FX	PI	РІ-Н	PO	РО-Н	МО
Receiver noise figure	F (dB)		7.00	7.00	7.00	7.00	7.00	7.00
Receiver noise input power	$P_n(dBW)$		-146.98	-146.98	-146.98	-146.98	-146.98	-146.98
Minimum <i>C/N</i> ratio	$(C/N)_{min}$	R = 1/2	10.90	16.30	16.30	16.30	16.30	14.80
	(dB)	R = 2/3	14.20	19.60	19.60	19.60	19.60	18.10
		R = 3/4	15.60	22.20	22.20	22.20	22.20	20.70
Implementation loss	$L_i(dB)$		3.00	3.00	3.00	3.00	3.00	3.00

TABLE 65 (end)

Reception mode			FX	PI	PI-H	PO	РО-Н	МО
Minimum receiver	$P_{s,min}(dBW)$	R = 1/2	-133.08	-127.68	-127.68	-127.68	-127.68	-129.18
input power level		R = 2/3	-129.78	-124.38	-124.38	-124.38	-124.38	-125.88
		R = 3/4	-128.38	-121.78	-121.78	-121.78	-121.78	-123.28
Antenna gain	$G_d$ (dBd)		0.00	-2.20	-19.02	-2.20	-19.02	-2.20
Effective antenna aperture	$A_a$ (dBm <sup>2</sup> )		0.70	-1.50	-18.32	-1.50	-18.32	-1.50
Feeder-loss	$L_f(dB)$		1.40	0.00	0.00	0.00	0.00	0.28
Minimum power flux-	$\phi_{min} (dBW/m^2)$	R = 1/2	-132.38	-126.18	-109.36	-126.18	-109.36	-127.40
density at receiving place		R = 2/3	-129.08	-122.88	-106.06	-122.88	-106.06	-124.10
prace		R = 3/4	-127.68	-120.28	-103.46	-120.28	-103.46	-121.50
Minimum field-	$E_{min}$	R = 1/2	13.42	19.62	36.44	19.62	36.44	18.40
strength level at	$(dB(\mu V/m))$	R = 2/3	16.72	22.92	39.74	22.92	39.74	21.70
receiving antenna		R = 3/4	18.12	25.52	42.34	25.52	42.34	24.30
Allowance for man-made noise	$P_{MMN}(dB)$		10.43	10.43	0.00	10.43	0.00	10.43
Location probability	p (%)		70.00	95.00	95.00	95.00	95.00	99.00
Distribution factor	μ		0.52	1.65	1.65	1.65	1.65	2.33
Standard deviation of field strength	$\sigma_m$ (dB)		3.80	3.80	3.80	3.80	3.80	3.10
Standard deviation of man-made noise	$\sigma_{MMN}$ (dB)		4.53	4.53	0.00	4.53	0.00	4.53
Standard deviation of building penetration loss	$\sigma_b(dB)$		0.00	3.00	3.00	0.00	0.00	0.00
Combined standard deviation of field strength	$\sigma_c(dB)$		5.91	6.63	4.84	5.91	3.80	5.49
Location correction factor	$C_l(dB)$		3.07	10.94	7.99	9.76	6.27	12.79
Antenna height loss	$L_h(dB)$		0.00	10.00	17.00	10.00	17.00	10.00
Building penetration loss	$L_b(dB)$		0.00	9.00	9.00	0.00	0.00	0.00
Minimum median	$E_{med}$	R = 1/2	26.93	59.99	70.43	49.81	59.71	51.62
field-strength level	$(dB(\mu V/m))$	R = 2/3	30.23	63.29	73.73	53.11	63.01	54.92
		R = 3/4	31.63	65.89	76.33	55.71	65.61	57.52

 ${\it TABLE~66}$  Minimum median field-strength level  $E_{med}$  for 200 kHz channel bandwidth and QPSK modulation in Band I

Reception mode			FX	PI	PI-H	PO	РО-Н	МО
Receiver noise figure	F (dB)		7.00	7.00	7.00	7.00	7.00	7.00
Receiver noise input power	$P_n(dBW)$		-143.97	-143.97	-143.97	-143.97	-143.97	-143.97
Minimum C/N ratio	$(C/N)_{min}$ (dB)	R = 1/2	1.10	6.40	6.40	6.40	6.40	5.50
		R = 2/3	3.30	9.40	9.40	9.40	9.40	8.60
		R = 3/4	4.20	11.50	11.50	11.50	11.50	9.80
Implementation loss	$L_i$ (dB)		3.00	3.00	3.00	3.00	3.00	3.00
Minimum receiver input	$P_{s,min}(dBW)$	R = 1/2	-139.87	-134.57	-134.57	-134.57	-134.57	-135.47
power level		R = 2/3	-137.67	-131.57	-131.57	-131.57	-131.57	-132.37
		R = 3/4	-136.77	-129.47	-129.47	-129.47	-129.47	-131.17
Antenna gain	$G_d(\mathrm{dBd})$		0.00	-2.20	-22.76	-2.20	-22.76	-2.20
Effective antenna aperture	$A_a$ (dBm <sup>2</sup> )		4.44	2.24	-18.32	2.24	-18.32	2.24
Feeder-loss	$L_f(dB)$		1.10	0.00	0.00	0.00	0.00	0.22
Minimum power	$\phi_{min}$	R = 1/2	-143.21	-136.81	-116.25	-136.81	-116.25	-137.49
flux-density at receiving place	$(dBW/m^2)$	R = 2/3	-141.01	-133.81	-113.25	-133.81	-113.25	-134.39
		R = 3/4	-140.11	-131.71	-111.15	-131.71	-111.15	-133.19
Minimum field-strength	$E_{min}$	R = 1/2	2.59	8.99	29.55	8.99	29.55	8.31
level at receiving antenna	$(dB(\mu V/m))$	R = 2/3	4.79	11.99	32.55	11.99	32.55	11.41
		R = 3/4	5.69	14.09	34.65	14.09	34.65	12.61
Allowance for man-made noise	$P_{MMN}$ (dB)		15.38	15.38	0.00	15.38	0.00	15.38
Location probability	p (%)		70.00	95.00	95.00	95.00	95.00	99.00
Distribution factor	μ		0.52	1.65	1.65	1.65	1.65	2.33
Standard deviation of field strength	$\sigma_m(dB)$		3.56	3.56	3.56	3.56	3.56	2.86
Standard deviation of man-made noise	$\sigma_{MMN}$ (dB)		4.53	4.53	0.00	4.53	0.00	4.53
Standard deviation of building penetration loss	$\sigma_b(dB)$		0.00	3.00	3.00	0.00	0.00	0.00
Combined standard deviation of field strength	$\sigma_c(dB)$		5.76	6.50	4.66	5.76	3.56	5.36
Location correction factor	$C_l(dB)$		3.00	10.72	7.68	9.51	5.87	12.48
Antenna height loss	$L_h(dB)$		0.00	8.00	815.00	8.00	815.00	8.00
Building penetration loss	$L_b(dB)$		0.00	98.00	98.00	0.00	0.00	0.00
Minimum median field-	$E_{med}$	R = 1/2	20.97	51.09	60.23	41.88	50.42	44.17
strength level	(4D(-37/))	R = 2/3	23.17	54.09	63.23	44.88	53.42	47.27
		R = 3/4	24.07	56.19	65.33	46.98	55.52	48.47

 ${\it TABLE~67}$  Minimum median field-strength level  $E_{med}$  for 200 kHz channel bandwidth and QPSK modulation in Band II

Reception mode			FX	PI	PI-H	PO	РО-Н	МО
Receiver noise figure	F (dB)		7.00	7.00	7.00	7.00	7.00	7.00
Receiver noise input power	$P_n(dBW)$		-143.97	-143.97	-143.97	-143.97	-143.97	-143.97
Minimum C/N ratio	$(C/N)_{min}$ (dB)	R = 1/2	1.10	6.40	6.40	6.40	6.40	5.50
		R = 2/3	3.30	9.40	9.40	9.40	9.40	8.60
		R = 3/4	4.20	11.50	11.50	11.50	11.50	9.80
Implementation loss	$L_i(dB)$		3.00	3.00	3.00	3.00	3.00	3.00
Minimum receiver input	$P_{s,min}(dBW)$	R = 1/2	-139.87	-134.57	-134.57	-134.57	-134.57	-135.47
power level		R = 2/3	-137.67	-131.57	-131.57	-131.57	-131.57	-132.37
		R = 3/4	-136.77	-129.47	-129.47	-129.47	-129.47	-131.17
Antenna gain	$G_d(\mathrm{dBd})$		0.00	-2.20	-19.02	-2.20	-19.02	-2.20
Effective antenna aperture	$A_a$ (dBm <sup>2</sup> )		0.70	-1.50	-18.32	-1.50	-18.32	-1.50
Feeder-loss	$L_f(dB)$		1.40	0.00	0.00	0.00	0.00	0.28
Minimum power	$\phi_{min}$	R = 1/2	-139.17	-133.07	-116.25	-133.07	-116.25	-133.69
flux-density at receiving place	(dBW/m²)	R = 2/3	-136.97	-130.07	-113.25	-130.07	-113.25	-130.59
		R = 3/4	-136.07	-127.97	-111.15	-127.97	-111.15	-129.39
Minimum field-strength	$E_{min}$	R = 1/2	6.63	12.73	29.55	12.73	29.55	12.11
level at receiving	$(dB(\mu V/m))$	R = 2/3	8.83	15.73	32.55	15.73	32.55	15.21
antenna		R = 3/4	9.73	17.83	34.65	17.83	34.65	16.41
Allowance for man-made noise	$P_{MMN}(dB)$		10.43	10.43	0.00	10.43	0.00	10.43
Location probability	p (%)		70.00	95.00	95.00	95.00	95.00	99.00
Distribution factor	μ		0.52	1.65	1.65	1.65	1.65	2.33
Standard deviation of field strength	$\sigma_m$ (dB)		3.80	3.80	3.80	3.80	3.80	3.10
Standard deviation of man-made noise	$\sigma_{MMN}$ (dB)		4.53	4.53	0.00	4.53	0.00	4.53
Standard deviation of building penetration loss	$\sigma_b(dB)$		0.00	3.00	3.00	0.00	0.00	0.00
Combined standard deviation of field strength	$\sigma_c(\mathrm{dB})$		5.91	6.63	4.84	5.91	3.80	5.49
Location correction factor	$C_l(dB)$		3.07	10.94	7.99	9.76	6.27	12.79
Antenna height loss	$L_h(dB)$		0.00	10.00	17.00	10.00	17.00	10.00
Building penetration loss	$L_b(dB)$		0.00	9.00	9.00	0.00	0.00	0.00
Minimum median	$E_{med}$	R = 1/2	20.14	53.10	63.54	42.92	52.82	45.33
field-strength level	$(dB(\mu V/m))$	R = 2/3	22.34	56.10	66.54	45.92	55.82	48.43
	 	R = 3/4	23.24	58.20	68.64	48.02	57.92	49.63

 ${\it TABLE~68}$  Minimum median field-strength level  $E_{med}$  for 200 kHz channel bandwidth and 16-QAM modulation in Band I

Reception mode			FX	PI	PI-H	PO	РО-Н	МО
Receiver noise figure	F (dB)		7.00	7.00	7.00	7.00	7.00	7.00
Receiver noise input power	$P_n(dBW)$		-143.97	-143.97	-143.97	-143.97	-143.97	-143.97
Minimum C/N ratio	$(C/N)_{min}$	R = 1/2	6.40	12.50	12.50	12.50	12.50	10.40
	(dB)	R = 2/3	9.10	14.90	14.90	14.90	14.90	13.20
		R = 3/4	10.20	17.00	17.00	17.00	17.00	15.60
Implementation loss	$L_i$ (dB)		3.00	3.00	3.00	3.00	3.00	3.00
Minimum receiver input	$P_{s,min}$ (dBW)	R = 1/2	-134.57	-128.47	-128.47	-128.47	-128.47	-130.57
power level		R = 2/3	-131.87	-126.07	-126.07	-126.07	-126.07	-127.77
		R = 3/4	-130.77	-123.97	-123.97	-123.97	-123.97	-125.37
Antenna gain	$G_d$ (dBd)		0.00	-2.20	-22.76	-2.20	-22.76	-2.20
Effective antenna aperture	$A_a$ (dBm <sup>2</sup> )		4.44	2.24	-18.32	2.24	-18.32	2.24
Feeder-loss	$L_f(dB)$		1.10	0.00	0.00	0.00	0.00	0.22
Minimum power flux-	$\phi_{min}$	R = 1/2	-137.91	-130.71	-110.15	-130.71	-110.15	-132.59
density at receiving place	$(dBW/m^2)$	R = 2/3	-135.21	-128.31	-107.75	-128.31	-107.75	-129.79
prace		R = 3/4	-134.11	-126.21	-105.65	-126.21	-105.65	-127.39
Minimum field-strength	$E_{min}$	R = 1/2	7.89	15.09	35.65	15.09	35.65	13.21
level at receiving antenna	$(dB(\mu V/m))$	R = 2/3	10.59	17.49	38.05	17.49	38.05	16.01
antenna		R = 3/4	11.69	19.59	40.15	19.59	40.15	18.41
Allowance for man-made noise	$P_{MMN}$ (dB)		15.38	15.38	0.00	15.38	0.00	15.38
Location probability	p (%)		70.00	95.00	95.00	95.00	95.00	99.00
Distribution factor	μ		0.52	1.65	1.65	1.65	1.65	2.33
Standard deviation of field strength	$\sigma_m(dB)$		3.56	3.56	3.56	3.56	3.56	2.86
Standard deviation of man-made noise	$\sigma_{MMN}$ (dB)		4.53	4.53	0.00	4.53	0.00	4.53
Standard deviation of building penetration loss	$\sigma_b(dB)$		0.00	3.00	3.00	0.00	0.00	0.00
Combined standard deviation of field strength	$\sigma_c$ (dB)		5.76	6.50	4.66	5.76	3.56	5.36
Location correction factor	$C_l(dB)$		3.00	10.72	7.68	9.51	5.87	12.48
Antenna height loss	$L_h(dB)$		0.00	8.00	815.00	8.00	815.00	8.00
Building penetration loss	$L_b(dB)$		0.00	98.00	98.00	0.00	0.00	0.00
Minimum median	$E_{med}$	R = 1/2	26.27	57.19	66.33	47.98	56.52	49.07
field-strength level	$(dB(\mu V/m))$	R = 2/3	28.97	59.59	68.73	50.38	58.92	51.87
		R = 3/4	30.07	61.69	70.83	52.48	61.02	54.27

 ${\it TABLE~69}$  Minimum median field-strength level  $E_{med}$  for 200 kHz channel bandwidth and 16-QAM modulation in Band II

Reception mode			FX	PI	РІ-Н	РО	РО-Н	МО
Receiver noise figure	F (dB)		7.00	7.00	7.00	7.00	7.00	7.00
Receiver noise input power	$P_n(dBW)$		-143.97	-143.97	-143.97	-143.97	-143.97	-143.97
Minimum C/N ratio	$(C/N)_{min}$ (dB)	R = 1/2	6.40	12.50	12.50	12.50	12.50	10.40
		R = 2/3	9.10	14.90	14.90	14.90	14.90	13.20
		R = 3/4	10.20	17.00	17.00	17.00	17.00	15.60
Implementation loss	$L_i$ (dB)		3.00	3.00	3.00	3.00	3.00	3.00
Minimum receiver input	$P_{s min} (\mathrm{dBW})$	R = 1/2	-134.57	-128.47	-128.47	-128.47	-128.47	-130.57
power level		R = 2/3	-131.87	-126.07	-126.07	-126.07	-126.07	-127.77
		R = 3/4	-130.77	-123.97	-123.97	-123.97	-123.97	-125.37
Antenna gain	$G_d(\mathrm{dBd})$		0.00	-2.20	-19.02	-2.20	-19.02	-2.20
Effective antenna aperture	$A_a$ (dBm <sup>2</sup> )		0.70	-1.50	-18.32	-1.50	-18.32	-1.50
Feeder-loss	$L_f(dB)$		1.40	0.00	0.00	0.00	0.00	0.28
Minimum power	$\phi_{min}$	R = 1/2	-133.87	-126.97	-110.15	-126.97	-110.15	-128.79
flux-density at receiving place	$(dBW/m^2)$	R = 2/3	-131.17	-124.57	-107.75	-124.57	-107.75	-125.99
place		R = 3/4	-130.07	-122.47	-105.65	-122.47	-105.65	-123.59
Minimum field-strength	$E_{min}$	R = 1/2	11.93	18.83	35.65	18.83	35.65	17.01
level at receiving antenna	$(dB(\mu V/m))$	R = 2/3	14.63	21.23	38.05	21.23	38.05	19.81
antenna		R = 3/4	15.73	23.33	40.15	23.33	40.15	22.21
Allowance for man- made noise	$P_{MMN}(dB)$		10.43	10.43	0.00	10.43	0.00	10.43
Location probability	p (%)		70.00	95.00	95.00	95.00	95.00	99.00
Distribution factor	μ		0.52	1.65	1.65	1.65	1.65	2.33
Standard deviation of field strength	$\sigma_m$ (dB)		3.80	3.80	3.80	3.80	3.80	3.10
Standard deviation of man-made noise	$\sigma_{MMN}$ (dB)		4.53	4.53	0.00	4.53	0.00	4.53
Standard deviation of building penetration loss	$\sigma_b(dB)$		0.00	3.00	3.00	0.00	0.00	0.00
Combined standard deviation of field strength	$\sigma_c(\mathrm{dB})$		5.91	6.63	4.84	5.91	3.80	5.49
Location correction factor	$C_l(dB)$		3.07	10.94	7.99	9.76	6.27	12.79
Antenna height loss	$L_h(dB)$		0.00	10.00	17.00	10.00	17.00	10.00
Building penetration loss	$L_b(dB)$		0.00	9.00	9.00	0.00	0.00	0.00
Minimum median	$E_{med}$	R = 1/2	25.44	59.20	69.64	49.02	58.92	50.23
field-strength level	$(dB(\mu V/m))$	R = 2/3	28.14	61.60	72.04	51.42	61.32	53.03
		R = 3/4	29.24	63.70	74.14	53.52	63.42	55.43
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 ${\it TABLE~70}$  Minimum median field-strength level  $E_{med}$  for 200 kHz channel bandwidth and 64-QAM modulation in Band I

Reception mode			FX	PI	РІ-Н	PO	РО-Н	МО
Receiver noise figure	F (dB)		7.00	7.00	7.00	7.00	7.00	7.00
Receiver noise input power	$P_n(dBW)$		-143.97	-143.97	-143.97	-143.97	-143.97	-143.97
Minimum C/N ratio	$(C/N)_{min}$ (dB)	R = 1/2	10.80	16.20	16.20	16.20	16.20	14.70
		R = 2/3	14.00	19.40	19.40	19.40	19.40	17.90
		R = 3/4	15.40	22.00	22.00	22.00	22.00	20.50
Implementation loss	$L_i(dB)$		3.00	3.00	3.00	3.00	3.00	3.00
Minimum receiver input	$P_{s,min}(dBW)$	R = 1/2	-130.17	-124.77	-124.77	-124.77	-124.77	-126.27
power level		R = 2/3	-126.97	-121.57	-121.57	-121.57	-121.57	-123.07
		R = 3/4	-125.57	-118.97	-118.97	-118.97	-118.97	-120.47
Antenna gain	$G_d(\mathrm{dBd})$		0.00	-2.20	-22.76	-2.20	-22.76	-2.20
Effective antenna aperture	$A_a$ (dBm <sup>2</sup> )		4.44	2.24	-18.32	2.24	-18.32	2.24
Feeder-loss	$L_f(dB)$		1.10	0.00	0.00	0.00	0.00	0.22
Minimum power	$\phi_{min}$	R = 1/2	-133.51	-127.01	-106.45	-127.01	-106.45	-128.29
flux-density at receiving place	(dBW/m <sup>2</sup> )	R = 2/3	-130.31	-123.81	-103.25	-123.81	-103.25	-125.09
		R = 3/4	-128.91	-121.21	-100.65	-121.21	-100.65	-122.49
Minimum field-strength	$E_{min}$	R = 1/2	12.29	18.79	39.35	18.79	39.35	17.51
level at receiving	$(dB(\mu V/m))$	R = 2/3	15.49	21.99	42.55	21.99	42.55	20.71
antenna		R = 3/4	16.89	24.59	45.15	24.59	45.15	23.31
Allowance for man-made noise	$P_{MMN}(dB)$		15.38	15.38	0.00	15.38	0.00	15.38
Location probability	p (%)		70.00	95.00	95.00	95.00	95.00	99.00
Distribution factor	μ		0.52	1.65	1.65	1.65	1.65	2.33
Standard deviation of field strength	$\sigma_m (dB)$		3.56	3.56	3.56	3.56	3.56	2.86
Standard deviation of man-made noise	$\sigma_{MMN}$ (dB)		4.53	4.53	0.00	4.53	0.00	4.53
Standard deviation of building penetration loss	$\sigma_b(dB)$		0.00	3.00	3.00	0.00	0.00	0.00
Combined standard deviation of field strength	$\sigma_c(\mathrm{dB})$		5.76	6.50	4.66	5.76	3.56	5.36
Location correction factor	$C_l(dB)$		3.00	10.72	7.68	9.51	5.87	12.48
Antenna height loss	$L_h(dB)$		0.00	8.00	815.00	815.00	8.00	8.00
Building penetration loss	$L_b(dB)$		0.00	98.00	98.00	0.00	0.00	0.00
Minimum median	$E_{med}$	R = 1/2	30.67	60.89	70.03	51.68	60.22	53.37
field-strength level	$(dB(\mu V/m))$	R = 2/3	33.87	64.09	73.23	54.88	63.42	56.57
		R = 3/4	35.27	66.69	75.83	57.48	66.02	59.17

 ${\it TABLE~71}$  Minimum median field-strength level  $E_{med}$  for 200 kHz channel bandwidth and 64-QAM modulation in Band II

Reception mode			FX	PI	РІ-Н	PO	РО-Н	МО
Receiver noise figure	F (dB)		7.00	7.00	7.00	7.00	7.00	7.00
Receiver noise input power	$P_n(dBW)$		-143.97	-143.97	-143.97	-143.97	-143.97	-143.97
Minimum C/N ratio	$(C/N)_{min}(dB)$	R = 1/2	10.80	16.20	16.20	16.20	16.20	14.70
		R = 2/3	14.00	19.40	19.40	19.40	19.40	17.90
		R = 3/4	15.40	22.00	22.00	22.00	22.00	20.50
Implementation loss	$L_i(dB)$		3.00	3.00	3.00	3.00	3.00	3.00
Minimum receiver input	$P_{s,min}$ (dBW)	R = 1/2	-130.17	-124.77	-124.77	-124.77	-124.77	-126.27
power level		R = 2/3	-126.97	-121.57	-121.57	-121.57	-121.57	-123.07
		R = 3/4	-125.57	-118.97	-118.97	-118.97	-118.97	-120.47
Antenna gain	$G_d(\mathrm{dBd})$		0.00	-2.20	-19.02	-2.20	-19.02	-2.20
Effective antenna aperture	$A_a$ (dBm <sup>2</sup> )		0.70	-1.50	-18.32	-1.50	-18.32	-1.50
Feeder-loss	$L_f(dB)$		1.40	0.00	0.00	0.00	0.00	0.28
Minimum power	$\phi_{min}$	R = 1/2	-129.47	-123.27	-106.45	-123.27	-106.45	-124.49
flux-density at receiving place	(dBW/m <sup>2</sup> )	R = 2/3	-126.27	-120.07	-103.25	-120.07	-103.25	-121.29
		R = 3/4	-124.87	-117.47	-100.65	-117.47	-100.65	-118.69
Minimum field-strength	$E_{min}$	R = 1/2	16.33	22.53	39.35	22.53	39.35	21.31
level at receiving	$(dB(\mu V/m))$	R = 2/3	19.53	25.73	42.55	25.73	42.55	24.51
antenna		R = 3/4	20.93	28.33	45.15	28.33	45.15	27.11
Allowance for man- made noise	$P_{MMN}$ (dB)		10.43	10.43	0.00	10.43	0.00	10.43
Location probability	p (%)		70.00	95.00	95.00	95.00	95.00	99.00
Distribution factor	μ		0.52	1.65	1.65	1.65	1.65	2.33
Standard deviation of field strength	$\sigma_m$ (dB)		3.80	3.80	3.80	3.80	3.80	3.10
Standard deviation of man-made noise	$\sigma_{MMN}$ (dB)		4.53	4.53	0.00	4.53	0.00	4.53
Standard deviation of building penetration loss	$\sigma_b(dB)$		0.00	3.00	3.00	0.00	0.00	0.00
Combined standard deviation of field strength	$\sigma_c(\mathrm{dB})$		5.91	6.63	4.84	5.91	3.80	5.49
Location correction factor	$C_l(dB)$		3.07	10.94	7.99	9.76	6.27	12.79
Antenna height loss	$L_h(dB)$		0.00	10.00	17.00	10.00	17.00	10.00
Building penetration loss	$L_b(dB)$		0.00	9.00	9.00	0.00	0.00	0.00
Minimum median	$E_{med}$	R = 1/2	29.84	62.90	73.34	52.72	62.62	54.53
field-strength level	$(dB\mu V/m)$	R = 2/3	33.04	66.10	76.54	55.92	65.82	57.73
	-	R = 3/4	34.44	68.70	79.14	58.52	68.42	60.33

 ${\it TABLE~72}$  Minimum median field-strength level  $E_{med}$  for 250 kHz channel bandwidth and QPSK modulation in Band I

Reception mode			FX	PI	РІ-Н	PO	РО-Н	MO
Receiver noise figure	F (dB)		7.00	7.00	7.00	7.00	7.00	7.00
Receiver noise input power	$P_n(dBW)$		-143.00	-143.00	-143.00	-143.00	-143.00	-143.00
Minimum C/N ratio	(C/N) <sub>min</sub>	R = 1/2	1.10	6.40	6.40	6.40	6.40	5.50
	(dB)	R = 2/3	3.20	9.40	9.40	9.40	9.40	8.50
		R = 3/4	4.20	11.50	11.50	11.50	11.50	9.80
Implementation loss	$L_i(dB)$		3.00	3.00	3.00	3.00	3.00	3.00
Minimum receiver input	$P_{s,min}$	R = 1/2	-138.90	-133.60	-133.60	-133.60	-133.60	-134.50
power level	(dBW)	R = 2/3	-136.80	-130.60	-130.60	-130.60	-130.60	-131.50
		R = 3/4	-135.80	-128.50	-128.50	-128.50	-128.50	-130.20
Antenna gain	$G_d(\mathrm{dBd})$		0.00	-2.20	-22.76	-2.20	-22.76	-2.20
Effective antenna aperture	$A_a$ (dBm <sup>2</sup> )		4.44	2.24	-18.32	2.24	-18.32	2.24
Feeder-loss	$L_f(dB)$		1.10	0.00	0.00	0.00	0.00	0.22
Minimum power	$\phi_{min}$	R = 1/2	-142.24	-135.84	-115.28	-135.84	-115.28	-136.52
flux-density at receiving place	$(dBW/m^2)$	R = 2/3	-140.14	-132.84	-112.28	-132.84	-112.28	-133.52
piace		R = 3/4	-139.14	-130.74	-110.18	-130.74	-110.18	-132.22
Minimum field-strength	$E_{min}$ (dB( $\mu$ V/m))	R = 1/2	3.56	9.96	30.52	9.96	30.52	9.28
level at receiving antenna		R = 2/3	5.66	12.96	33.52	12.96	33.52	12.28
antenna		R = 3/4	6.66	15.06	35.62	15.06	35.62	13.58
Allowance for man- made noise	$P_{MMN}(dB)$		15.38	15.38	0.00	15.38	0.00	15.38
Location probability	<i>p</i> (%)		70.00	95.00	95.00	95.00	95.00	99.00
Distribution factor	μ		0.52	1.65	1.65	1.65	1.65	2.33
Standard deviation of field strength	$\sigma_m$ (dB)		3.56	3.56	3.56	3.56	3.56	2.86
Standard deviation of man-made noise	$\sigma_{MMN}$ (dB)		4.53	4.53	0.00	4.53	0.00	4.53
Standard deviation of building penetration loss	$\sigma_b(\mathrm{dB})$		0.00	3.00	3.00	0.00	0.00	0.00
Combined standard deviation of field strength	$\sigma_c(\mathrm{dB})$		5.76	6.50	4.66	5.76	3.56	5.36
Location correction factor	$C_l(dB)$		3.00	10.72	7.68	9.51	5.87	12.48
Antenna height loss	$L_h(dB)$		0.00	8.00	815.00	8.00	815.00	8.00
Building penetration loss	$L_b(dB)$		0.00	98.00	98.00	0.00	0.00	0.00
Minimum median	$E_{med}$	R = 1/2	21.93	52.06	61.20	42.85	51.39	45.14
field-strength level	$(dB(\mu V/m))$	R = 2/3	24.03	55.06	64.20	45.85	54.39	48.14
		R = 3/4	25.03	57.16	66.30	47.95	56.49	49.44

 ${\it TABLE~73}$  Minimum median field-strength level  $E_{med}$  for 250 kHz channel bandwidth and QPSK modulation in Band II

Reception mode			FX	PI	PI-H	PO	РО-Н	МО
Receiver noise figure	F (dB)		7.00	7.00	7.00	7.00	7.00	7.00
Receiver noise input power	$P_n(dBW)$		-143.00	-143.00	-143.00	-143.00	-143.00	-143.00
Minimum C/N ratio	$(C/N)_{min}$	R = 1/2	1.10	6.40	6.40	6.40	6.40	5.50
	(dB)	R = 2/3	3.20	9.40	9.40	9.40	9.40	8.50
		R = 3/4	4.20	11.50	11.50	11.50	11.50	9.80
Implementation loss	$L_i$ (dB)		3.00	3.00	3.00	3.00	3.00	3.00
Minimum receiver input	$P_{s,min}$	R = 1/2	-138.90	-133.60	-133.60	-133.60	-133.60	-134.50
power level	(dBW)	R = 2/3	-136.80	-130.60	-130.60	-130.60	-130.60	-131.50
		R = 3/4	-135.80	-128.50	-128.50	-128.50	-128.50	-130.20
Antenna gain	$G_d(\mathrm{dBd})$		0.00	-2.20	-19.02	-2.20	-19.02	-2.20
Effective antenna aperture	$A_a$ (dBm <sup>2</sup> )		0.70	-1.50	-18.32	-1.50	-18.32	-1.50
Feeder-loss	$L_f(dB)$		1.40	0.00	0.00	0.00	0.00	0.28
Minimum power	$\phi_{min}$	R = 1/2	-138.20	-132.10	-115.28	-132.10	-115.28	-132.72
flux-density at receiving place	(dBW/m <sup>2</sup> )	R = 2/3	-136.10	-129.10	-112.28	-129.10	-112.28	-129.72
prace		R = 3/4	-135.10	-127.00	-110.18	-127.00	-110.18	-128.42
Minimum field-strength	$\frac{E_{min}}{(dB(\mu V/m))}$	R = 1/2	7.60	13.70	30.52	13.70	30.52	13.08
level at receiving antenna		R = 2/3	9.70	16.70	33.52	16.70	33.52	16.08
antenna		R = 3/4	10.70	18.80	35.62	18.80	35.62	17.38
Allowance for man- made noise	$P_{MMN}(\mathrm{dB})$		10.43	10.43	0.00	10.43	0.00	10.43
Location probability	p (%)		70.00	95.00	95.00	95.00	95.00	99.00
Distribution factor	μ		0.52	1.65	1.65	1.65	1.65	2.33
Standard deviation of field strength	$\sigma_m$ (dB)		3.80	3.80	3.80	3.80	3.80	3.10
Standard deviation of man-made noise	$\sigma_{MMN}$ (dB)		4.53	4.53	0.00	4.53	0.00	4.53
Standard deviation of building penetration loss	$\sigma_b(\mathrm{dB})$		0.00	3.00	3.00	0.00	0.00	0.00
Combined standard deviation of field strength	$\sigma_c (\mathrm{dB})$		5.91	6.63	4.84	5.91	3.80	5.49
Location correction factor	$C_l(dB)$		3.07	10.94	7.99	9.76	6.27	12.79
Antenna height loss	$L_h(dB)$		0.00	10.00	17.00	10.00	170.00	10.00
Building penetration loss	$L_b(dB)$		0.00	9.00	9.00	0.00	0.00	0.00
Minimum median	$E_{med}$	R = 1/2	21.11	54.07	64.51	43.89	53.79	46.30
field-strength level	$(dB(\mu V/m))$	R = 2/3	23.21	57.07	67.51	46.89	56.79	49.30
		R = 3/4	24.21	59.17	69.61	48.99	58.89	50.60

 ${\it TABLE~74}$  Minimum median field-strength level  $E_{med}$  for 250 kHz channel bandwidth and 16-QAM modulation in Band I

Reception mode			FX	PI	РІ-Н	PO	РО-Н	МО
Receiver noise figure	F (dB)		7.00	7.00	7.00	7.00	7.00	7.00
Receiver noise input power	$P_n$ (dBW)		-143.00	-143.00	-143.00	-143.00	-143.00	-143.00
Minimum <i>C/N</i> ratio	$(C/N)_{min}$	R = 1/2	6.30	12.40	12.40	12.40	12.40	10.30
	(dB)	R = 2/3	9.10	14.90	14.90	14.90	14.90	13.20
		R = 3/4	10.20	17.00	17.00	17.00	17.00	15.60
Implementation loss	$L_i$ (dB)		3.00	3.00	3.00	3.00	3.00	3.00
Minimum receiver input	$P_{s,min}(dBW)$	R = 1/2	-133.70	-127.60	-127.60	-127.60	-127.60	-129.70
power level		R = 2/3	-130.90	-125.10	-125.10	-125.10	-125.10	-126.80
		R = 3/4	-129.80	-123.00	-123.00	-123.00	-123.00	-124.40
Antenna gain	$G_d(\mathrm{dBd})$		0.00	-2.20	-22.76	-2.20	-22.76	-2.20
Effective antenna aperture	$A_a$ (dBm <sup>2</sup> )		4.44	2.24	-18.32	2.24	-18.32	2.24
Feeder-loss	$L_f(dB)$		1.10	0.00	0.00	0.00	0.00	0.22
Minimum power	$\phi_{min}$	R = 1/2	-137.04	-129.84	-109.28	-129.84	-109.28	-131.72
flux-density at receiving place	$(dBW/m^2)$	R = 2/3	-134.24	-127.34	-106.78	-127.34	-106.78	-128.82
prace		R = 3/4	-133.14	-125.24	-104.68	-125.24	-104.68	-126.42
Minimum field-strength	$E_{min}$	R = 1/2	8.76	15.96	36.52	15.96	36.52	14.08
level at receiving antenna	$(dB(\mu V/m))$	R = 2/3	11.56	18.46	39.02	18.46	39.02	16.98
antenna		R = 3/4	12.66	20.56	41.12	20.56	41.12	19.38
Allowance for man- made noise	$P_{MMN}(dB)$		15.38	15.38	0.00	15.38	0.00	15.38
Location probability	p (%)		70.00	95.00	95.00	95.00	95.00	99.00
Distribution factor	μ		0.52	1.65	1.65	1.65	1.65	2.33
Standard deviation of field strength	$\sigma_m$ (dB)		3.56	3.56	3.56	3.56	3.56	2.86
Standard deviation of man-made noise	$\sigma_{MMN}$ (dB)		4.53	4.53	0.00	4.53	0.00	4.53
Standard deviation of building penetration loss	$\sigma_b(dB)$		0.00	3.00	3.00	0.00	0.00	0.00
Combined standard deviation of field strength	$\sigma_c(\mathrm{dB})$		5.76	6.50	4.66	5.76	3.56	5.36
Location correction factor	$C_l(dB)$		3.00	10.72	7.68	9.51	5.87	12.48
Antenna height loss	$L_h(dB)$		0.00	8.00	815.00	8.00	815.00	8.00
Building penetration loss	$L_b(dB)$		0.00	98.00	98.00	0.00	0.00	0.00
Minimum median	$E_{med}$	R = 1/2	27.13	58.06	67.20	48.85	57.39	49.94
field-strength level	$(dB(\mu V/m))$	R = 2/3	29.93	60.56	69.70	51.35	59.89	52.84
		R = 3/4	31.03	62.66	71.80	53.45	61.99	55.24

 ${\it TABLE~75}$  Minimum median field-strength level  $E_{med}$  for 250 kHz channel bandwidth and 16-QAM modulation in Band II

Reception mode			FX	PI	PI-H	PO	РО-Н	МО
Receiver noise figure	F(dB)		7.00	7.00	7.00	7.00	7.00	7.00
Receiver noise input power	$P_n(dBW)$		-143.00	-143.00	-143.00	-143.00	-143.00	-143.00
Minimum C/N ratio	$(C/N)_{min}$ (dB)	R = 1/2	6.30	12.40	12.40	12.40	12.40	10.30
		R = 2/3	9.10	14.90	14.90	14.90	14.90	13.20
		R = 3/4	10.20	17.00	17.00	17.00	17.00	15.60
Implementation loss	$L_i(dB)$		3.00	3.00	3.00	3.00	3.00	3.00
Minimum receiver	$P_{s,min}$	R = 1/2	-133.70	-127.60	-127.60	-127.60	-127.60	-129.70
input power level	(dBW)	R = 2/3	-130.90	-125.10	-125.10	-125.10	-125.10	-126.80
		R = 3/4	-129.80	-123.00	-123.00	-123.00	-123.00	-124.40
Antenna gain	$G_d(\mathrm{dBd})$		0.00	-2.20	-19.02	-2.20	-19.02	-2.20
Effective antenna aperture	$A_a$ (dBm <sup>2</sup> )		0.70	-1.50	-18.32	-1.50	-18.32	-1.50
Feeder-loss	$L_f(dB)$		1.40	0.00	0.00	0.00	0.00	0.28
Minimum power	$\phi_{min}(dBW/m^2)$	R = 1/2	-133.00	-126.10	-109.28	-126.10	-109.28	-127.92
flux-density at receiving place		R = 2/3	-130.20	-123.60	-106.78	-123.60	-106.78	-125.02
recerving place		R = 3/4	-129.10	-121.50	-104.68	-121.50	-104.68	-122.62
Minimum field-	$E_{min}$	R = 1/2	12.80	19.70	36.52	19.70	36.52	17.88
strength level at receiving antenna	(dB(μV/m))	R = 2/3	15.60	22.20	39.02	22.20	39.02	20.78
		R = 3/4	16.70	24.30	41.12	24.30	41.12	23.18
Allowance for man- made noise	$P_{MMN}(dB)$		10.43	10.43	0.00	10.43	0.00	10.43
Location probability	p (%)		70.00	95.00	95.00	95.00	95.00	99.00
Distribution factor	μ		0.52	1.65	1.65	1.65	1.65	2.33
Standard deviation of field strength	$\sigma_m$ (dB)		3.80	3.80	3.80	3.80	3.80	3.10
Standard deviation of man-made noise	$\sigma_{MMN}$ (dB)		4.53	4.53	0.00	4.53	0.00	4.53
Standard deviation of building penetration loss	$\sigma_b(dB)$		0.00	3.00	3.00	0.00	0.00	0.00
Combined standard deviation of field strength	$\sigma_c(dB)$		5.91	6.63	4.84	5.91	3.80	5.49
Location correction factor	$C_l(dB)$		3.07	10.94	7.99	9.76	6.27	12.79
Antenna height loss	$L_h(dB)$		0.00	10.00	17.00	10.00	17.00	10.00
Building penetration loss	$L_b(dB)$		0.00	9.00	9.00	0.00	0.00	0.00
Minimum median	$E_{med}$	R = 1/2	26.31	60.07	70.51	49.89	59.79	51.10
field-strength level	$(dB(\mu V/m))$	R = 2/3	29.11	62.57	73.01	52.39	62.29	54.00
		R = 3/4	30.21	64.67	75.11	54.49	64.39	56.40

 ${\it TABLE~76}$  Minimum median field-strength level  $E_{med}$  for 250 kHz channel bandwidth and 64-QAM modulation in Band I

Reception mode			FX	PI	РІ-Н	PO	РО-Н	МО
Receiver noise figure	F (dB)		7.00	7.00	7.00	7.00	7.00	7.00
Receiver noise input power	$P_n(dBW)$		-143.00	-143.00	-143.00	-143.00	-143.00	-143.00
Minimum C/N ratio	$(C/N)_{min}$	R = 1/2	10.60	16.10	16.10	16.10	16.10	14.60
	(dB)	R = 2/3	14.00	19.40	19.40	19.40	19.40	17.90
		R = 3/4	15.40	22.00	22.00	22.00	22.00	20.50
Implementation loss	$L_i$ (dB)		3.00	3.00	3.00	3.00	3.00	3.00
Minimum receiver input	$P_{s,min}$	R = 1/2	-129.40	-123.90	-123.90	-123.90	-123.90	-125.40
power level	(dBW)	R = 2/3	-126.00	-120.60	-120.60	-120.60	-120.60	-122.10
		R = 3/4	-124.60	-118.00	-118.00	-118.00	-118.00	-119.50
Antenna gain	$G_d(\mathrm{dBd})$		0.00	-2.20	-22.76	-2.20	-22.76	-2.20
Effective antenna aperture	$A_a$ (dBm <sup>2</sup> )		4.44	2.24	-18.32	2.24	-18.32	2.24
Feeder-loss	$L_f(dB)$		1.10	0.00	0.00	0.00	0.00	0.22
Minimum power	$\phi_{min}$	R = 1/2	-132.74	-126.14	-105.58	-126.14	-105.58	-127.42
flux-density at receiving place	(dBW/m <sup>2</sup> )	R = 2/3	-129.34	-122.84	-102.28	-122.84	-102.28	-124.12
prace		R = 3/4	-127.94	-120.24	-99.68	-120.24	-99.68	-121.52
Minimum field-strength	$E_{min}$	R = 1/2	13.06	19.66	40.22	19.66	40.22	18.38
level at receiving antenna	$(dB(\mu V/m))$	R = 2/3	16.46	22.96	43.52	22.96	43.52	21.68
antenna		R = 3/4	17.86	25.56	46.12	25.56	46.12	24.28
Allowance for man- made noise	$P_{MMN}(dB)$		15.38	15.38	0.00	15.38	0.00	15.38
Location probability	p (%)		70.00	95.00	95.00	95.00	95.00	99.00
Distribution factor	μ		0.52	1.65	1.65	1.65	1.65	2.33
Standard deviation of field strength	$\sigma_m$ (dB)		3.56	3.56	3.56	3.56	3.56	2.86
Standard deviation of man-made noise	$\sigma_{MMN}$ (dB)		4.53	4.53	0.00	4.53	0.00	4.53
Standard deviation of building penetration loss	$\sigma_b(dB)$		0.00	3.00	3.00	0.00	0.00	0.00
Combined standard deviation of field strength	$\sigma_c(dB)$		5.76	6.50	4.66	5.76	3.56	5.36
Location correction factor	$C_l(dB)$		3.00	10.72	7.68	9.51	5.87	12.48
Antenna height loss	$L_h(dB)$		0.00	8.00	815.00	8.00	815.00	8.00
Building penetration loss	$L_b(dB)$		0.00	98.00	98.00	0.00	0.00	0.00
Minimum median	$E_{med}$	R = 1/2	31.43	61.76	70.90	52.55	61.09	54.24
field-strength level	$(dB(\mu V/m))$	R = 2/3	34.83	65.06	74.20	55.85	64.39	57.54
		R = 3/4	36.23	67.66	76.80	58.45	66.99	60.14

 ${\it TABLE~77}$  Minimum median field-strength level  $E_{med}$  for 250 kHz channel bandwidth and 64-QAM modulation in Band II

Reception mode			FX	PI	PI-H	PO	РО-Н	MO
Receiver noise figure	F (dB)		7.00	7.00	7.00	7.00	7.00	7.00
Receiver noise input power	$P_n(dBW)$		-143.00	-143.00	-143.00	-143.00	-143.00	-143.00
Minimum C/N ratio	(C/N) <sub>min</sub>	R = 1/2	10.60	16.10	16.10	16.10	16.10	14.60
	(dB)	R = 2/3	14.00	19.40	19.40	19.40	19.40	17.90
		R = 3/4	15.40	22.00	22.00	22.00	22.00	20.50
Implementation loss	$L_i(dB)$		3.00	3.00	3.00	3.00	3.00	3.00
Minimum receiver input	$P_{s,min}$	R = 1/2	-129.40	-123.90	-123.90	-123.90	-123.90	-125.40
power level	(dBW)	R = 2/3	-126.00	-120.60	-120.60	-120.60	-120.60	-122.10
		R = 3/4	-124.60	-118.00	-118.00	-118.00	-118.00	-119.50
Antenna gain	$G_d$ (dBd)		0.00	-2.20	-19.02	-2.20	-19.02	-2.20
Effective antenna aperture	$A_a$ (dBm <sup>2</sup> )		0.70	-1.50	-18.32	-1.50	-18.32	-1.50
Feeder-loss	$L_f(dB)$		1.40	0.00	0.00	0.00	0.00	0.28
Minimum power	$\phi_{min}$	R = 1/2	-128.70	-122.40	-105.58	-122.40	-105.58	-123.62
flux-density at receiving place	(dBW/m <sup>2</sup> )	R = 2/3	-125.30	-119.10	-102.28	-119.10	-102.28	-120.32
prace		R = 3/4	-123.90	-116.50	-99.68	-116.50	-99.68	-117.72
Minimum field-strength	$E_{min}$	R = 1/2	17.10	23.40	40.22	23.40	40.22	22.18
level at receiving antenna	$(dB(\mu V/m))$	R = 2/3	20.50	26.70	43.52	26.70	43.52	25.48
		R = 3/4	21.90	29.30	46.12	29.30	46.12	28.08
Allowance for man-made noise	$P_{MMN}(dB)$		10.43	10.43	0.00	10.43	0.00	10.43
Location probability	p (%)		70.00	95.00	95.00	95.00	95.00	99.00
Distribution factor	μ		0.52	1.65	1.65	1.65	1.65	2.33
Standard deviation of field strength	$\sigma_m (dB)$		3.80	3.80	3.80	3.80	3.80	3.10
Standard deviation of man-made noise	$\sigma_{MMN}$ (dB)		4.53	4.53	0.00	4.53	0.00	4.53
Standard deviation of building penetration loss	$\sigma_b(\mathrm{dB})$		0.00	3.00	3.00	0.00	0.00	0.00
Combined standard deviation of field strength	$\sigma_c(\mathrm{dB})$		5.91	6.63	4.84	5.91	3.80	5.49
Location correction factor	$C_l(dB)$		3.07	10.94	7.99	9.76	6.27	12.79
Antenna height loss	$L_h$		0.00	10.00	17.00	10.00	17.00	10.00
Building penetration loss	$L_b$		0.00	9.00	9.00	0.00	0.00	0.00
Minimum median	$E_{med}$	R = 1/2	30.61	63.77	74.21	53.59	63.49	55.40
field-strength level	$(dB(\mu V/m))$	R = 2/3	34.01	67.07	77.51	56.89	66.79	58.70
		R = 3/4	35.41	69.67	80.11	59.49	69.39	61.30

#### 5.3.2 Out-of-band emissions

The spectrum masks for RAVIS transmission (for three types of channel bandwidth) [10] compared to spectrum mask for analogue FM (according to ETSI EN 302 018-2 [7]) are given in Tables 78-81 and Fig. 3. RAVIS spectrum masks are fitting into analogue FM spectrum mask.

TABLE 78

Spectrum mask for FM transmission

Frequency offset (kHz)	Level (dBc)/(1 kHz)
0	0
±100	0
±200	-80
±300	-85
±400	-85

TABLE 79

Spectrum mask for RAVIS transmission, 100 kHz channel bandwidth

Frequency offset (kHz)	Level (dBc)/(1 kHz)
0	-20
±50	-20
±70	-50
±100	-70
±200	-80
±300	-85
±400	-85

TABLE 80 Spectrum mask for RAVIS transmission, 200 kHz channel bandwidth

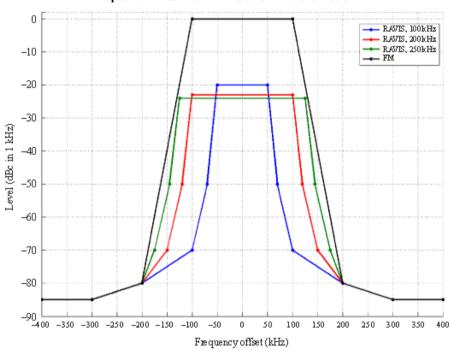
Frequency offset (kHz)	Level (dBc)/(1 kHz)
0	-23
±100	-23
±120	-50
±150	-70
±200	-80
±300	-85
±400	-85

TABLE 81

Spectrum mask for RAVIS transmission, 250 kHz channel bandwidth

Frequency offset (kHz)	Level (dBc)/(1 kHz)
0	-24
±125	-24
±145	-50
±175	-70
±200	-80
±300	-85
±400	-85

FIGURE 3
Spectrum mask for RAVIS and FM transmission



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## **5.3.3** Protection ratios

## **5.3.3.1** Protection ratios for FM

Basic protection ratios for FM interfered with by RAVIS are given in Table 82.

TABLE 82 Basic protection ratios  $PR_{basic}$  for FM interfered with by RAVIS

Frequency offset (kHz)		0	±100	±200	±300	±400
Basic protection ratio, channel bandwidth $B = 100 \text{ kHz}$	PR <sub>basic</sub> (dB)	50	35	5	-5	-10
Basic protection ratio, channel bandwidth $B = 200 \text{ kHz}$	PR <sub>basic</sub> (dB)	50				
Basic protection ratio, channel bandwidth $B = 250 \text{ kHz}$	PR <sub>basic</sub> (dB)	50				

## **5.3.3.2** Protection ratios for RAVIS

Basic protection ratios for RAVIS interfered with by RAVIS are given in Table 83.

TABLE 83 Basic protection ratios  $PR_{basic}$  for RAVIS interfered with by RAVIS

Basic protection ratios PRbasic for RAVIS interfered with by RAVIS									
Frequency offset (kl	Hz)	0	±100	±200	±300	±400			
B = 100  kHz, QPSK, R = 1/2	$PR_{basic}$ (dB)	8	0	-48	-55	-56			
B = 100  kHz, QPSK, R = 2/3	PR <sub>basic</sub> (dB)	9	2	-47	-54	-55			
B = 100 kHz, QPSK, R = 3/4	PR <sub>basic</sub> (dB)	10	3	-46	-53	-54			
B = 100 kHz, 16-QAM, R = 1/2	PR <sub>basic</sub> (dB)	12	6	-43	-51	-52			
B = 100 kHz, 16-QAM, R = 2/3	$PR_{basic}$ (dB)	14	8	-41	-49	-50			
B = 100 kHz, 16-QAM, R = 3/4	PR <sub>basic</sub> (dB)	15	9	-40	-48	-49			
B = 100  kHz, 64-QAM, R = 1/2	$PR_{basic}$ (dB)	16	10	-39	-47	-48			
B = 100 kHz, 64-QAM, R = 2/3	PR <sub>basic</sub> (dB)	19	13	-36	-44	-45			
B = 100 kHz, 64-QAM, R = 3/4	PR <sub>basic</sub> (dB)	20	14	-35	-43	-44			
B = 200  kHz,  QPSK, R = 1/2	$PR_{basic}$ (dB)	8	6	-22	-51	-54			
B = 200 kHz, QPSK, R = 2/3	PR <sub>basic</sub> (dB)	9	7	-6	-50	-53			
B = 200  kHz,  QPSK, R = 3/4	PR <sub>basic</sub> (dB)	10	8	-1	-49	-52			
B = 200  kHz, 16-QAM, R = 1/2	$PR_{basic}$ (dB)	12	10	2	-47	-49			
B = 200  kHz, 16-QAM, R = 2/3	$PR_{basic}$ (dB)	14	12	5	-45	-48			
B = 200  kHz, 16-QAM, R = 3/4	PR <sub>basic</sub> (dB)	15	13	6	-44	-47			
B = 200  kHz, 64-QAM, R = 1/2	$PR_{basic}$ (dB)	16	14	7	-42	-46			
B = 200  kHz, 64-QAM, R = 2/3	$PR_{basic}$ (dB)	19	17	10	-39	-43			
B = 200  kHz, 64-QAM, R = 3/4	PR <sub>basic</sub> (dB)	20	18	11	-38	-41			
B = 250  kHz,  QPSK, R = 1/2	PR <sub>basic</sub> (dB)	8	6	2	-47	-52			
B = 250  kHz,  QPSK, R = 2/3	PR <sub>basic</sub> (dB)	9	7	3	-46	-51			
B = 250 kHz, QPSK, R = 3/4	PR <sub>basic</sub> (dB)	10	8	5	-44	-50			
B = 250  kHz, 16-QAM, R = 1/2	PR <sub>basic</sub> (dB)	12	10	7	-41	-48			
B = 250 kHz, 16-QAM, R = 2/3	PR <sub>basic</sub> (dB)	14	12	9	-35	-46			
B = 250 kHz, 16-QAM, R = 3/4	$PR_{basic}$ (dB)	15	13	10	-32	-45			
B = 250 kHz, 64-QAM, R = 1/2	PR <sub>basic</sub> (dB)	16	14	11	-30	-44			
B = 250 kHz, 64-QAM, R = 2/3	PR <sub>basic</sub> (dB)	19	17	14	-24	-41			
B = 250 kHz, 64-QAM, R = 3/4	PR <sub>basic</sub> (dB)	20	18	15	-23	-40			

Basic protection ratios for RAVIS interfered with by FM are given in Table 84.

TABLE 84 Basic protection ratios  $PR_{basic}$  for RAVIS interfered with by RAVIS

Frequency offset (kH	0	±100	±200	±300	±400	
B = 100 kHz, QPSK, R = 1/2	PR <sub>basic</sub> (dB)	8	28	20	-55	-56
B = 100  kHz, QPSK, R = 2/3	PR <sub>basic</sub> (dB)	9	29	22	-54	-55
B = 100  kHz, QPSK, R = 3/4	PR <sub>basic</sub> (dB)	10	30	23	-53	-54
B = 100 kHz, 16-QAM, R = 1/2	PR <sub>basic</sub> (dB)	12	29	25	-51	-52
B = 100 kHz, 16-QAM, R = 2/3	PR <sub>basic</sub> (dB)	14	26	27	-49	-50
B = 100 kHz, 16-QAM, R = 3/4	PR <sub>basic</sub> (dB)	15	25	28	-48	-49
B = 100 kHz, 64-QAM, R = 1/2	PR <sub>basic</sub> (dB)	16	24	29	-47	-48
B = 100  kHz, 64-QAM, R = 2/3	$PR_{basic}$ (dB)	19	21	32	-44	-45
B = 100  kHz, 64-QAM, R = 3/4	$PR_{basic}$ (dB)	20	20	33	-43	-44
B = 200  kHz,  QPSK, R = 1/2	PR <sub>basic</sub> (dB)	8	30	26	-51	-54
B = 200  kHz, QPSK, R = 2/3	PR <sub>basic</sub> (dB)	9	31	27	-49	-53
B = 200  kHz,  QPSK, R = 3/4	PR <sub>basic</sub> (dB)	10	32	28	-48	-51
B = 200 kHz, 16-QAM, R = 1/2	PR <sub>basic</sub> (dB)	12	34	30	-46	-49
B = 200  kHz, 16-QAM, R = 2/3	PR <sub>basic</sub> (dB)	14	36	32	-45	-47
B = 200  kHz, 16-QAM, R = 3/4	$PR_{basic}$ (dB)	15	37	33	-44	-46
B = 200  kHz, 64-QAM, R = 1/2	$PR_{basic}$ (dB)	16	38	34	-43	-45
B = 200 kHz, 64-QAM, R = 2/3	PR <sub>basic</sub> (dB)	19	41	37	-40	-42
B = 200  kHz, 64-QAM, R = 3/4	$PR_{basic}$ (dB)	20	42	38	-39	-39
B = 250  kHz,  QPSK, R = 1/2	$PR_{basic}$ (dB)	8	30	27	-45	-52
B = 250  kHz,  QPSK, R = 2/3	PR <sub>basic</sub> (dB)	9	31	28	7	-51
B = 250  kHz,  QPSK, R = 3/4	PR <sub>basic</sub> (dB)	10	32	29	16	-50
B = 250 kHz, 16-QAM, R = 1/2	PR <sub>basic</sub> (dB)	12	34	31	20	-48
B = 250  kHz, 16-QAM, R = 2/3	PR <sub>basic</sub> (dB)	14	36	33	23	-46
B = 250 kHz, 16-QAM, R = 3/4	PR <sub>basic</sub> (dB)	15	37	34	24	-45
B = 250 kHz, 64-QAM, R = 1/2	PR <sub>basic</sub> (dB)	16	38	35	25	-44
B = 250 kHz, 64-QAM, R = 2/3	PR <sub>basic</sub> (dB)	19	41	38	28	-41
B = 250  kHz, 64-QAM, R = 3/4	$PR_{basic}$ (dB)	20	42	39	30	-40

## 5.3.4 Sharing criteria with other services

The potential interference from RAVIS to the services in adjacent frequency ranges (for example, to aeronautical radionavigation service in the band above 108.0 MHz) is not higher as the one of analogue FM service.

#### Attachment 1

#### **Normative references**

## 1 Symbols and abbreviations

For the purposes of the present Report, the following symbols and abbreviations apply:

 $\varphi_{min}$  minimum power flux-density at receiving place (dBW/m<sup>2</sup>)

A<sub>a</sub> effective antenna aperture (dBm<sup>2</sup>)

B receiver noise bandwidth (Hz)

CF combined location correction factor (dB)

 $C_1$  location correction factor (dB)

 $c_0$  velocity of light in free space (km/s)

d antenna directivity

DAB Digital audio broadcasting

 $D_{echo(max)}$  Maximum echo delay distance (km)

DRM+ DRM mode E

E RMS field-strength level (dB)

 $E_{min}$  equivalent minimum RMS field-strength level at receiving place (dB( $\mu$ V/m))

 $E_{med}$  equivalent median RMS field-strength level, planning value (dB( $\mu$ V/m))

 $F_a$  antenna noise figure (dB)

 $F_{a,med}$  antenna noise figure mean value (dB)

 $F_r$  receiver noise figure (dB)

 $F_s$  system equivalent noise figure (dB)

FM frequency modulation  $f_a$  antenna noise factor  $f_r$  receiver noise factor g linear antenna gain (dB)

G antenna gain (dB)

 $G_D$  antenna gain with reference to half-wave dipole (dBd)

 $\Delta G$  antenna gain variation (dB)

η antenna efficiency

*k* Boltzmann's constant (J/K)

K correction factor for the macro-scale standard deviation  $\sigma_m$  (dB)

l cable length (m)  $\lambda$  wavelength (m)

 $L_b$  mean building penetration loss (dB)

 $L_f$  feeder loss (dB)

 $L'_f$  feeder loss per unit length (dB/m)

L<sub>h</sub> height loss correction factor (10 m a.g.l. to 1.5 m. a.g.l.) (dB)

μ distribution factor

MMN allowance for man-made noise

MSC main service channel

 $N_s$  number of symbols per frame in DRM mode E (ms)

OFDM Orthogonal Frequency Division Multiplexing

p percentage of receiving locations (location probability) (%)

*PL* protection level in DRM mode E

 $P_{mmn}$  man-made noise level (dB)

 $P_n$  receiver noise input power (dBW)

*PR* protection ratio (dB)

 $PR_{basic}$  basic protection ratio (dB)

 $P_{s,min}$  minimum receiver signal input power (dBW)

QAM quadrature amplitude modulation

R code rate

 $R_L$  antenna loss resistance  $(\Omega)$ 

 $R_r$  antenna radiation resistance  $(\Omega)$ 

 $\sigma_b$  building penetration loss standard deviation (dB)

 $\sigma_c$  combined standard deviation (dB)  $\sigma_m$  macro-scale standard deviation (dB)

 $\sigma_{m,DRM}$  macro-scale standard deviation for DRM (dB)  $\sigma_{m,DAB}$  macro-scale standard deviation for DAB (dB)  $\sigma_{m,FM}$  macro-scale standard deviation for FM (dB)  $\sigma_{MMN}$  man-made noise standard deviation (dB)

SDC service description channel SFN single frequency network

T elementary time period of DRM mode E (ms)

 $T_f$  duration of transmission frame of DRM mode E (ms)

 $T_g$  duration of guard interval of DRM mode E (ms)  $T_s$  duration of OFDM symbol of DRM mode E (ms)

 $T_u$  duration of useful (orthogonal) part of DRM mode E (ms)

 $T_0$  absolute temperature (K)

VHF very high frequency

 $Z_{F0}$  characteristic impedance in free space  $(\Omega)$ .

#### 2 References

- [1] GE06 Final Acts of the Regional Radiocommunication Conference for planning of the digital terrestrial broadcasting service in parts of Regions 1 and 3, in the frequency bands 174-230 MHz and 470-862 MHz (RRC-06) Annex 3: Technical basis and characteristics.
- [2] EBU-TECH 3317 [July, 2007] Planning parameters for hand held reception concerning the use of DVB-H and T-DMB in Bands III, IV, V and the 1.5 GHz band.
- [3] ETSI TR 101 190; Digital Video Broadcasting (DVB); Implementation guidelines for DVB terrestrial services; Transmission aspects.

- [4] KRAUS, J.D. [December, 2001] Antennas, Mc Graw Hill College; 3rd revised edition.
- [5] GE84 Final Acts of the Regional Administrative Conference for the Planning of VHF Sound Broadcasting (Region 1 and Part of Region 3); Geneva 1984.
- [6] ETSI EN 201 980; Digital Radio Mondiale (DRM); System Specification.
- [7] ETSI EN 302 018-2; Electromagnetic compatibility and Radio spectrum Matters (ERM); Transmitting equipment for the Frequency Modulated (FM) sound broadcasting service.
- [8] Documentation G531/00328/07 [September, 2007] Compatibility Measurements DRM120, DRM and HD Radio interfering with FM Broadcast, Narrowband FM (BOS) and Aeronautical Radionavigation, German Network Agency and University of Applied Science of Kaiserslautern.
- [9] Russian Federation national standard GOST R 54309-2011 "Realtime audiovisual information system (RAVIS). Framing structure, channel coding and modulating for digital terrestrial narrowband broadcasting system for the VHF band. Technical specification"
- [10] Russian Federation national standard GOST R 55686-2013 "Realtime audiovisual information system (RAVIS). Digital modulator. Main parameters and technical requirements"
- [11] Russian Federation national standard GOST R 55687-2013 "Realtime audiovisual information system (RAVIS). Test radio receiver. General technical requirements"
- [12] Russian Federation national standard GOST R 55688-2013 "Realtime audiovisual information system (RAVIS). Content creator. Structure and protocols of data transmission"
- [13] Russian Federation national standard GOST R 55689-2013 "Realtime audiovisual information system (RAVIS). Norms and methods of metrology support"

## **Recommendations and Reports ITU-R**

Recommendation ITU-R BS.412-9 – Planning standards for terrestrial FM sound broadcasting at VHF.

Recommendation ITU-R BS.599 – Directivity of antennas for the reception of sound broadcasting in band 8 (VHF).

Recommendation ITU-R BS.641 – Determination of radio-frequency protection ratios for frequency-modulated sound broadcasting.

Recommendation ITU-R BS.1660-3 - Technical basis for planning of terrestrial digital sound broadcasting in the VHF band.

Recommendation ITU-R BT.1368-8 – Planning criteria for digital terrestrial television services in the VHF/UHF bands.

Recommendation ITU-R P.372-8 – Radio Noise.

Recommendation ITU-R P.1546-4 – Method for point-to-area predictions for terrestrial services in the frequency range 30 MHz to 3 000 MHz.

Recommendation ITU-R SM.328-11 – Spectra and bandwidth of emissions.

Report ITU-R BS.945-2 – Methods for the assessment of multiple interference.

## **Attachment 2**

## **Technical references**

# 1 Position of DRM frequencies

## 1.1 VHF Band II

he DRM centre frequencies are positioned in 100 kHz distance according to the FM frequency grid and ETSI-DRM [6]. The nominal carrier frequencies are, in principle, integral multiples of 100 kHz [5], see Table 85. A 50 kHz channel spacing is considered.

TABLE 85

Position of DRM frequencies in VHF Band II (87.5-108 MHz)

Position of DRM frequencies in VHF Band II (87.5-108 MHz)										
DRM channel centre frequency fc (MHz)	DRM channel number	DRM channel centre frequency fc (MHz)	DRM channel number	DRM channel centre frequency fc (MHz)	DRM channel number	DRM channel centre frequency fc (MHz)	DRM channel number			
87.6	1	92.7	52	97.8	103	102.9	154			
87.7	2	92.8	53	97.9	104	103.0	155			
87.8	3	92.9	54	98.0	105	103.1	156			
87.9	4	93.0	55	98.1	106	103.2	157			
88.0	5	93.1	56	98.2	107	103.3	158			
88.1	6	93.2	57	98.3	108	103.4	159			
88.2	7	93.3	58	98.4	109	103.5	160			
88.3	8	93.4	59	98.5	110	103.6	161			
88.4	9	93.5	60	98.6	111	103.7	162			
88.5	10	93.6	61	98.7	112	103.8	163			
88.6	11	93.7	62	98.8	113	103.9	164			
88.7	12	93.8	63	98.9	114	104.0	165			
88.8	13	93.9	64	99.0	115	104.1	166			
88.9	14	94.0	65	99.1	116	104.2	167			
89.0	15	94.1	66	99.2	117	104.3	168			
89.1	16	94.2	67	99.3	118	104.4	169			
89.2	17	94.3	68	99.4	119	104.5	170			
89.3	18	94.4	69	99.5	120	104.6	171			
89.4	19	94.5	70	99.6	121	104.7	172			
89.5	20	94.6	71	99.7	122	104.8	173			
89.6	21	94.7	72	99.8	123	104.9	174			
89.7	22	94.8	73	99.9	124	105.0	175			

TABLE 85 (end)

DRM channel centre frequency fc (MHz)	DRM channel number	DRM channel centre frequency fc (MHz)	DRM channel number	DRM channel centre frequency fc (MHz)	DRM channel number	DRM channel centre frequency fc (MHz)	DRM channel number
89.8	23	94.9	74	100.0	125	105.1	176
89.9	24	95.0	75	100.1	126	105.2	177
90.0	25	95.1	76	100.2	127	105.3	178
90.1	26	95.2	77	100.3	128	105.4	179
90.2	27	95.3	78	100.4	129	105.5	180
90.3	28	95.4	79	100.5	130	105.6	181
90.4	29	95.5	80	100.6	131	105.7	182
90.5	30	95.6	81	100.7	132	105.8	183
90.6	31	95.7	82	100.8	133	105.9	184
90.7	32	95.8	83	100.9	134	106.0	185
90.8	33	95.9	84	101.0	135	106.1	186
90.9	34	96.0	85	101.1	136	106.2	187
91.0	35	96.1	86	101.2	137	106.3	188
91.1	36	96.2	87	101.3	138	106.4	189
91.2	37	96.3	88	101.4	139	106.5	190
91.3	38	96.4	89	101.5	140	106.6	191
91.4	39	96.5	90	101.6	141	106.7	192
91.5	40	96.6	91	101.7	142	106.8	193
91.6	41	96.7	92	101.8	143	106.9	194
91.7	42	96.8	93	101.9	144	107.0	195
91.8	43	96.9	94	102.0	145	107.1	196
91.9	44	97.0	95	102.1	146	107.2	197
92.0	45	97.1	96	102.2	147	107.3	198
92.1	46	97.2	97	102.3	148	107.4	199
92.2	47	97.3	98	102.4	149	107.5	200
92.3	48	97.4	99	102.5	150	107.6	201
92.4	49	97.5	100	102.6	151	107.7	202
92.5	50	97.6	101	102.7	152	107.8	203
92.6	51	97.7	102	102.8	153	107.9	204

#### 1.2 VHF Band III

The frequency band of a DAB block has a bandwidth of 1.536 MHz with lower and upper guard channels to fit into the 7 MHz channels of VHF Band III. The DRM centre frequencies are positioned in 100 kHz distance beginning by 174.05 MHz and integral multiples of 100 kHz up to 229.95 MHz, see Table 86.

The nomenclature of the DRM channel identifier is given by:

(No. of the VHF channel) – (No. of the DRM channel suffix in the VHF channel),

e.g. for the first DRM channel in this table the identifier is "5-1".

TABLE 86

Position of DRM frequencies in VHF Band III (174-230 MHz)

DRM	DRM channel centre frequency $f_C$ (MHz) in VHF channel (number)									
channel suffix	5	6	7	8	9	10	11	12		
1	174.050	181.050	188.050	195.050	202.050	209.050	216.050	223.050		
2	174.150	181.150	188.150	195.150	202.150	209.150	216.150	223.150		
3	174.250	181.250	188.250	195.250	202.250	209.250	216.250	223.250		
4	174.350	181.350	188.350	195.350	202.350	209.350	216.350	223.350		
5	174.450	181.450	188.450	195.450	202.450	209.450	216.450	223.450		
6	174.550	181.550	188.550	195.550	202.550	209.550	216.550	223.550		
7	174.650	181.650	188.650	195.650	202.650	209.650	216.650	223.650		
8	174.750	181.750	188.750	195.750	202.750	209.750	216.750	223.750		
9	174.850	181.850	188.850	195.850	202.850	209.850	216.850	223.850		
10	174.950	181.950	188.950	195.950	202.950	209.950	216.950	223.950		
11	175.050	182.050	189.050	196.050	203.050	210.050	217.050	224.050		
12	175.150	182.150	189.150	196.150	203.150	210.150	217.150	224.150		
13	175.250	182.250	189.250	196.250	203.250	210.250	217.250	224.250		
14	175.350	182.350	189.350	196.350	203.350	210.350	217.350	224.350		
15	175.450	182.450	189.450	196.450	203.450	210.450	217.450	224.450		
16	175.550	182.550	189.550	196.550	203.550	210.550	217.550	224.550		
17	175.650	182.650	189.650	196.650	203.650	210.650	217.650	224.650		
18	175.750	182.750	189.750	196.750	203.750	210.750	217.750	224.750		
19	175.850	182.850	189.850	196.850	203.850	210.850	217.850	224.850		
20	175.950	182.950	189.950	196.950	203.950	210.950	217.950	224.950		
21	176.050	183.050	190.050	197.050	204.050	211.050	218.050	225.050		
22	176.150	183.150	190.150	197.150	204.150	211.150	218.150	225.150		
23	176.250	183.250	190.250	197.250	204.250	211.250	218.250	225.250		
24	176.350	183.350	190.350	197.350	204.350	211.350	218.350	225.350		
25	176.450	183.450	190.450	197.450	204.450	211.450	218.450	225.450		
26	176.550	183.550	190.550	197.550	204.550	211.550	218.550	225.550		
27	176.650	183.650	190.650	197.650	204.650	211.650	218.650	225.650		
28	176.750	183.750	190.750	197.750	204.750	211.750	218.750	225.750		
29	176.850	183.850	190.850	197.850	204.850	211.850	218.850	225.850		
30	176.950	183.950	190.950	197.950	204.950	211.950	218.950	225.950		
31	177.050	184.050	191.050	198.050	205.050	212.050	219.050	226.050		
32	177.150	184.150	191.150	198.150	205.150	212.150	219.150	226.150		

TABLE 86 (end)

DRM	DRM channel centre frequency $f_C$ (MHz) in VHF channel (number)									
channel suffix	5	6	7	8	9	10	11	12		
33	177.250	184.250	191.250	198.250	205.250	212.250	219.250	226.250		
34	177.350	184.350	191.350	198.350	205.350	212.350	219.350	226.350		
35	177.450	184.450	191.450	198.450	205.450	212.450	219.450	226.450		
36	177.550	184.550	191.550	198.550	205.550	212.550	219.550	226.550		
37	177.650	184.650	191.650	198.650	205.650	212.650	219.650	226.650		
38	177.750	184.750	191.750	198.750	205.750	212.750	219.750	226.750		
39	177.850	184.850	191.850	198.850	205.850	212.850	219.850	226.850		
40	177.950	184.950	191.950	198.950	205.950	212.950	219.950	226.950		
41	178.050	185.050	192.050	199.050	206.050	213.050	220.050	227.050		
42	178.150	185.150	192.150	199.150	206.150	213.150	220.150	227.150		
43	178.250	185.250	192.250	199.250	206.250	213.250	220.250	227.250		
44	178.350	185.350	192.350	199.350	206.350	213.350	220.350	227.350		
45	178.450	185.450	192.450	199.450	206.450	213.450	220.450	227.450		
46	178.550	185.550	192.550	199.550	206.550	213.550	220.550	227.550		
47	178.650	185.650	192.650	199.650	206.650	213.650	220.650	227.650		
48	178.750	185.750	192.750	199.750	206.750	213.750	220.750	227.750		
49	178.850	185.850	192.850	199.850	206.850	213.850	220.850	227.850		
50	178.950	185.950	192.950	199.950	206.950	213.950	220.950	227.950		
51	179.050	186.050	193.050	200.050	207.050	214.050	221.050	228.050		
52	179.150	186.150	193.150	200.150	207.150	214.150	221.150	228.150		
53	179.250	186.250	193.250	200.250	207.250	214.250	221.250	228.250		
54	179.350	186.350	193.350	200.350	207.350	214.350	221.350	228.350		
55	179.450	186.450	193.450	200.450	207.450	214.450	221.450	228.450		
56	179.550	186.550	193.550	200.550	207.550	214.550	221.550	228.550		
57	179.650	186.650	193.650	200.650	207.650	214.650	221.650	228.650		
58	179.750	186.750	193.750	200.750	207.750	214.750	221.750	228.750		
59	179.850	186.850	193.850	200.850	207.850	214.850	221.850	228.850		
60	179.950	186.950	193.950	200.950	207.950	214.950	221.950	228.950		
61	180.050	187.050	194.050	201.050	208.050	215.050	222.050	229.050		
62	180.150	187.150	194.150	201.150	208.150	215.150	222.150	229.150		
63	180.250	187.250	194.250	201.250	208.250	215.250	222.250	229.250		
64	180.350	187.350	194.350	201.350	208.350	215.350	222.350	229.350		
65	180.450	187.450	194.450	201.450	208.450	215.450	222.450	229.450		
66	180.550	187.550	194.550	201.550	208.550	215.550	222.550	229.550		
67	180.650	187.650	194.650	201.650	208.650	215.650	222.650	229.650		
68	180.750	187.750	194.750	201.750	208.750	215.750	222.750	229.750		
69	180.850	187.850	194.850	201.850	208.850	215.850	222.850	229.850		
70	180.950	187.950	194.950	201.950	208.950	215.950	222.950	229.950		

## **2** Computations of correction factors

## 2.1 Computation of the antenna gain for portable handheld reception

The antenna (linear) gain g is the product of directivity d and efficiency  $\eta$  [4].

$$g = \eta \cdot d \tag{28}$$

For lossless antennas the efficiency equals one and the gain equals the directivity.

Portable handheld reception antennas are very lossy, and therefore the gain is much lower than directivity. They are also short linear antennas, with small dimensions compared to wavelength, and have a constant directivity of about 1.5 (1.8 dBi or -0.4 dBd). The gain changes with frequency only due to efficiency.

To estimate the efficiency change with frequency a transmitting antenna is considered. That leads to the values for a receiving antenna also, because antennas are reciprocal; their directivity, efficiency and gain are the same as receiving or transmitting antenna [4].

To transfer the maximum energy from a port to an antenna or vice versa the antenna has to be matched to the port impedance. A matched antenna has an equivalent series circuit with radiation resistance  $R_r$ , antenna loss resistance and a matching circuit loss resistance. We consider the reactive part of the serial impedance as zero. The radiation resistance is small and the transmitted energy is dissipated mostly in the antenna loss resistance and the matching circuit. Only the energy in  $R_r$  is radiated. Combining all losses in  $R_L$  the antenna efficiency:

$$\eta = \frac{R_r}{R_r + R_I} \approx \frac{R_r}{R_I} \tag{29}$$

 $R_r$  can be neglected in the denominator, because  $R_r$  is much lower than  $R_L$ .

For the antenna length  $l \ll \lambda$  the radiation resistance magnitude is proportional to the square of the antenna length l relative to wavelength  $\lambda$  [4]:

$$R_r = k \cdot \left(\frac{1}{\lambda}\right)^2 = k' \cdot (l \cdot f)^2 (\Omega)$$
 (30)

where  $\lambda$  was substituted by c/f, with c the light velocity.

If the antenna dimension is not changed, and it is considered that the losses in the antenna and the matching circuit does not change significantly in the frequency range of interest, the efficiency  $\eta_2$  at a frequency  $f_2$ , compared to the efficiency  $\eta_1$  at a frequency  $f_1$ , changes as follows:

$$\frac{\eta_2}{\eta_1} = \left(\frac{f_2}{f_1}\right)^2 = \frac{G_2}{G_1} \tag{31}$$

The same is true for the gain G (dB), since the directivity does not change.

Changing the frequency from  $f_1$  to  $f_2$  the gain changes with:

$$\Delta G = 20 \log_{10} \left( \frac{f_2}{f_I} \right) \quad (dB) \tag{32}$$

## 2.2 Computation of man-made noise allowance from the antenna noise factor

#### Definition of the antenna noise factor

An antenna for terrestrial communications with efficiency one receives from its environment, no matter what shape its receiving diagram has, thermal noise with a power n:

$$n = kTB$$

where:

k: Boltzmann's constant (J/K)

T: environment temperature (K)

B: bandwidth (Hz).

If the antenna receives in the same bandwidth B Gaussian noise like man-made noise with a power i, the total power received is:

$$p_a = n + i$$

We can define an antenna noise factor  $f_a$  as:

$$f_a = \frac{p_a}{n} = \frac{n+i}{n} = 1 + \frac{i}{n}$$

and an antenna noise figure  $F_a$  given in dB [4]:

$$F_a = 10\log_{10}(f_a)$$

#### The man-made noise allowance for coverage calculations

In a link budget used for coverage calculations, the receiver is taken into account by its noise figure  $F_r$ . It can be shown, that the effect of the man-made noise i received by the antenna is equivalent to an increase of the receiver noise figure  $F_r$  by an amount MMN in dB, called man-made noise allowance.

If the antenna does not receive man-made noise, the total equivalent noise at a receiver input is:

$$p = p_r + n$$

with:

p: power sum (W)

 $p_r$ : receiver noise corresponding to the noise figure and the bandwidth (W)

n: thermal noise (kTB) (W)

 $f_r$ : receiver noise factor calculated from the noise figure  $\left(f_r = 10^{\frac{F_r}{10}}\right)$ .

The receiver noise factor is defined as:

$$f_r = \frac{p}{n} = \frac{p_r + n}{n} = 1 + \frac{p_r}{n}$$

If man-made noise *i* is received, the power at the receiver input is:

$$p = p_r + n + i$$

The interference power is increased by a factor mmn:

$$mmn = \frac{p_r + n + i}{p_r + n} = 1 + \frac{i}{p_r + n} = 1 + \frac{\frac{i}{n}}{1 + \frac{p_r}{n}}$$

but:

$$\frac{p_r}{n} = f_r - 1$$

and

$$\frac{i}{n} = f_a - 1$$

The factor mmn can be expressed as a function of  $f_r$  and  $f_a$ :

$$mmn = 1 + \frac{f_a - 1}{f_r}$$

or in dB, the allowance for man-made noise MMN:

$$MMN = 10\log\left(1 + \frac{f_a - 1}{f_r}\right)$$

The system equivalent noise figure to be used for coverage calculations is increased to:

$$F_s = F_r + MMN$$

#### Special case with antenna gain below 1.8 dBi

The antenna gain is the product of directivity and efficiency. The lowest realistic directivity is the one of a short dipole (length  $<<\lambda$ ) and it has the value 1.5 (1.8 dBi). Any gain lower than 1.8 dBi (-0.4 dBd) is due to an antenna efficiency  $\eta$  lower than 1.

If the antenna efficiency is  $\eta$ , from the received wanted signal w only  $\eta^*w$  reaches the receiver, but the Gaussian noise and the man-made noise getting into the receiver are also reduced to  $\eta^*n$  and  $\eta^*i$ .

The interference power at the receiver input is increased due to man-made noise interference i by the factor mmn:

$$mmn = \frac{p_r + n + \eta_i}{p_r + n} = 1 + \frac{\eta_i}{p_r + n} = 1 + \frac{\frac{\eta_i}{n}}{1 + \frac{p_r}{n}}$$

$$MMN = 10\log\left(1 + \eta \frac{f_a - 1}{f_r}\right)$$

The efficiency  $\eta$  can be calculated from the antenna gain  $G_D$ , for gains lower than -0.4 dBd:

$$\eta = 10^{\frac{G_D + 0.4}{10}}$$